

| | |
|---|--|
| DISTRICT | Rosebud |
| DIST_NO | 4010 |
| COUNTY If different from written on document | Pershing |
| TITLE If not obvious | Rosebud - Dreamland 1998 |
| AUTHOR | Langstaff G; Blattman M; Allen K; Gili M; Clayton R |
| DATE OF DOC(S) | 1998 |
| MULTI_DIST Y / N? | |
| Additional Dist Nos: | |
| QUAD_NAME | Sulphur 7½' |
| P_M_C_NAME (mine, claim & company names) | Rosebud Mine |
| COMMODITY If not obvious | gold; silver |
| NOTES | Correspondence; rock nomenclature; geology handwritten notes; assays; geochemistry 22p |

Keep docs at about 250 pages if no oversized maps attached
(for every 1 oversized page (>11x17) with text reduce
the amount of pages by ~25)

| | | |
|----------|----------|---------|
| SS: | DD | 9/12/08 |
| | Initials | Date |
| DB: | | |
| | Initials | Date |
| SCANNED: | | |
| | Initials | Date |

DREAMLAND 1998

60001970

4010

**NEWMONT GOLD COMPANY
ROSEBUD J.V.**

To: Whomever

Date: November 23, 1998

From: George Langstaff

Subject: **GL's Descriptive Rock Nomenclature for Rosebud Logging**

Rocks are identified as felsic volcanic rock (F), mafic volcanic rock (M), tuff (T), breccia (B), or sedimentary rock (S) as follows:

A. Volcanic Rocks (dominantly aphanitic)

1. Root Name – Composition

F – felsic, few mafic minerals (e.g., trachyte, dacite)

M – mafic, more mafic minerals (e.g., andesite, trachyte)

2. Prefix - Structure

b – brecciated (includes flow breccia as well as strongly fractured rock)

s – pseudobreccia (formed by alteration along fractures)

3. 1st Suffix – Texture

a – aphyric (no phenocrysts ≥ 1 mm)

p – porphyritic

distinctive varieties:

sp – sparsely porphyritic ($\leq 1\%$ phenocrysts)

cp – coarsely porphyritic (some phenocrysts > 4 mm)

a. 2nd Suffix – Minerals (precede with dash; if more than one, list from least to most abundant, left to right, e.g., Fp-q,p,k)

q – quartz

b – biotite

f – feldspar

h – hornblende

p – plagioclase

y – pyroxene

k – K-feldspar

o – olivine

4. Parentheses – Descriptive Features

am – amygdaloidal

sp – spherulitic

bd – banded

ve – vesicular

gl – glassy

lm – laminated (planar features ≤ 2 mm)

mmb – contains mafic magma blobs

Examples: Mcp-y,p – coarsely porphyritic pyroxene < plagioclase-phyric basalt
bFa – brecciated, aphyric rhyolite
Fsp-f(mmb) – sparsely porphyritic, feldspar(can't be identified)-phyric
latite with mafic magma blobs

Note: Alteration can eliminate mafic phenocrysts, can make K-feldspar and plagioclase indistinguishable, and can make porphyritic rocks appear to be aphyric.

The abundance of phenocrysts can vary within the same unit and some types of phenocrysts (e.g., quartz) may not be present everywhere.

B. Pyroclastic Rocks

1. Root Name

T - Tuff

2. 1st Suffix – Fragment Type (if more than one, list from least to most abundant left to right and separate by slashes, e.g., Tv/c)

a – ash (≤ 2 mm by definition but more useful to identify pyroclasts ≥ 1 mm as lithic, vitric, or crystal)

b - blocks \pm lapilli \pm ash (> 6.4 cm)

l - lithic lapilli \pm ash

v - vitric lapilli \pm ash (includes shards and pumice)

c - crystal lapilli \pm ash

a. 2nd Suffix – Minerals

see A.3.a. above

3. Parentheses – Descriptive Features

lp - lithophysal

sw - strongly welded

ww - weakly welded

and see A.4. above

Examples: Ta – ash tuff

Tl/c-q,k – lithic < crystal lapilli-ash tuff with quartz < sanidine phenocrysts

C. Breccias – if extrusive, pyroclastic, or sedimentary origin is uncertain; otherwise use protolith root name; can include fault breccias if protolith is uncertain

1. Root Name

B - Breccia

2. 1st Suffix – Number of Clast Types

m – monomict

p - polymict

3. 2nd Suffix – Support

c – clast-supported

x – matrix-supported

4. 3rd Suffix – Rounding of Clasts

r – rounded

s – subrounded to subangular

a – angular

Examples: Bmca – monomict, clast-supported breccia with dominantly angular clasts

Bpxa/s – polymict, matrix-supported breccia with subrounded clasts more abundant than angular clasts

D. Sedimentary Rocks

1. Root Name
 - S** – clastic sedimentary rock
2. 1st Suffix – Dominant Clast Size
 - c** – conglomerate (>2 mm)
 - a. Prefix – Support
 - c** – clast-supported
 - x** – matrix-supported
 - s** – sandstone (.0625 to 2 mm)
 - m** – mudstone (<.0625 mm, includes silt and clay)
3. 2nd Suffix – Secondary Clast Size (if more than one, list from least to most abundant and separate by slashes, e.g., Sst/p)
 - p** – pebbly, conglomeratic
 - n** – sandy
 - d** – muddy
 - t** – tuffaceous
4. 3rd Suffix – Structure
 - 1** – massive (beds >10 m thick)
 - 2** – thick-bedded (.05-10 m thick)
 - 3** – medium-bedded (.01-.05 m thick)
 - 4** – thin-bedded (1-10 cm thick)
 - 5** – laminated (<1 cm thick)
5. Parentheses – Descriptive Features
 - bt** – bioturbated
 - cs** – cross stratification
 - fs** – fossils
 - gn** – normally graded bedding
 - gr** – reversely graded bedding
 - sf** – syn-sedimentary folds

Examples: xSct1 – tuffaceous, matrix-supported conglomerate without apparent bedding
 Ssd4(gn) – thin-bedded, muddy sandstone with normally graded bedding
 Sm – massive mudstone

KDA

Hydrothermal Breccia in RS-425

| Interval | from depth | to depth | Au(FA) | Ag(AA) | Al(%) | As(ppm) | Ca(%) | Cu | Fe(%) | Hg(ppb) | K(%) | Mn | Mo | Na(%) | P(%) | Pb | Sb | Se | Zn |
|------------|---------------|---------------|---------------|-------------|------------|-----------|------------|----------|-------------|----------|------------|-----------|----------|-------------|--------------|-----------|----------|-------------|-----------|
| 4.8 | 1604.6 | 1609.4 | 0.007 | 0.01 | 1.15 | 22 | 0.16 | 1 | 1.06 | 25 | 0.66 | 700 | 0 | 0.03 | 0.008 | 25 | 0 | 3.5 | 68 |
| 4.8 | 1609.4 | 1614.2 | 0.012 | 0.7 | 1.12 | 16 | 0.16 | 2 | 1.26 | 60 | 0.69 | 1071 | 1 | 0.03 | 0.009 | 27 | 0 | 4.2 | 75 |
| 5.1 | 1614.2 | 1619.3 | 0.006 | 0.9 | 1.12 | 16 | 0.16 | 2 | 1.26 | 60 | 0.69 | 1071 | 1 | 0.03 | 0.009 | 27 | 0 | 4.2 | 75 |
| 4.7 | 1619.3 | 1624 | 0.009 | 0.6 | 1.12 | 16 | 0.16 | 2 | 1.26 | 60 | 0.69 | 1071 | 1 | 0.03 | 0.009 | 27 | 0 | 4.2 | 75 |
| 5 | 1624 | 1629 | 0.176 | 0.8 | 1.12 | 16 | 0.16 | 2 | 1.26 | 60 | 0.69 | 1071 | 1 | 0.03 | 0.009 | 27 | 0 | 4.2 | 75 |
| 4.6 | 1629 | 1633.6 | 0.45 | 0.9 | 0.85 | 103 | 0.2 | 3 | 1.73 | 40 | 0.53 | 404 | 2 | 0.03 | 0.008 | 26 | 4 | 14.2 | 92 |
| 5 | 1633.6 | 1638.6 | 0.084 | 0.8 | 0.85 | 103 | 0.2 | 3 | 1.73 | 40 | 0.53 | 404 | 2 | 0.03 | 0.008 | 26 | 4 | 14.2 | 92 |
| 4.6 | 1638.6 | 1643.2 | 0.058 | 0.9 | 0.85 | 103 | 0.2 | 3 | 1.73 | 40 | 0.53 | 404 | 2 | 0.03 | 0.008 | 26 | 4 | 14.2 | 92 |
| 5.3 | 1643.2 | 1648.5 | 0.145 | 0.9 | 0.85 | 103 | 0.2 | 3 | 1.73 | 40 | 0.53 | 404 | 2 | 0.03 | 0.008 | 26 | 4 | 14.2 | 92 |
| 5 | 1648.5 | 1653.5 | 0.54 | 1.5 | 0.6 | 72 | 0.2 | 5 | 1.14 | 0 | 0.4 | 96 | 9 | 0.03 | 0.007 | 67 | 0 | 16.1 | 90 |
| 2.2 | 1653.5 | 1655.7 | 0.173 | 1 | 0.6 | 72 | 0.2 | 5 | 1.14 | 0 | 0.4 | 96 | 9 | 0.03 | 0.007 | 67 | 0 | 16.1 | 90 |
| 2.9 | 1655.7 | 1658.6 | 8.359 | 7.4 | 0.6 | 72 | 0.2 | 5 | 1.14 | 0 | 0.4 | 96 | 9 | 0.03 | 0.007 | 67 | 0 | 16.1 | 90 |
| 2.9 | 1658.6 | 1661.5 | 47.793 | 46.5 | 0.6 | 72 | 0.2 | 5 | 1.14 | 0 | 0.4 | 96 | 9 | 0.03 | 0.007 | 67 | 0 | 16.1 | 90 |
| 1.8 | 1661.5 | 1663.3 | 0.222 | 0.5 | 0.55 | 88 | 0.11 | 4 | 1.04 | 10 | 0.36 | 102 | 4 | 0.02 | 0.007 | 13 | 3 | 9.5 | 76 |
| 1.3 | 1663.3 | 1664.6 | 1.397 | 1.7 | 0.57 | 177 | 0.16 | 4 | 1.28 | 15 | 0.39 | 68 | 5 | 0.02 | 0.008 | 20 | 4 | 18.9 | 81 |
| 2 | 1664.6 | 1666.6 | 0.293 | 0.6 | 0.56 | 103 | 0.14 | 3 | 1.11 | 10 | 0.38 | 44 | 3 | 0.03 | 0.01 | 14 | 0 | 7.5 | 94 |
| 4.6 | 1666.6 | 1671.2 | 0.08 | 0.5 | 0.55 | 138 | 0.19 | 2 | 1.24 | 10 | 0.37 | 82 | 4 | 0.03 | 0.01 | 18 | 0 | 10.8 | 90 |
| 4.4 | 1671.2 | 1675.6 | 0.371 | 1 | 0.53 | 156 | 0.26 | 3 | 1.29 | 0 | 0.36 | 145 | 5 | 0.04 | 0.008 | 22 | 0 | 17.2 | 73 |
| 2.9 | 1675.6 | 1678.5 | 0.155 | 1.6 | 0.53 | 134 | 0.35 | 5 | 1.56 | 10 | 0.36 | 258 | 10 | 0.04 | 0.009 | 26 | 6 | 21.9 | 83 |
| 5 | 1678.5 | 1683.5 | 0.027 | 0.9 | 0.67 | 18 | 0.26 | 2 | 1.32 | 15 | 0.34 | 556 | 7 | 0.05 | 0.01 | 20 | 3 | 8.8 | 72 |
| 5.2 | 1683.5 | 1688.7 | 0.008 | 0.8 | 0.81 | 9 | 0.25 | 2 | 1.46 | 15 | 0.37 | 844 | 7 | 0.05 | 0.012 | 22 | 0 | 2.1 | 86 |
| 4.9 | 1688.7 | 1693.6 | 0.007 | 0.001 | 0.8 | 9 | 0.37 | 2 | 1.24 | 10 | 0.37 | 566 | 7 | 0.05 | 0.011 | 21 | 0 | 0.3 | 76 |
| 5 | 1693.6 | 1698.6 | 0.008 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 5.1 | 1698.6 | 1703.7 | 0.001 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 5.3 | 1703.7 | 1709 | 0.001 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 4.9 | 1709 | 1713.9 | 0.001 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 5.1 | 1713.9 | 1719 | 0.001 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 4.7 | 1719 | 1723.7 | 0.001 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 4.8 | 1723.7 | 1728.5 | 0.001 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 5 | 1728.5 | 1733.5 | 0.006 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 2 | 1733.5 | 1735.5 | 0.001 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 4.9 | 1735.5 | 1740.4 | 0.001 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 5.1 | 1740.4 | 1745.5 | 0.006 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 4.5 | 1745.5 | 1750 | 0.001 | 0.001 | 0.84 | 5 | 0.52 | 2 | 1.61 | 15 | 0.36 | 1398 | 3 | 0.04 | 0.012 | 23 | 0 | 0.3 | 87 |
| 3.6 | 1750 | 1753.6 | 0.009 | 0.01 | 0.8 | 7 | 0.35 | 3 | 4.06 | 85 | 0.33 | 4040 | 1 | 0.05 | 0.009 | 22 | 0 | 0.9 | 95 |

HECLA MINING COMPANY

COEUR D'ALENE, IDAHO 83815

| | | | |
|---------------|--------------------|--------------------------------|----------------------------|
| BY <u>KAA</u> | DATE <u>4/9/99</u> | JOB TITLE | JOB NO. |
| CHK. | DATE | George Langstaff - Deep Decade | DIVISION |
| DWG. NO. | | | SHEET <u>1</u> OF <u>4</u> |

- follow up for Hole RS-425
- LOCATION of Gold Deposit associated w/ RS-425 not easily predictable
- needs several Holes
- 5 2400' RUC + core tails = \$300,000⁰⁰
- George Believes drilling one or two Holes would not provide sufficient info & if not willing to spend 300,000⁰⁰ it would be better to spend this money elsewhere
- the existing holes don't adequately test the target.

-
- RS-425 - attitude of Breccia 30-40° to CA
 - RS-450 - Bladed Calc - indicative of Boiling
 - RS-423 - " " " " "

RS-450 - Marc + wc + calc - 15-60' 650 ppb Au 30° to CA
Pyrite & green clay 0.5 ppb Au < 30° to CA

RS-443 - intercepts
A) HydroBx 1609' 1.4 ppm Au - wc, marc, pyrite, quartz
B) " " 370 ppb Au -

RS-444 - 220 PPB Au @ 1803' green clay.

RS-401 - Hydro Bx w/ quartz, marc, pyrite + bladed calc
426 - Bx using w/ black dr 1240 .09 opt Au 15-25° to CA

-
- For Ranking meeting - George constructed possible vein targets that have not been intersected by drilling.
 - Estimated 0.800 opt Au & constructed tabular bodies through the area to illustrate what the potential is.
 - This demonstrates there is potential for ore bodies up to 500,000 of Au

HECLA MINING COMPANY

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|---------------|--------------------|-----------|-------------------|
| BY <u>KAA</u> | DATE <u>4/9/99</u> | JOB TITLE | JOB NO. |
| CHK. | DATE | | DIVISION |
| DWG. NO. | | | SHEET <u>2</u> OF |

Model 1) Dipping 65° to the south
710' dip length, 6' thick, \Rightarrow 500,000 Au of

Constants - RS 401
488
423

This model is probably the most Geologically Reasonable.

No Geologic Constraints

Model 2) strike 110° dips 45° to north
the dip is the same as the vein in 426.
447,000 Au of 6' thick

{ not very Geologically Feasible.

Model 3) strike 15° 75° west.
strike length of 2,000' 6' thick
= 660,000 Au of.

Costly Target to Pursue.

CONE - Looked at intercept w/in 425.

Sections:

- Assumptions - 1) units Dip Eastly
2) units thickness doesn't change much
3) Faults are all Normal.

2 sets of sections

- 1) one set at NW trending similar to mine set
- 2) one set of Fence Diagrams.

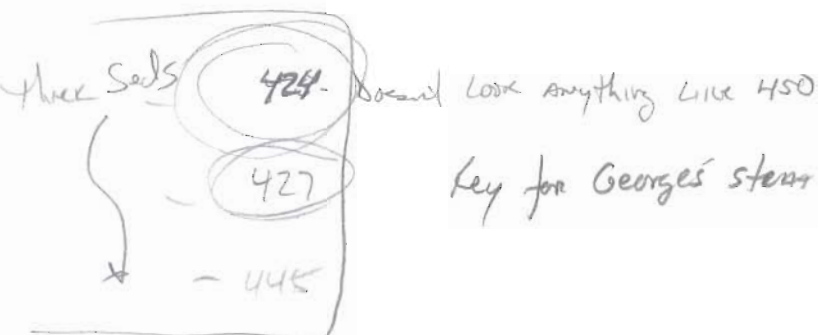
Rosebud quartz matrix \Rightarrow fp + quartz f (mmb)

George has several sections - of which I don't understand stratigraphy.

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|---------------|--------------------|-----------|-------------------|
| BY <u>KDA</u> | DATE <u>9/9/99</u> | JOB TITLE | JOB NO. |
| CHK. | DATE | | DIVISION |
| DWG. NO. | | | SHEET <u>3</u> OF |



Key for Georges starts is the "Biotite phyllite unit."

- George likes the Aphyric unit for hosting (TOP PART of a MASSIVE) ore.

- in conclusions -

- one NS Holes
- one EW Holes

- I need to get a copy of these sections & plan maps. The geology names of formations are so different I can't tell what the units ARE. Just need to continue w/ the mine set. [The rocks need relogged]

- Ramsey thinks the alteration in 450 is interesting.

The 2 Holes

⊗ George Recommends first 2 Holes Directly at the intercept. to Define the geometry & control of the 425 intercept.

⊗ Georges geochemical comparisons to the East Zone are based on only 3 holes which may not have intersected the actual East ore zone.

⊗ Geochem, there appears to be an elevation control.

- George Recommends choosing one of, because of costs of deep targets.

DL
WH
LB
BP

HECLA MINING COMPANY

COEUR D'ALENE, IDAHO 83815

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|---------------|--------------------|-------------------------|----------------------------|
| BY <u>CDA</u> | DATE <u>4/9/99</u> | JOB TITLE | JOB NO. |
| CHK. | DATE | <u>DREAMLAND Review</u> | DIVISION |
| DWG. NO. | | | SHEET <u>4</u> OF <u>4</u> |

RANDY THINKS BY PURSUING DREAMLAND, WE ARE CHASING A "RED HERRING"
SPENDING A sum of 120,000⁰⁰ for nothing the time & place.

- I HAVE ASKED for copies of George's fence diagrams.

- IP DOWN HOLE survey in 425 SHOWS NO chargeable body
within radius of 500'.

Strat Column of Greater Dreamland Area

X Sc - muddy, generally matrix-supported conglomerate with minor sandstone and mudstone

Fp-~~g~~f (mmb) - weakly porphyritic rhyolite flows and intrusions with very rare quartz ≤ 1 mm and 1-2% ^{anhedral-subhedral} kspar + plag < 3 mm phenocrysts and rare to 5% mafic magma blobs < 2 cm

Fp-b, f (mmb) - weakly porphyritic rhyolite flows and intrusions with very rare to 1% biotite ≤ 1 mm and 1-2% anhedral-subhedral kspar + plag < 3 mm phenocrysts and rare to 5% mafic magma blobs; may be gradational with Fp-~~g~~f (mmb)

Sc/SS/Sm - various conglomerates, sandstones, and mudstones

Fp-b, f (am) - weakly porphyritic rhyolite-quartz latite flows with $\leq 1\%$ euhedral biotite ≤ 1 mm and $< 1\%$ to locally 5% subhedral kspar + plag phenocrysts < 3 mm; locally amygdaloidal with up to 10% irregular amygdalites ≤ 5 mm

Sc - discontinuous conglomerate and conglomeratic sandstone

Fp-h, b - weakly porphyritic felsic flow with $\leq 1\%$ euhedral biotite ≤ 1 mm and possibly rare hornblende phenocrysts

Sc - commonly clast-supported conglomerate, possibly with intercalation of Fa or Fa (mmb)

Fa or Fsp-f - aphyric or sparsely feldspar-phyric rhyolite flow with no or rare subhedral kspar or plagioclase phenocrysts usually ≤ 1 mm

Sc - ~~discontinuous~~ ^{local} commonly clast-supported conglomerate, possibly with intercalation of Fa or Fsp-f

Fa or Fsp-f - see above; may be intercalated with or laterally equivalent to aphyric rhyolite flow with rare to 1% mafic magma blobs < 2 cm

Sc - ~~local conglomerate~~ discontinuous, commonly clast-supported conglomerate and volcanic breccia

Fa - essentially aphyric alkali-feldspar rhyolite to rhyolite flow but may have rare kspar and plag phenocrysts ≤ 1 mm locally

Sc + SS - conglomerate and sandstone

Mp-b/hp - porphyritic rhyodacite to andesite flow or intrusion with 15-30% subhedral plag ≤ 3 mm and either ~5% euhedral biotite and hornblende or 5-15% euhedral to embayed hornblende phenocrysts ≤ 3 mm, locally with rare amygdalites < 2 mm

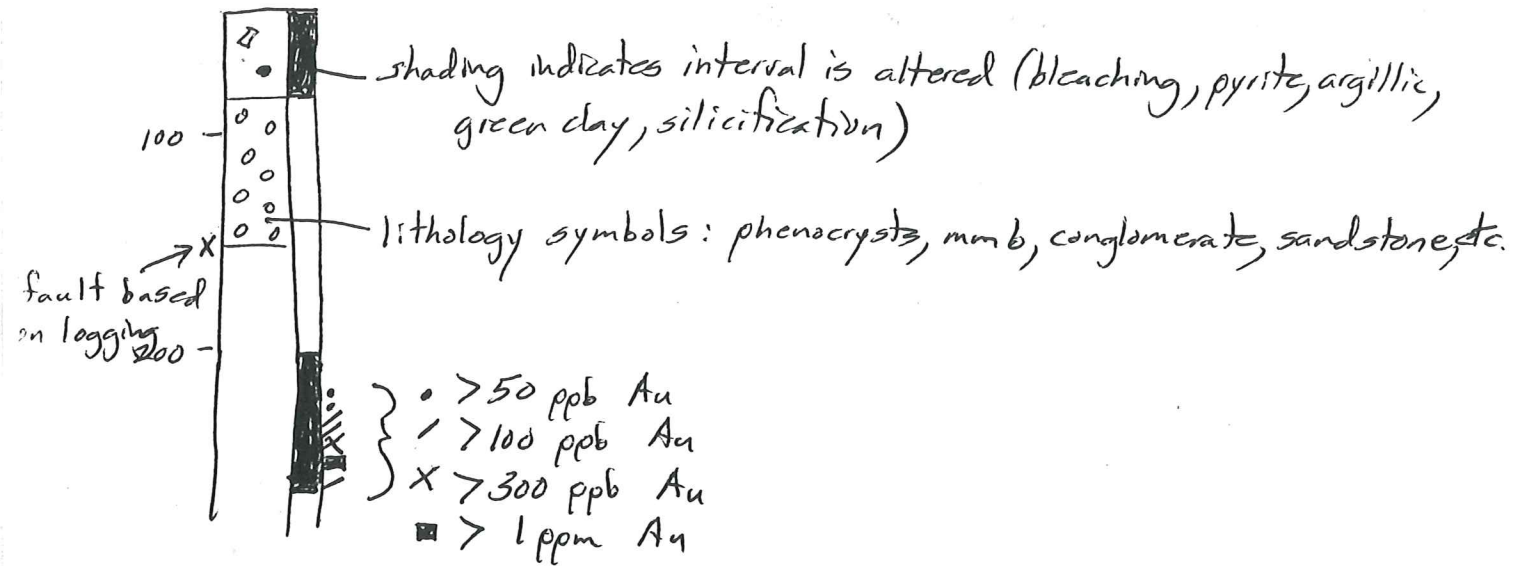
Sc + SS - sandstone or conglomerate

M (am) - amygdaloidal mafic flow or intrusion (andesite?) with 3-15% subhedral hornblende microphenocrysts and up to 10% irregular, cusped amygdalites


SS + Sm - ~~fine~~ moderately to well sorted fine to very coarse sandstone and siltstone, including normally graded turbidite beds

Sc + SS - heterogeneous matrix- and clast-supported conglomerate and sandstone with volcanic rock and pumice (?) clasts as well as common basement (phyllite, vein quartz, granitoid) clasts

Legend for drill hole strip charts



THE ROSEBUD MINING CO., LLC
MEMORANDUM

TO: Matt Blattman
FROM: Kurt D. Allen 
DATE: April 16, 1998
SUBJECT: Dreamland Geology Items You Requested.

3.2.2 Down-hole Survey

The down-hole survey of hole RS-425 was completed by Wellbore Navigation at 15032 Redhill, STE. D, Tustin, CA 92680. Survey results were obtained with the use of a surface recording gyroscopic survey system.

3.2.3 Assay Information

Significant assay results from drill hole RS-425 include two intercepts as follows:

| From | To | Length | Average Gold Grade (opt) |
|---------|---------|--------|--------------------------|
| 1655.7' | 1658.6' | 2.9' | 0.247 |
| 1658.6' | 1661.5' | 2.9' | 1.400 |

These intercepts appear to be associated with a silica and sulfide hydrothermal breccia/breccia vein. This hydrothermal breccia appears to be hosted within fine-grained, aphanitic, rhyolitic?, volcanic rock. This rock unit appears to have a large similarity to the Dozer Formation observed at Rosebud. The lower contact is gradational into a series of weakly mineralized clay-marcasite veinlets and joints oriented 20-30 degrees to the core axis. Silver values across the 5.8 feet are relatively low at 0.79 oz/ton, for a Ag: Au ratio of 1:1. This ratio is in contrast to a mineralized intercept in the pre-collar (25 feet of 0.038 oz/ton Au and 6.65 oz/ton Ag from 115-140 feet), that has a ratio of 175:1. The 5.8-foot intercept contains anomalous selenium (11-16 ppm), but subdued levels of arsenic (97 ppm), antimony (7 ppm), and mercury (100 ppb).

The nearest hole, RS-408, which contained visually attractive alteration at similar depths, but only 0.030 oz/ton gold, is 500 feet southwest. The next closest holes are RS-401 (1000 feet northwest) and RS-424 (900 feet southeast). The intercept in RS-425 is located 3800 feet northwest of the existing mine workings, and only 200 feet lower than the North Zone deposit. Historic Rosebud drill intercepts of similar high-grades (+1 oz/ton) are rare outside of the known deposits. Additionally, low silver : gold ratios are seen in Rosebud deposits, in contrast to many isolated or peripheral drill intercepts which have silver : gold ratios of 100-1000:1.

3.3 Rosebud Shear

The Rosebud shear is a fault zone with very little known about its actual location, size, competency, content, or sense of offset. The proposed drift to gain access to the intercept in hole RS-425 and set up underground exploration drill stations will cross the Rosebud shear. Main benefit to drilling the pilot hole described below is to locate the shear zone and determine the size and competency of the shear zone.

3.3 Pilot Hole etc, etc, etc.,

FOR MATT

6

3. Geology

3.1. Overview

3.2. Drill Hole Information

3.2.1. Collar

Drill hole RS-425 was surveyed by Rosebud Mine personnel and the results of this survey are as follows:

| | |
|-----------|---------------|
| Northing | 2,207,270.600 |
| Easting | 479,388.479 |
| Elevation | 5,641.958 |

3.2.2. Down-hole survey

Results from the down-hole survey, obtained from the **BLAH-BLAH-BLAH-BLAH**

3.2.3. Assay information

Drill hole RS-425

| Interval | Length | Average Grade (opt) |
|-----------------|----------|---------------------|
| 1655.7 – 1658.6 | 2.9 feet | 0.208 |
| 1658.6 – 1661.5 | 2.9 feet | 1.504 |

BLAH-BLAH-BLAH-BLAH

3.2.4. Coordinates of intercept

The drill hole information, such as collar coordinates, down-survey, and assay intervals, was entered in the Rosebud Mine's SURPAC database to obtain mine coordinates of the intercept. The calculations realized a value of:

| | |
|-----------|---------------|
| Northing | 2,207,342.166 |
| Easting | 479,391.176 |
| Elevation | 3,982.823 |

3.3. Rosebud Shear

BLAH-BLAH-BLAH-BLAH

3.4. Pilot hole

The proposed Dreamland drift, to intersect the gold intercept from exploration drill hole RS-425, needs to have a core hole drilled along its trace before development drifting begins. It is conceivable that the core hole to be drilled along the drift trace could possibly consist of one hole up to 4,000 feet in length, depending on ground conditions. The main purpose for the core hole would be for gathering geotechnical data for rock mass classification. This data will be used for assisting the driving of the drift by being able to anticipate areas of poor ground conditions which may need special ground control attention.

In addition to the geotechnical needs, a low-angle core hole from Stope 31 access to the Dreamland intercept, should cut some moderately- to highly-perspective, possibly gold-bearing northeast trending structures. The most notable structure would be the Mother Load structure. At the surface, the Mother Load structure contains anomalous geochemical values, which could become stronger with depth. There may also be several other, as yet undefined, high-angle gold bearing structures in the area between Stope 31 access and the Dreamland intercept.

The hole would require the mobilization of the LM 75 to the site, which will allow us to use HQ sized core rods. The drill should be able to get up to 2,500 feet with HQ before having to reduce down to NQ sized core rods, depending on ground conditions. This hole could take up to 30 days to drill and up to 27 days to log.

To: Ron Clayton
From: Matt Blattman
Matt Gili
CC: Rosebud Joint Venture Committee
Date: 04/13/98
Re: Proposed Dreamland Exploration Drift

A FE

In response to favorable exploration drill hole results, it is proposed that an exploration drift be driven from the current Rosebud Mine workings to the Dreamland area. This exploration drift will allow access for underground drilling and mapping of the potential ore structure.

Prior to driving the drift, a pilot hole will need to be drilled down the centerline of the drift. This hole will enable us to better understand the geologic and ground conditions before mining, thus allowing us to be better prepared for hazardous mining conditions. Drilling will cost approximately \$156,500.

The drift will be driven from the Stope 31 access directly to the high grade intercept found in the exploration drill hole RS-425. Phase 1 will be composed of driving the drift a distance of 4,050 feet at a 15.3% grade, muckbays will be driven on 400 foot intervals, and pumping stations will be created every 500 feet. At the end of the 4,050 main drift, two 250 foot cross-cuts will be mined to provide drilling stations for extensive underground drilling. Total equivalent footage to be mined is 5,250 feet at a cost of \$300 per foot. Budgeted mining costs for Phase 1 are \$1,983,000. Mining rate for the project is scheduled at an average 19.2 feet per day, requiring approximately 10 months to complete the mining of Phase 1.

If supplementary drilling is deemed necessary, Phase 2 is scheduled to add an extra 1,540 equivalent feet of mining with similar muckbay and pumping station intervals at a total mining cost of \$564,000. An extra 3 months will be needed to complete Phase 2 mining.

The additional mining will require an expansion of the Rosebud Mine's equipment fleet. It is foreseen that required equipment will include: one LHD, two 20-ton trucks, one jumbo, one bolter, and an extra lift tractor. Expected equipment cost total is \$1,817,600.

Manpower costs to operate this equipment are included in the mining cost. The drift will be mined by two miners, two truck drivers, and one mechanic per shift. The mechanic's cost is separate from the mining cost and therefore added to the total at \$215,000.

Ventilation for the tunnel will be provided by two 150hp fans in series, blowing air through an oval 48" fiberglass duct, exhausting at the working face. Total capital costs for the ventilation is estimated at \$289,000. A savings of approximately \$133,500 could be obtained by using round 48" steel duct.

Mine dewatering will be conducted by using the same type of development pump skids as are currently being used in the Rosebud Mine. A total of four skids will be necessary to complete Phase 1 and the fourth skid providing dewatering capabilities for Phase 2. Capital costs for dewatering are approximately \$125,300.

The 750 kva transformer being used near Stope 13 will be moved to the new Dreamland drift and will provide power for the majority of Phase 1. Near the completion of Phase 1, it will become necessary to

purchase a single 1,000 kva transformer. This new transformer will then have enough power to finish Phase 1 and also Phase 2. Total costs for the electrical equipment is estimated to be \$36,750.

Cost summaries are as follows:

| Phase 1 Totals | | Phase 2 Totals | |
|-----------------------|------------------|-----------------------|------------------|
| Equipment | 1,817,600 | Equipment | 0 |
| Ventilation | 155,221 | Ventilation | 0 |
| Electrical | 36,743 | Electrical | 5,511 |
| Dewatering | 125,315 | Dewatering | 0 |
| Manpower | 165,066 | Manpower | 49,520 |
| Mining | 1,982,625 | Mining | 563,625 |
| Subtotal | 4,282,570 | Subtotal | 618,656 |
| Drilling | 929,219 | Drilling | 733,594 |
| Total | 5,212,000 | Total | 1,353,000 |

Apr-14-98 04:09P

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P.01

Northwest Drilling
A Division of Boart Longyear Company
194 Arden Drive, Belgrade, Montana 59714
Telephone: 406-388-0002 • Fax: 406-388-6588
E-mail: thess@boartlongyear.com
Website: www.boartlongyear.com

Fax Message**NORTHWEST DRILLING**To: Rurf AlkaPage 1 of 2Company: Hecla MiningFax Number: 702-623-6967From: Tony Hess

Date/Time Sent: _____

Date: 4-14-98

Reference No.: _____

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NORTHWEST DRILLING

April 14, 1998

Hecla Mining Company
PO Box 2610
58 Miles West of Winnemucca
Winnemucca, NV 89446

Re: Deep hole prices for Rosebud Underground Mine

Mr. Kurt Allen

Dear Kurt;

The drill we are proposing is the Longyear LM90 125 HP drill, which is capable of drilling 3000 to 4000 feet depth, depending on hole conditions. We feel that drilling HQ to approximately 2000 feet and then reducing to NQ would give us the best opportunity to reach the maximum depth. 3000 feet is probably feasible under average hole conditions, and then it will depend on what the formation gives us without the cost becoming too high with hole stabilizing operations such as cementing.

Footage Rates

| Depth | HQ | NQ |
|-----------|----------|----------|
| 0-500 | \$ 17.50 | \$ 14.50 |
| 500-1000 | 20.00 | 16.50 |
| 1000-1500 | 22.50 | 19.00 |
| 1500-2000 | 26.00 | 21.75 |
| 2000-2500 | | 25.00 |
| 2500-3000 | | 28.50 |
| 3000-3500 | | 33.00 |
| 3500-4000 | | 38.00 |

Since the LM90 is a larger more expensive drill to own, maintain and operate the hourly rates will be as follows:

Operating \$ 97.50
Non-operating \$ 87.50

All other parts of the current contract will be as stated.

Regards

Tony Hess
Northwest Drilling

THE ROSEBUD MINING CO., LLC
MEMORANDUM

TO: Ron Clayton

FROM: Kurt D. Allen 

DATE: April 8, 1998

SUBJECT: Preliminary Cost Estimate for the Pilot Core Hole for the Dreamland Drift.

The proposed Dreamland drift, to intersect the gold intercept from exploration drill hole RS-425, needs to have a core hole drilled along its trace before development drifting begins. The core hole to be drilled along the drift trace could possibly consist of one hole up to 4,000 feet in length, depending on ground conditions. The main purpose for the core hole would be for gathering geotechnical data for rock mass classification. This data will be used for assisting the driving of the drift by being able to anticipate areas of poor ground conditions which may need special ground control attention.

In addition to the geotechnical needs, a low-angle core hole from Stope 31 access to the Dreamland intercept, should cut some moderately- to highly-perspective, possibly gold-bearing northeast trending structures. The most notable structure would be the Mother Load structure. At the surface, the Mother Load structure contains anomalous geochemical values, which could become stronger with depth. There may also be several other, as yet undefined, high-angle gold bearing structures in the area between Stope 31 access and the Dreamland intercept.

The hole would require the mobilization of the LM 75 to the site, which will allow us to use HQ sized core rods. We should be able to get up to 2,500 feet with HQ before we have to reduce down to NQ sized core rods (depending on ground conditions). This hole could take up to 30 days to drill and up to 27 days to log. Preliminary costs for the hole total \$156,500.00 consisting of \$125,000.00 for the drilling, \$13,500 for the logging, and up to \$18,000 for the assaying. Actual estimates for the above drilling will be received April 13th.

4,000' Hole w/ LM 75 DRILL

- 2,500' HQ @ 3-4 + THIN

2.5-3⁰⁰/500'

- 1,500' NQ @ -

HI

| | | | | |
|-----------|------|----------------------|---|----------------------|
| 0-500 | HQ @ | 21 ⁵⁰ /ft | = | 10,750 ⁰⁰ |
| 500-1000 | HQ @ | 24 ⁵⁰ /ft | = | 12,250 ⁰⁰ |
| 1000-1500 | HQ @ | 27 ⁵⁰ /ft | = | 13,750 ⁰⁰ |
| 1500-2000 | HQ @ | 30 ⁵⁰ /ft | = | 15,250 ⁰⁰ |
| 2000-2500 | HQ @ | 33 ⁵⁰ /ft | = | 16,750 ⁰⁰ |
| 2500-3000 | NQ @ | 32 ⁵⁰ /ft | = | 16,250 ⁰⁰ |
| 3000-3500 | NQ @ | 35 ⁵⁰ /ft | = | 17,750 ⁰⁰ |
| 3500-4000 | NQ @ | 38 ⁵⁰ /ft | = | 19,250 ⁰⁰ |

122,000⁰⁰

LM75 MOBILIZATION

1,500⁰⁰

LM75 De-MOBILIZATION

1,500⁰⁰

LOGGING - 27 DAYS @ 500⁰⁰/DAY = 13,500⁰⁰

ASSAYING -

18,000⁰⁰

156,500⁰⁰

3/31/98 - Dreamland Drive meeting w/
Randy / George / Mark / Matt / Kirt.

- Randy said they will cut a section through trace of
PROPOSED drift.

- is core fault Rosebud shear -
- shaft
- motherload

Goldora

(604) 298 - 6623

Bill Forsyth

Alan Moss

DREAMLAND MEETING 3/26/98

- 1) Check on DRILL LIGS for LONG HOLES 2000 feet.
- 2) Check on DROPPAGE for STAYING on LINE of proposed Drift.

$$\begin{array}{r} 250 \\ 4000 \\ \hline 100,000 \end{array}$$

- 3) Talk to Randy - Tuesday meet w/ Eng.

D-53-94

WALCH
SILVER + GREEN
+ GORD UNDERSTOOD
30-28
GEOB

WORKING CLASS
FOR WORKING DISTRICT