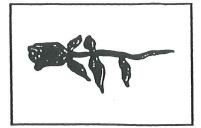
DISTRICT	Rosehud
DIST_NO	4010
COUNTY If different from written on document	Pershing
TITLE If not obvious	Rosch d-Resouve/Reserve Due Diligerere
AUTHOR	Cameron D. Muerhoff, C; Ristercelli's Knudsen H; Herdrickson R.; Clayton, R
DATE OF DOC(S)	1996-1997
MULTI_DIST Y / N2	
Additional Dist_Nos:	
QUAD_NAME	Sulphur 72
P_M_C_NAME (mine, claim & company names)	Roschad Mine Rosehad Minne Co LLC: Heela Minny Co.; Mine Development Accounted Santa Fe Poditie Gob
COMMODITY If not obvious	gold; silver
NOTES	correspondence; handwritten notes; varingrame; statisties
Keep docs at about 250 pages if	no oversized maps attached SS: DP g // 08
(for every 1 oversized page (>11) the amount of pages by ~25)	(17) with text reduce Initials Date DB: Initials Date
Revised: 1/22/08	SCANNED: Initials Date

6000 1880

4010



AS POSSIBLE.

The Rosebud Mining Company LLC

P.O. Box 2610
Winnemucca, NV 89446
Phone (702) 623-6912
Fax (702) 623-6967
Hecla Mining Co. - Manager of Mining

FACSIMILE COVER SHEET

TO: Don Cameron	FROM: Charlie Muerhoff
Hecla Mining Company	
NUMBER OF PAGES INCLUDING O	COVER:6
MESSAGE: This is really all	I have from Pete Knudsen.
Remember - he wor	had on the south zone only. If
ž.	the North's East zones, let me
know.	•
	·
We talked to Pek	today - he said he would be happy
to beef-up the pa	port if you wish to see more
documentation.	
•	,
	Charlie

Fax

To:

Steve Ristorcelli

Of:

Mine Development Associates

Fax:

702-856-6053

Phone:

702-856-5700

Pages:

1, including this cover sheet.

Date:

September 28, 1996

Steve;

The basic data used in this analysis consisted of the five foot composites. The short lengths that Charlie has classified as string #2 were not used. In all cases the variograms were calculated using a maximum assay value of 4 opt. Correlograms were calculated and then converted to variograms.

Methodology

Zones 1 and 2 were initially analyzed separately. As in the previous work, useful variograms can be obtained, but the variograms are fairly fuzzy. By combining zones 1 and 2, better variograms were obtained. Both mineralization in both zones appears to have the same spatial characteristics. Zone 1 is higher grade than zone 2, but they have the same coefficient of variation. The grouping of the data made the variograms much easier to interpret and model.

Results for Zone 1&2

Zone 11 and 21 were combined. The mineralization in zones 11 and 21 is roughly tabular with a strike of N5E and dip of about 35 to the SE. Within the tabular body the continuity of mineralization is anisotropic. The greatest continuity is along the strike of the zone.

From the desk of ...

H. Peter Knudsen Dean Montana Tech School of Mines Montana Tech 1330 West Park St. Butte, Montana 59701 408-498-4395

11:57

The variograms for zone 11 & 21 has the following parameters;

Nested Spherical Mod	lel				
Nugget Effect	=	0.60			
C1 value	=	0.30	Range	=	20 feet
C2 value	=	.10	Range	=	80 feet
Bearing of major axis	=	5	Dip	=	0.0
Tilt	=	30			
Anisotropy factors					
Semi-major	=	1.33	Minor	=	1.67

Zones 12 to 15 and 22 to 25 were also grouped together. This variograms is actually quite similar to the variograms for zones 11 and 21, except the direction of greatest continuity is along the direction of the dip. The variograms for these zones has the following parameters;

Nested Spherical Model										
Nugget Effect	=	0.55								
C1 value	=	0.30	Range =	25 feet						
C2 value	=	.15	Range =	100 feet						
Bearing of major axis		95	Dip =	30.						
Tilt	=	0.0								
Anisotropy factors										
Semi-major	=	1.33	Minor =	2.00						

Zone 3

Zone 3 proved to be more of a challenge than zones 1 &2. This is probably mostly due to the smaller number of samples available. Zones 31 to 35 were grouped together in order to get a useable variograms. While the variograms are somewhat fuzzy, the variograms show that the mineralization in zone 3 has different directions of continuity than the mineralization in zones 1 and 2. In zone 3 the mineralization has the greatest continuity in the vertical direction. In the horizontal plane the mineralization appears to be isotropic.

The parameters of the variograms are;

Nested Spherical I	Model			
Nugget Effect	=	0.30		
C1 value		0.40	Range =	100 feet

From the deak of ...

H. Peter Knudsen Dean Montana Tech School of Mines Montana Tech 1330 West Park St. Butte, Montana 59701 406-498-4395

C2 value	=	0.30	Range =	200 feet
Bearing of major axis	=	0.0	Dip =	90.0
Tilt	=	0.0	•	
Anisotropy factors				
Semi-major	=	2.00	Minor =	2.00

5406 496 4133

Zone 4

Zone 4 is a challenge. Variograms were calculated in a direction of N45E with a 35 degree dip, N45W with a zero dip, and S45W with a 60 degree dip. The first two variograms are fuzzy and there from these the mineralization appears to be isotropic. The third direction which is perpendicular to the zone gives a 2 to 1 Anisotropy.

The parameters are;

Spherical Model				
Nugget Effect	=	0.35		
C1 value	=	0.65	Range =	70 feet
Bearing of major axis	=	45.0	Dip =	35.0
Tilt	=	0.0	-	
Anisotropy factors				
Semi-major	=	1.00	Minor =	2.00
Comments				

The more that I look at this data, the more that I think Indicator kriging is a better way to estimate the grades of this deposit. The indicator variograms that I have looked at are much easier to interpret. This would be a plus in helping unravel the question of which directions have the best continuity in each zone. Indicator kriging would also be the best way to handle the high grades, rather than the arbitrary cutting that is now being practices.

Variograms for Rosebud

Zones 11&21 combined.

11:58

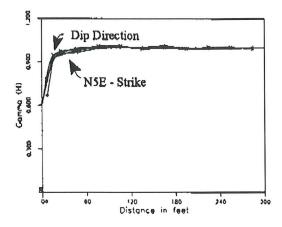


Figure 1. Zones 11&21 - dip and strike directions.

Zones 12 to 25 combined.

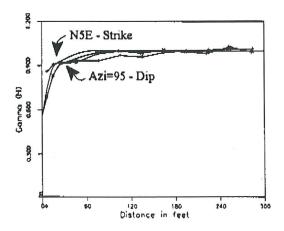


Figure 4. Zones 12 to 25 - dip and strike directions.

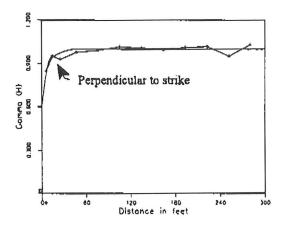


Figure 2. Zones 11&21 - perpendicular to structure.

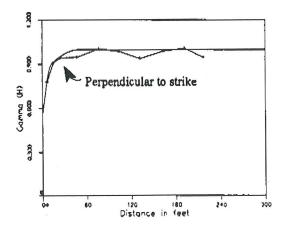


Figure 3. Zones 12 to 25 - perpendicular to structure.

Zone 3 Variograms

11:58

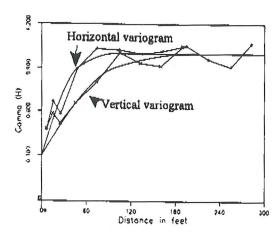


Figure 5. Zone 3 - Horizontal and vertical variograms.

Zone 4 variograms.

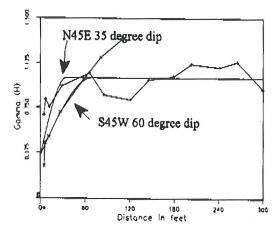


Figure 6. Zone 4 variograms.

7/8/96

charlie: FXI

See 7 1/30 am today

Geostatistical Analysis of the Rosebud Deposit

by

H. Peter Knudsen, Ph.D., P.E.
Professor
Montana Tech
of the
University of Montana
Butte, Montana 59707

VERY ROUGH

July 18, 1996

Prepared for

Mine Development Associates.

1.0 Introduction

Mine Development Associates contracted H. Peter Knudsen to determine the variography of the Rosebud Deposit. Work performed includes calculation of basic statistics and variogram models for four geologic/mineralogic zones of the deposit.

2.0 Data

The basic data used in this analysis consisted of 5ft composites prepared by Mine Development Associates. The data was grouped by MDA into four zones and within each major zone the data was further separated into five separate grade zones.

2.1 Zone 1

Many different attempts were made to model the mineralization in zone 1. The high grade samples in this zone cause the (traditional) variograms calculated to be erratic and unusable. To limit the influence of the high grades on the variogram calculation, only grades less than 4 opt were used. In addition, there are too few samples in the x4 and x5 zones to calculate variograms.

Grouping 13,14, and 15 together gives enough data to obtain an useable variogram. Adding in zone 12 improves the variogram enough so that anisotropy can be determined. The range of influence appears to be the same between the variograms calculated for 13,14 and 15, as it is for the grouping of 12,13,14, and 15. The variograms are shown in Figure 1 and 2. The variogram parameters for the grouped data from zones 12,13,14, and 15 are listed below.

Spherical Model

Nugget Effect = 0.02

C Value = 0.35

Spherical Model

Nugget Effect = 0.02

Spherical Model

HJ

Figure 1. Zone 1 Variograms (12,13,14,15).

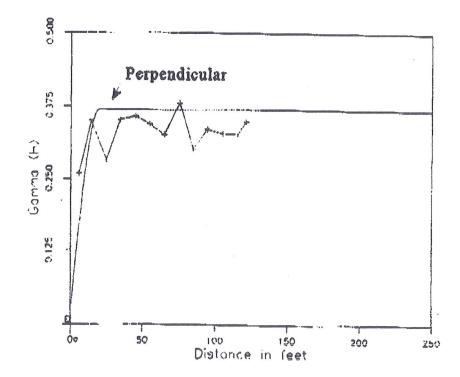


Figure 2. Zone 1 variogram (perpendicular to zone).

2.2 Zone 2

The zone 2 variograms are similar to zone 1. Again only grades less than 4 opt were used in the calculation. The resulting variograms are shown in Figure 3 and 4. The variogram parameters for the grouped data from zones 22,23,24, and 25 are listed below.

Spherical Model			
Nugget Effect	=	0.07	
C Value		0.18	
Range	=	50 feet	(On strike)
Range	=		(Down dip)
Range	663		(Perpendicular to zone)
			, , , , , , , , , , , , , , , , , , , ,

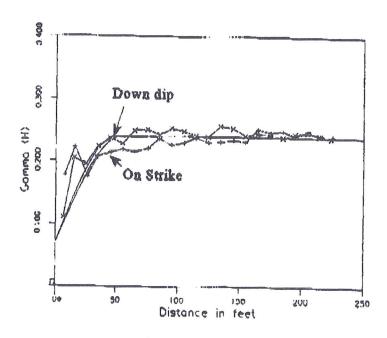


Figure 3. Zone 2 Variograms.

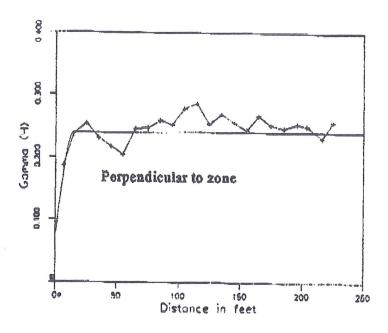


Figure 4. Zone 2 variogram (perpendicular).

2.3 Zone 3

The mineralization in zone 3 has a strong near vertical continuity. The range in the dip direction is 90 feet. The variograms are shown in Figures 5 and 6. The variogram parameters for the grouped data from zones 32,33,34, and 35 are listed below.

Spherical Model			
Nugget Effect		0.08	
C Value	=	0.21	0
Range	etamp	60 feet	(On strike)
Range	•	90 feet	(Down dip)
Range		15 feet	(Perpendicular to zone)

When the data from zones 31,32,33,34,and 35 where grouped together, the variograms were smoother and better defined, but the ranges and anisotropy remained the same.

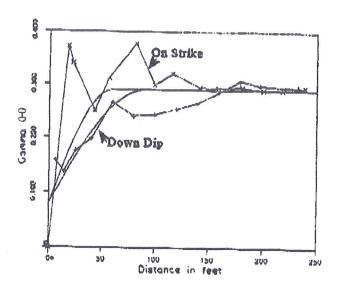


Figure 5. Variograms for zone 3 (32,33,34,35).

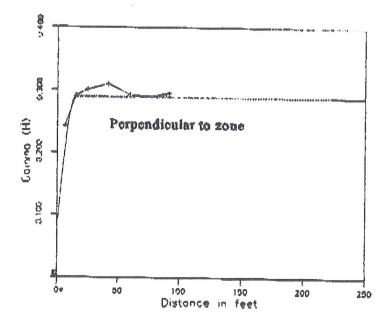


Figure 6. Zone 3 variogram (perpendicular to zone).

2.4 Zone 4

All the data in zone 4 was grouped together to get enough samples to calculate a variogram, yet only the omni-directional variogram had any observable structure. There are not enough samples to determine anisotropy. The omni-directional variogram is shown in Figures 7. The variogram parameters are shown below.

Nested Spherical N	Model		7
Nugget Effect	=	0.010	v.
C1 Value	=	0.010 0.015	
Range 1	=	20 feet	
C2 Value		0.015	
Range 2	=	90 feet	

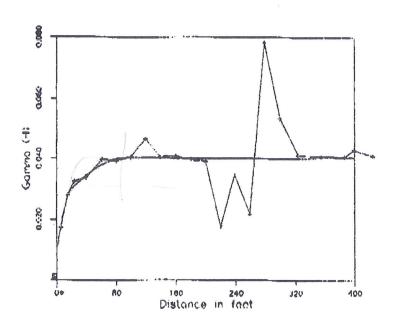


Figure 7. Omni-directional variogram for zone 4.

3.0 Indicator Variograms

Indicator variograms were calculated for zone 1 using all the data and using only the data from 12, 13,14, and 15. The variograms for the second grouping are better behaved that when zone 11 is added to the data set. In general the variograms are very smooth and easy to interpret and I believe can be used to better define the anisotropy of the mineralization. Selected printouts of the variograms are attached. I have not fit models to any of the indicator variograms.

AM

FOR CUTOFF = 0.100E-01

Zone ? GOLD DATA

						CURROLLI I CH
C	NGLE = 85. LASS SIZE = AX DISTANCE = OGARITHMS =NO	D1P = 25 545		= 35.	MEAN VARIANCE STD DEVIATION NO.OF SAMPLES	0.2030.1620.4021699
	0:STANCE 0 - 15 15 - 30 30 - 45 45 - 70 70 - 95 95 - 120 120 - 145 145 - 170 170 - 195 195 - 220 220 - 245 245 - 270 270 - 395 295 - 320 320 - 345 345 - 370 370 - 395 395 - 420 420 - 445 445 - 470 470 - 495 495 - 520 520 - 545	23144 23379 25339 26949 25652 25662 21667 21827 18199 14534 13780 12751	DRIFT -0.763E-01 -0.862E-02 0.468E-01 0.568E-02 -0.678E-02 -0.115E-01 -0.236E-01 -0.336E-01 -0.336E-01 -0.336E-01 -0.37E-02 0.341E-01 -0.37E-02 0.341E-01 -0.140E-01 -0.140E-01 -0.472E-01 0.356E-01	GAMM/ 1,08 0.659 0.643 0.774 0.770 0.893 0.945 0.945 0.944 0.939 0.934 0.946 0.953 0.953 0.968 0.978 0.968 0.978	(H) X_GAMMA(1 0.967 0.934 0.956 0.971 0.989 0.988 0.984 1.00 0.993 1.02 1.00 0.985 1.01 0.970 0.989 0.989 0.999 0.991 0.975 0.995	
	0.108E+01 + 0.103E+01 +	幹	# # # # # #	** *		章 章
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	0.922E+00 +		xxx		" " "	X
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187	0.813E+00 +	X X				
A	0.759E+00 + 0.705E+00 +	v				
M	0.651E+00 +	X				
A	0.596E+00 +	^				
	0.5426+00 +					
	0.488E+00 +					
1/r	0.434E+00 +					
M	0.380E+00 +					
r e	0.325E+00 +					
	0.2716+00 +					
	0.217E+00 +					
	0.163E+00 +					
	0.108E+00 +					
	0.542E-01 +					
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						5 4 4 4

INDICATOR VARIOGRAM FOR CUTOFF # 0.500E-01

Zone 1 GOLD DAYA

DATA USED IN CALCULATIONS

10

```
ANGLE = 85. DIP = 0. WINDOW = 35. MEAN
                                                          - 0,620
                    25.
CLASS SIZE =
                                            VARIANCE
                                                          € 0.236
MAX DISTANCE =
                    545.
                                            STD DEVIATION = 0.485
LOGARITHMS -NO
                                            NO. OF SAMPLES =
     DISTANCE
                # PAIRS
                                      Gamma (H) X_Gamma(H) aver dist
0.664 0.604 11.6
                            DRIFT
     0 .
            15
                   131
                         0.687E-01
                                     0.664
                                                                 11.6
    15 -
                   567
                        -0.564E-01
                                     0.711
                                                  0.667
    30 -
            45
                  2349
                         0.643E-01
                                     0.846
                                                  0.783
                                                                 39.0
    45 -
            70
                  9247
                         0.554E-01
                                     0.939
                                                  0.875
                                                                 58.5
    70 -
            95
                 14285
                         0.951E-01
                                     0.978
                                                  0.907
                                                                 83.5
    95 -
           120
                 19471
                         0.806E-01
                                      1.04
                                                  0.972
                                                                107.8
   120 -
           145
                 23144
                         0.767E-01
                                      1.02
                                                  0.960
                                                                132.4
   145 -
           170
                 23379
                         0.2966-01
                                      1.03
                                                  0.975
                                                                157.6
   170 .
           195
                 25339
                         0.3452-01
                                      1.04
                                                  0.990
                                                                182.8
                        0.346E-01
-0.317E-01
   195 -
           550
                 26949
                                     0.997
                                                  0.950
                                                                207.6
   220 -
           245
                 25652
                                      1.02
                                                  0.984
                                                                232.4
   245 .
           270
                 25462
                         0.441E-01
                                      1.05
                                                   1.01
                                                                257.2
   270 -
           295
                 21667
                         0.8265.02
                                      1.02
                                                  0.984
                                                                282.4
   295 .
           320
                 21827
                         0.317E-01
                                      1.05
                                                   1.02
                                                                307.5
   320 -
           345
                 18195
                         0.238E-01
                                      1.01
                                                  0.996
                                                                332.1
   345 -
           370
                 14534
                         0.755E-01
                                      1.01
                                                   1.01
                                                                357.7
   370 -
           395
                 13780
                         0.8236-01
                                     0.980
                                                   1.01
                                                                382.3
   395 -
           420
                 12751
                         0.220E-01
                                     0.988
                                                   1.02
                                                                407.3
  420 -
           445
                 11336
                        -0.181E-01
                                      1.01
                                                   1.02
                                                                432.4
   445 -
           470
                 10925
                        -0.8242-03
                                     0.988
                                                   1.01
                                                                457.2
   470 -
           495
                  9049
                         0.119E-01
                                      1.01
                                                  1.00
                                                                481.8
   495 .
           520
                  7990
                         0.651E-01
                                                                508.2
                                     0.898
                                                  0.919
  520 .
           545
                  7688
                         0.6112-01
                                     0.936
                                                  0.919
                                                                531.1
   0.105E+01 +
                         ** ** ** ** **
   0.100E+01 +
   0.949E+00 +
   0.897E+00 +
                 X w
   0.844E+00 +
  0.791E+00 +
   0.738E+00 + X
  0.686E+00 + X*
  0.633E+00 + *
M
  0.580E+00 +
   0.527E+00 +
   0.475E+00 +
  0.422E+00 +
  0.369E+00 +
   0.3162+00 +
   0.264E+00 +
   0.211E+00 +
   0.158E+00 +
   0,105E+00 +
   0.527E-01 +
             0.
                      100.
                                200.
                                          300.
                                                    400.
                                                               500.
```

INDICATOR VARIOGRAM FOR CUTOFF = 0.100

Zone 1 GOLD DATA

```
ANGLE = 85. DIP = 0. WINDOW = 35. MEAN CLASS SIZE = 25. VARIA
                                                       - 0.725
                                         VARIANCE
                                                      ≈ 0.200
MAX DISTANCE -
                   545.
                                         STD DEVIATION = 0.447
LOGARITHMS -NO
                                         NO. OF SAMPLES =
    DISTANCE
               PAIRS
                        DRIFT
                                   GAMMA (H) X_GAMMA(H) AVER DIST
0.554 0.367 11.6
    0 -
           15
                 131 0.7635-02
                                   0.554
   15 .
           30
                 567 -0.670E-01
                                   0.927
                                               0.675
                                                             8.85
   30 -
           45
                 2349
                       0.438E-01
                                   0.975
                                               0.750
                                                             39.0
   45 .
           70
                 9247
                       0.5528-07
                                    1.02
                                               0.818
                                                             58.5
   70 .
          95
                14285
                       0.977E-01
                                    1.12
                                               0.887
                                                             83.5
   95 -
          120
                19471
                       0.837e-01
                                    1.11
                                               0.940
                                                            107.8
  120 -
          145
                23144
                       0.763E-01
                                    1.12
                                              0.945
                                                            132.4
  145 .
          170
                23379
                       0.4682-01
                                    1.10
                                              0.938
                                                            157.6
  170 -
          195
                25339
                       0.524E-01
                                    1.09
                                              0.947
                                                            182.8
  195 -
          220
                26949
                       0.445E-01
                                    1.06
                                              0.933
                                                            207.6
  550 -
          245
                25652
                     -0.213E-01
                                    1.06
                                               0.975
                                                            232.4
  245 -
          270
                25462
                       0.514E-01
                                    1.12
                                               1.03
                                                            257.2
  270 .
          295
               21667
                       0.9098-02
                                    1.07
                                                            282.4
                                                1.00
  295 .
          320
               21827
                       0.103E-01
                                    1.05
                                               1.01
                                                            307.5
  320 -
          345
                18195
                       0.137E-01
                                               1.01
                                   1.01
                                                            332.1
  345 .
         370
                14534
                       0.642E-01
                                   0.991
                                               1.02
                                                            357.7
  370 -
         395
                13780
                       0.673E-01
                                   0.905
                                               1.02
                                                            382.3
  395 .
          420
                12751
                       0.604E-02
                                   0.930
                                                            407.3
                                               1.01
  420 -
         445
                11336
                     -0.243E-01
                                   0.974
                                               1.02
                                                            432.4
  445 .
         470
                10925
                                  0.948
                      -0.4238-01
                                               1.03
                                                            457.2
  470 .
         495
                9049
                     -0.6198-02
                                   8.946
                                               1.02
                                                            481.8
  495 -
         520
                7990
                      0.161E-01
                                   0.841
                                              0.980
                                                            508.2
  520 -
         545
                7688
                       0.260E-03
                                  0.898
                                              0.972
                                                            531.1
   0.112E+01 +
                    x x x x x x x
                     0.107E+01 +
                 X
   0.101E+01 +
               K
   0.956E+00 + X
   0.899E+00 +
  0.843E+00 +
  0.787E+00 +
  0.7316+00 + *
M 0.675E+00 +
A 0.618E+00 +
   0.562E+00 + X
  0.506E+00 +
 0.450E+00 +
H 0.394E+00 +
  0.337E+00 +
  0.281E+00 +
  0.225E+00 +
  0.169E+00 +
  0.112E+00 +
  0.562E-01 +
                                    проимофоновфонофонования
                   100.
                             200.
                                      300. 400.
                                                          500.
```

1 INDICATOR VARIOGRAM FOR CUTOFF = 0.250

Zone 1 GOLD DATA

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MINE DEVELOPMENT ASSOCIATES

MINE ENGINEERING SERVICES SURPAC MINING SYSTEMS

DATE: September 11, 1996

TO: Charlie

FAX: 702-623-6967 FROM: Steven Ristorcelli

THIS TRANSMISSION CONSISTS OF __17 PAGES INCLUDING THIS COVER PAGE.

IF ALL PAGES ARE NOT RECEIVED, PHONE (702) 856-5700.

FAX NUMBER: (702) 856-6053

Charlie.

This fax is to paraphrase the conversation w/ Pete K. today and give you some more "support" data. Basically, the only valid point Santa Fe has is the estimation from variable length samples.

- lf there is a bias in the data, then there will be a bias in the kriging. The weighted averages by zone did not change significantly based on the fax I sent to you this morning. I am sending several sheets on the zones showing the statistics of all samples less than 2.5 ft in length (the point at which Pete K. starts to get concerned). I have looked at them and found that they are not terribly different from the stats of the corresponding zones in total. Don't forget, once we move out and cut the outliers it will result in lower means. As we stated, send Pete both files (assay and composite down hole by rock type) and he will be the judge as to whether we should use 5 ft composites or assays. Consider compositing to 5 ft just to avoid having to constantly deal with these sorts of headaches. I don't feel it will materially affect the outcome, just the perception. And finally, there is no reason to work with 10 ft composites over 5 ft composites. Kriging will put valid grades in 10 ft blocks from 5 ft samples.
- 2. Pete used correlograms.
- 3. The comment on sub-blocking by Santa Fe is not applicable and therefore does not warrant a comment. However, Santa Fe's note on this is nonsense. Sub-blocking is for geometry only.
- 4. On his comment no. 5 in the Conclusions, Pete just shrugged it off as nonsense. I have asked him to comment on it in writing for you or to call you today. My comments are: kriging takes into account and compensates for clustered data. Second, we used zones because there is a radical change in local means. The zoning takes this into account and therefore in all our estimation domains we do have "stationarity of mean". And of coarse, the second half of this paragraph is also moot because we used the correlogram.

STAT. BASIC STATS	Descriptive by ZONE: G_	Statistics	(all9999.	sta;		÷		
Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sam	Minimum	: Maximum	Range
AUAVG2 AGAVG LENGTH	67 67 67	.064701 2.535821 1.770149	021620 509497 1.624600	.151023 5.581139 1.915699	4.3350 169.9000 113.600C	0.000000 0.000000 .30000	2.90700 75.05000 2.50000	2.90700 75.05000 2.20000
112 JAN		0.019			· · · · · · · · · · · · · · · · · · ·			
STAT. BASIC STATS	Descriptive by ZONE: G_1		(all9999.	sta;				
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtesis	
AUAYG2 AGAYG LENGT!!	.1252 155.8739 .3561	.35389 12.48495 .59671	.043235 1.525279 .072900	8.088548 5.624617 769735	.292836 .292836 .292836	65.90396 30.71450 22525	.577996 .577996 .577996	Sec.

211 total An 0.019 0.679 Ag Q.35 2.75 Length 4.78 1.07

STAT. BASIC STATS	Descriptive by ZONE: G_		s (al19999.sta)			*		
Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sum	Minimum	Maximum.	Range
AUAVG2 AGAVG LENGTH	3C 3C 3C :	.134600 1.573667 1.886667	.074664 .279591 1.705125	.194536 2.367743 2.368208	4.03800 47.21000 56.60000	C.030000 C.030000 .600000	.80700 14.63000 2.50000	.83703 14.63003 1.93003

STAT. BASIC STATS		criptive Statistics (all9999.sta) ZONE: G_2:12									
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis				
AUAVG2 AGAVG LENGTH	.02576 12.01038 .23637	.160511 3.465599 .48617?	.029305 .632729 .088763	2.788296 3.105729 798526	.426892 .426892 .426892	10.20313 9.25076 .45625	.832746 .832746 .832746				

STAT. BASIC STATS	Descriptive by ZONE: G		s (all9999.	sta				
Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
AUAVG2 AGAVG LENGTE	22 22 22	.652545 5.195000 1.677273	.005558 1.032625 1.332494	1.299533 9.357375 2.022051	14.3560 114.2900 36.9000	.00400C .04000C .20000C	7.08500 33.14000 2.50000	7.08100 33.10000 2.30000

STAT. BASIC STATS	Descriptive by ZONE: G	re Statistics 23:13	s (all9999.	sta)			
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis
AUAVG2 AGAVG LENGTH	2.12936 i 88.13321 .60470	1.459233 9.387929 .777623	.311110 2.001513 .165790	4.456865 2.260857 599855	.490962 .490962 .490962	2C.47442 4.17403 -1.09765	.952780 .952780 .952780

STAT. Descriptive Statistics (all9999.sta) BASIC by ZONE: G_4:14 STATS								
Variable	Valid N	Mear.	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
AUAVG2 AGAVG LENGTH	14 14 14	1.086714 6.994286 1.471429	.512210 099181 1.085482	1.66122 14.08775 1.85737	15.21400 97.92000 20.60000	.013000 .160000	2.65500 42.97000 2.50090	2.64200 42.81000 2.10000

STAT. BASIC STATS	Descriptive Statisti by ZONE: G_4:14	.cs (all9999.	sta}	*		
Variable	Variance : Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis
AUAVG2 ASAVG LENGTH	.9901 .99501 150.9348 12.28555 .4468 .66844	3.233452	.475894 2.455401 .132272	.597380 .597380 .597380	-1.62392 5.81033 -1.03856	1.15405C 1.15405C 1.154C50

Z 14 1.202 0.918 7.44 12.57 4.37 1.16 STAT. Descriptive Statistics (all9999.sta)
BASIC by ZONE: G_B:15

STATS

,	'ariable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
	AUAVG2	3	19.34133	-41.6631	80.34579	58.C24C0	2.975000	47.57900	44.60400
÷	AGAVG	3	22.56333	-13.7702	58.89682	67.690C0	8.770000	37.90000	29.13000
	LENGTH	3	1.56667	C874	3.22069	4.70000	1.000000	2.30000	1.30000

STAT. Descriptive Statistics (all9999.sta; BASIC by ZONE: G_5:15 STATS											
Variable	Variance	Std.Dev.	Standard Error	: Skewness	Std.Err. Skewness	Kurtcsis	Std.Err. Kurtosis				
AUAVG2 AGAVG LENSTH	603.0756 213.9256 .4433	24.55760 14.62620 ! .66583	14.17834 8.44444 .38442	1.666996 .469546 1.055832	1.224745 1.224745 1.224745		=======================================				

Z 15 7.292 10.178 15.08 13.07 4.35

STAT. BASIC STATS	Descriptive by ZONE: G		s (all9999.s	sta)				
Variable	Valid N	Mear.	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
AUAVG2 AGAVG LENGTH	40 40 40	.014575 .456000 1.785000	.007683 058947 1.609150	.021467 .970947 1.960850	.58300 · 18.24000 · 71.40000	0.000000 0.000000 .600000	.114000 7.950000 2.500000	.114000 7.950000 1.900000

STAT. Descriptive Statistics (all9999.sta) BASIC by ZONE: G_6:21 STATS											
	Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis			
	AUAVG2 AGAVG LENGTH	.000464 2.592542 .302333	.021549 1.610137 .549848	.003407 .254585 .086939	2.973792 4.319718 573342	.373783 .373783 .373783	11.20121 17.77601 81862	.732600 .732600 .732600			

STAT. BASIC STATS	Descriptive by ZONE: G		s (all9999.	sta:		÷		
Variable	Valid X	Mean	Confid. -95.000%	Confid. 95.000	Sun	Minimum	Maximum	Range
AUAVG2 AGAVG LENGTH	17 17 17	.163529 2.249824 1.935294	.055634 932085 1.632783	.271425 5.429732 2.237805	2.78000 38.23000 32.90000	.001000 .040000 .600000	.82200 25.94000 2.50000	.82100 25.90000 1.90000

STAT. BASIC STATS	Descriptive Statistics (all9999.sta) by ZONE: G_7:22										
Variable	Variance	Std.Dev.	Standard Error	Skewness	Kurtosis	Std.Err. Kurtosis					
AUAVG2 PVADA ETDNEL	.04404 38.27528 .34618	.209852 6.186701 .588368	.050897 1.500496 .142700	2.25489 3.94781 -1.05138	.549747 .549747 .549747	5.65850 15.93977 .09321	1.063198 1.063198 1.063198				

Z 22 0.100 0.119 0.715 1.701 5.00

STAT. Descriptive Statistics (all9999.sta) by ZONE: G_8:23 BASIC STATS Confid. Confid. Wariable Valid N -95.000ā 95.000 Mean Sum Minimum Maximum Range 11

.907405

2.070746

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5.633CC

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.003000

.060000

.200000

2.055000

4.4400C0

2.400000

2.052000

4.380000

2.200000

STAT. Descriptive Statistics (all9999.sta) BASIC by ZONE: G 8:23 STATS Standard Std.Err. Std.Err. Variable Variance Error Skewness Skewness Kurtosis Std. Dev. Kurtosis AUAVG2 .346252 .588432 .177419 2.012456 .660637 4.739305 1.279416 AGAVG 1.556022 1.247406 .376107 1.883283 4.160826 1.279416 .660687 .569636 LENGTE .754743 .227563 -.932233 .660687 .C43244 1.27941€

.1:6777

.394708

1.074775

Z 23 0.364 0.453 1,84 3.59 4.68

.512091

1.232727

1.581818

1:

11

AUAVG2

LENGTH

AGAVG

STAT. BASIC STATS	Descriptive by ZONE: G	e Statistics 9:24	s (all9999.	stā;	•			
Variable	Valid N	.Mear.	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
AUAVG2 AGAVG LENGTH	2 2 2	.572000 .640000 2.000000	-5.52698 63062	6.670979 1.910620	1.144000 1.280000 4.000000	.092000 .540000 2.000000	1.052000 .740000 2.000000	.960000 .200000 0.000000

STAT. Descriptive Statistics (all9999.sta) BASIC by ZONE: G_9:24 STATS										
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis			
AUAVG2 AGAVG LENGTH	.460800 .020000 0.000000	.678823 .141421 C.COCCOO	.480000 .100000 0.000000							

STAT. BASIC STATS	Descriptive by ZONE: G	Statistics 10:31	all9999.	sta;	*				
Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sun	Minimum	Maximum	Range	
ADAVG2 AGAVG LENGTH	14 14 14	.024286 .150714 1.850000	.010981 .035227 1.581322	.037590 .266201 2.118678	.3400C 2.11000 25.90000	.001000 .030000 .900000	.07300C .77000C 2.500000	.072000 .740000 1.600000	

STAT. BASIC STATS		Descriptive Statistics (all9999.sta) by ZONE: G_10:31										
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis					
AUAVG2 AGAVG LENGTH	.000531 .040007 .216538	.023043 .200018 .465337	.006159 .053457 .124367	.982547 2.731652 863027	.597380 .597380 .597380	229038 7.714764 .536183	1.154050 1.154050 1.154050					

STAT. BASIC STATS	Descriptive by ZONE: G		all9999.s	sta;		*		
Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
AUAVG2 AGAVG LENGTH	5 5 5	.080200 .212000 1.660000	.023331 .113681 .757762	.137069 .310319 2.562238	.401000 1.060000 8.300000	.02900C .140000 .800000	.147000 .340000 2.500000	.118000 .200000 1.700000
STAT.	Descriptive	e Statistics	s (all9999.	sta)				

STAT. BASIC STATS	Descriptive by ZONE: G	Statistics _11:32	(all9999.s	sta)			·
Variable	Variance	Std. Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis
AUAVG2 AGAVG LENGTH	.002098 .006270 .528000	.045801 .079183 .726636	.320483 .335412 .324962	.688155 1.324727 273938	.912871 .912871 .912871	20590 1.63298 -2.34440	2.000000 2.000000 2.000000

STAT. BASIC STATS	Descriptive by ZONE: G	e Statistics _12:33	s (ali9999.	sta:	*				
Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range	
AUAVG2 AGAVG LENGTH	2 2 2	.447000 .695000	-1.10316 89328 -3.48249	1.997157 2.283276 6.682482	.894C00 1.390C00 3.200C00	.325000 .570000 1.200000	.569000 .820000 2.00000	.244000 .250000 .800000	

STAT. BASIC STATS		Descriptive Statistics (all9999.sta) by ZONE: G_12:33									
Variable	Variance	Std.Dev.	Standard Error Skewnes		Std.Err. Skewness	Std.Err. Kurtosis					
AUAVG2 AGAVG LENGTH	.029768 .031250 .320000	.172534 .176777 .565685	.122000 .125000 .400000		 	 	 				

STAT. BASIC

Descriptive Statistics 'all9999.sta. by ZONE: G_13:34

STATS

Variable	Valid N	Mean	Confid- -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
AUAVG2	1	1.753000			1.753000	1.753000	1.753000	
AGAVG	1	2.440000			2.440000	2.44C00C	2.440000	
LENGTH	1	1.000000	;		1.000000	1.000000	1.000000	

STAT. BASIC STATS	Descriptive by ZONE: G	e Statistics _13:34	s (all9999.	sta)			
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis
ATAVG2							
AGAVG	i	·			!		
LENGTH	·				:		

234 1.399 1.547 2.95 4.00

STAT. BASIC STATS	Descriptive by ZONE: 3		s 'all9999.s	sta'	*			
Variable	Valid N	Mean	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
AUAVG2 AGAVG LENGTH	14 14 14	.027643 .205714 1.642857	004257 .068002 1.339259	.059542 .343427 .1.946455	.38700 2.88000 23.00000	0.000000 0.00000 .40000	.218000 .870000 2.500000	.218000 .870000 2.100000

STAT. BASIC STATS	Descriptive Statistics (all9999.sta) by ZONE: G_14:41								
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis		
AUAVG2 AGAVG LENGTH	.003052 .056868 .276484	.055249 .238512 .525817	.014766 .063745 .140531	3.632359 2.067220 878563	.597380 .597380 .597380	13.42695 4.29740 1.31034	1.154050 1.154050 1.154050		

Z 41 0.017 0.028 0.18 0.363 4.62

for Z42

STAT. BASIC STATS	Descriptive by ZONE: G		s (all9999.s	*				
Variable	Valid N	Mean	Confid- -95.000%	Confid. 95.000	Sum	Minimum	Maximum.	Range
AUAVG2	1	.492000			.492000	.492000	.492000	
AGAVG	1	.81C00C			-81C0C0	.810000	.B1000C	
LENGTH	2	1.100000			1.100000	1.100000	1.100000	

STAT. BASIC STATS	ASIC by ZONE: G_15:43									
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis			
AUAVG2										
AGAVG					·					
LENGTH			i							

243 0.314 0.219 1.17 3.19 5.07

STAT. BASIC STATS	Descriptive by ZONE: G		all99999.s	ta;		*		
Variable	Valid N	Mean	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
AUAVG2 AGAVG LENGTH	1 1 1	1.517000 3.940000 2.300000			1.517000 3.940000 2.300000	1.51700C 3.94000C 2.30000C	1.517000 3.940000 2.300000	

STAT. BASIC STATS	BASIC by ZONE: G_16:44											
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis					
AUAVG2												
AGAVG												
LENGTH					·							



School of Mines Montana Tech Memorandum

September 13, 1996

To:

Charlie Muerhoff, Steve Ristorcelli

From:

Pete Knudsen, Dean

Re:

Geostat questions

Concerns expressed by Santa Fe

1. Use of assay data violates Santa Fe's standard practices. Comment:

It is important that all samples have the same support, ie., length. It is acceptable to use assay data as long as they have the same lengths. There is always some samples that will have shorter lengths, usually at the end of the hole. These can be ignored if they are very small, or used in the analysis if they are at least one half the length of the other samples. What must be avoided is the use of short samples that were expressly taken to sample a high grade structure. This will lead to a bias.

The resolution to this problem is to composite use down-the-hole composites of 5 feet length.

2. A relative variogram or correlogram may be more appropriate. Comment:

Correlograms were calculated and converted to variograms.

3. Block Size. Santa Fe seems to worry that the sub - blocking ability of SURPAC2 will change the "variance". Also, Santa Fe seems to feel the composite length must be the same as the block height.

Comment:

Kriging can be done with composites that are a different size than the block. Most software is not written for the case of the composites being longer than the block, but all of the software that I know of will correctly calculate the Kriging weights for samples that are a shorter length. What must be done is to use the correct block descritization. In the case of a 10 ft high block and 5 ft samples, the vertical descritization must be two!

Santa Fe's worries about sub-blocking revolve about a 'change of support'. The purpose of Kriging is to make optimal estimates of the grade of each block. A block that is on the edge of an ore zone should correctly model the geometry of the zone. That is why sub-blocks are used. We are not violating any principle of geostatistics by keeping and using on a portion of a block. Assume the original kriged block is say 25'x25'x10' but only 25'x12'x10' of the block is in the zone. If we use the same composites to estimate the full block, and then use them again to krige only the partial block, the kriged estimates will be very similar. The kriging variance will be almost the same in each case, because the main determinate of the kriging variance is the samples and their locations. In each case the same samples are used, hence the kriging variance will be nearly identical.

Santa Fe also makes the assumption that if the block size should change, a new size composite should be computed. This assumption is not true.



Post-it® Fax Note	7671	Date 9/18 # of pages ▶ 4
To Steve R	. 6	From Charlie
Co./Dept.		Co.
Phone #		Phone #
Fax #		Fax #

Robin Hendrickson SFPG Reno Exploration Office 250 South Rock Blvd. Suite 100 Reno Nv. 89502

Sept. 16, 1996

Dear Robin:

We have reviewed your comments of September 4, 1996 and asked both Peter Knudsen and Steve Ristorcelli to review and comment on the same. Both of these gentlemen have been significantly involved in the Rosebud Mineral Resource estimation process. Charlie Muerhoff has summarized and consolidated those comments and our response.

Hecla, as well as many other mining companies, has experienced the ill effects of mineral resource models which give little attention to the geologic features which control mineralization. There are numerous examples of "reserve busts" resulting from mathematical models which don't attempt to represent controlling geologic features. Accurately interpreting and modeling the geologic controls has been a main focus of the delineation drilling and modeling employed at the Rosebud Project from the outset. Numerous in-house and outside experts have been involved in this program since inception. These techniques are not new in the broad sense but have been advanced to the needs of this particular ore body and underground mining methods. The model and techniques have been audited formally by two consulting firms one of which specializes in performing audits for financial institutions for the purposes of project financing and valuation.

Throughout this entire process the Rosebud Staff has been very open to constructive criticism and the model has significantly improved through the efforts, talents, and experience of the vast resource of people which have been a part of this effort. In continuing this process we are making a change in response to one of your suggestions and have supplied comments to the remainder as attachments to this letter.

Sincerely,

Ronald W. Clayton

Rosebud Project General Mgr.

cc: George Johnson

Ron Parrat

HECLA MINING COMPANY ROSEBUD PROJECT

September 16, 1996

Memorandum to:

Ron Clayton

From:

Charlie Muerhoff Charles

RE:

Response to SFPG Letter Regarding Rosebud Project Modeling,

Dated 9/4/96

This memorandum is intended to address the conclusions and recommendations included in the letter sent to you by Skip McIntosh, SFPG regarding Rosebud Project Modeling, dated September 4, 1996. The letter was forwarded to Pete Knudsen and Steve Ristorcelli for their review; their comments have been incorporated into my response.

1. SFPG: The modeling strategy currently being adopted (sub-blocking, assay based variograms and assay based interpolation) for the Rosebud model will most likely lead to an overestimation of the grade and ounces when applying a cutoff grade for mining.

Response: The use of assay data in geostatistics and for block estimation (regardless of the method) is acceptable as long as each sample has the same support, i.e., length. To resolve this problem, we will weight-average downhole assays to five-foot composites within gold domains. Since this will undoubtedly result in composites less than five-feet in length occurring at the margin of the domains, Pete Knudsen recommends using the composites which are at least one-half the length of the other samples (i.e., at least 2½ feet) and discarding those samples which are less than one-half the length of the other samples. Subblocking is addressed in item 3 below.

In their examination of the data, SFPG uses the global population of South Zone drill samples rather than samples from the mineralized zone. Sample data from surface drill holes which include up to 600 feet of unmineralized rock has been included in their analysis. This affects the perceived bias to higher grades in the shorter assay intervals and unfairly accentuates this relationship. Steve Ristorcelli examined the relationship between shorter assay intervals and grades on a domain by domain basis and found the bias to be very minimal. In fact, in some of the higher grade zones, samples that are shorter than five feet actually have a lower average grade, rather than higher.

SFPG: This is the problem which Lauren Roberts has described as being his experience at other operations i.e., the model has predicted more ounces than mining demonstrated.

Response: I believe Lauren's comments have been taken out of context. This particular methodology has not been used at any of Hecla's operations until Rosebud. I used a very simplified version when modeling the GP Blanket at Republic and the model compared favorably to actual production, with an overall tonnage variance of -8% and gold ounce variance of +4% as compared to the actual tonnage and ounces produced.

SFPG: The best way to eliminate the problems of changing support variograms and block sizes is to focus on "internal dilution" or the Volume Variance: change in support issues.

Response: As stated above, we will composite the data to five-foot sample lengths, negating the change in support issue. Block size is addressed in item 3 below.

2. Composites should be used in the interpolation process. Grades should be estimated by Kriging, Inverse Distance power (...) and Nearest Neighbor methods. All three methods should be evaluated as a basis for mine planning.

Response: Ten-foot composites were used in previous resource calculations, and we will use five-foot composites for the current model. Surpac (and MEDS) will correctly calculate the Kriging weights for sample composites that are shorter than the size of the block. As far as the estimation method is concerned: just as we did for the 1995 Mineral Inventory, several estimation methods will be used as to evaluate the current model. For the 1995 model, six different iterations of the resource estimate were generated by Kriging, nearest neighbor, and manual polygonal methods. The Kriged model was selected for inclusion in the 1995 RMI and was used for the feasibility mine planning.

3. SFPG: The block size should be held constant at a size equal to the appropriate SMU for an underground mining project.

Response: In general, I do not agree with this argument. Given the proper understanding of the deposit, combined with the ability to mine at highly variable widths and heights, block sizes should not be held constant for an underground mining situation. The block size should take into account the differing styles and geometry of the mineralization within a given deposit and the differing mining methods to be employed for the most efficient extraction.

In regards to the current model, we are not planning to use sub-blocking (yet), but we are using partial blocks at the individual domain boundaries. The resultant whole block will receive the weighted average grade of those partial blocks which comprise it. Sub-blocking or partial blocking is for geometry purposes only and change of support is not an issue. Pete Knudsen described this to me as follows: "The purpose of Kriging is to make optimal estimates of the grade of each block. A block that is on the edge of an ore zone should correctly model the geometry of the zone. That is why sub-blocks are used. We are not violating any principle of geostatistics by keeping and using only a portion of a block. Assume the original kriged block is say 25'x25'x10' but only 25'x12'x10' of the block is in the zone. If we use the same composites to estimate the full block, and then use them again to krige only the partial block, the kriged estimates will be very similar. The kriging variance will be almost the same in each case, because the main determinate of the kriging variance is the samples and their locations. In each case the same samples are used, hence the kriging variance will be nearly identical."

4. SFPG: Simplify the interpolation strategy minimum number of statistically supported mineral domains within 4 area domains instead of 19 different domains. Let the modeling define the grade distribution boundaries rather than trying to visually estimate them from the assays. There are inherent errors in the assays which could lead to bias in the grade zoning.

Response: We are currently using four area domains, with each subdivided into four or five grade population domains (total of 19 domains). The grade population domains are individually modeled to reflect their respective occurrences as they relate to style of mineralization and geologic control or their spatial relationship to particular stratigraphic units. If grade population boundaries coincide with recognizable geologic boundaries and controls, why let these boundaries be defined by geostatistics where grades will smear across their respective geologic boundary? GEOLOGY MUST BE HONORED. Our approach all along has been to model the grade populations (low-grade as well as high-grade) to the geology. The result is often sharp contrasts in grade at boundaries between high-grade and low-grade

mineralization (the use of partial block composites at domain boundaries actually create a 'transitional' grade boundary over a block width), but this approach is applicable to the observed distribution and occurrence of mineralization in the Rosebud Deposit.

As you are aware, it has always been our intention to perform several estimations of the model using different types of methods, just as we did for the 1995 RMI model. We will include a model where the grade domain boundaries internal to the area domains will be disregarded.

As far as 'inherent errors in the assays' is concerned, I don't understand this statement. Any error that is inherent to the assays would also be included in the subsequent composite. Given the sample protocol used for core, and the minimal variance found in original assays vs. check assays vs. metallic screen assays vs. CN bottle roll results, I don't believe there are inherent errors in the core sample assays. In regards to LAC's reverse-circulation drilling, we have identified some downhole smearing, especially where high inflows of water were encountered. This has been taken into account when modeling the grade domains (assays from several holes were either restricted or eliminated completely based on conflicting data from nearby core holes).

5. SFPG: The highly clustered spatial distribution of drilling samples and the high grade outliers in the distribution of values in the South Zone raises the problem of different local mean values within the densely drilled zones compared with the distal (lower grade zones). This condition would render the assumption of stationarity of the mean invalid. Hecla does not decluster the data before calculating variograms. The effect of clustering and non stationarity may be minimized by calculating the variogram using a method which reduces the effect of the local mean on the variogram curve. These methods include calculating a relative variogram, or using either the covariance or correlogram function to characterize the spatial continuity of the mineralization.

Response: One of the reasons the grade domain methodology was chosen was because of the observed radical changes in local means. Again, instead of smoothing data, we chose to model the variability of grades by separating recognized grade populations and modeling them individually. The use of grade domains takes the change in local means into account; there is a stationarity of the mean within each grade domain.

Pete Knudsen did use correlograms and converted them to variograms.

Let me know if you have any questions.

enclosures: Pete Knudsen correspondence

Steve Ristorcelli correspondence & statistical analysis

Indicator Kriging Model of the the Rosebud Deposit

by

H. Peter Knudsen, Ph.D., P.E.

January 6, 1997

Prepared for

Mine Development Associates.

1.0 Introduction

Mine Development Associates contracted H. Peter Knudsen to develop a indicator krigingin model of the Rosebud Deposit. Work performed includes calculation of basic statistics, calculation and modeling of indicator variograms, and indicator kriging for four geologic/mineralogic zones of the deposit.

2.0 Data

The basic data used in this analysis consisted of 5ft composites prepared by Mine Development Associates. The data was grouped by MDA into four zones. Each zone was analyzed independently.

2.1 Zone 1

All data in zone 1 were grouped together. Indicator cutoffs were chosen based on the likely economic cutoffs and the need to retain definition in the high grade tail of the distribution. The cutoffs chosen are listed below.

Number	Cutoff Value	Cumulative Percent
1	0.05	63.7%
2	0.10	74.4%
3	0.15	80.0%
4	0.25	85.3%
5	0.40	89.2%
6	0.60	92.8%
7	1.00	95.9%
8	2.00	98.3%
9	3.00	99.3%
10	10.00	99.99%

Indicator variograms were calculated and modeled for each indicator cutoff. In general the variograms were well behaved and fairly easy to model. Anistropy was found in the lower cutoffs but as the cutoff increased the anisotropy became less apparent. The anistropy ellipsoid in oriented with the major axis at N5E with a dip of 30 degrees.

The variogram parameters for the grouped data from 12 to 15 are listed below. A nested spherical model was used as the variogram model.

Variogram Parameters for Zone 1

#	Со	C1	R1	C2	R2	Bearing	Dip	Tilt	Major AF	Minor AF	
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1	0.2	.45	30'	.35	150.'	5	0	30	1.5	1.5
2	0.2	.45	30'	.35	150.'	5	0	30	1.5	1.5
3	0.2	.4	30'	.4	150.'	5	0	30	1.5	1.5
4	0.2	.4	30'	.4	150.'	5	0	30	1.5	1.5
5	0.2	.4	30'	.4	150.'	5	0	30	1.5	1.5
6	0.25	.5	30'	.25	100'	5	0	30	1.0	1.0
7	0.5	.35	20'	.15	120'	5	0	30	1.0	1.5
8	0.6	.25	10'	.15	100'	5	0	30	1.0	1.0
9	0.6	.4	25'	0	0	5	0	30	1.0	1.5
10	1.0	0	0	0	0	0	0	0	1.0	1.0

The variogram for the 0.05opt cutoff is shown in Figure 1.

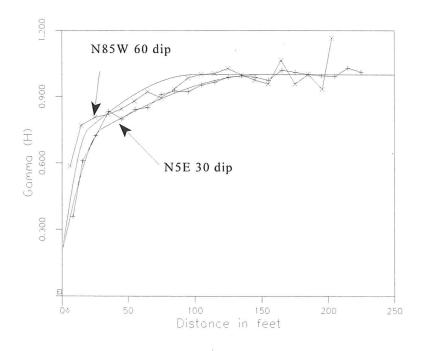


Figure 1. Zone 1 variograms for 0.05 opt cutoff.

2.2 Zone 2

For consistency in the modeling the same cutoffs were used for all zones. All the data from Zone 2 (21,22,23,24,and 25) were used. The zone 2 variograms are similar to zone 1, except the ansistropy between the plane of the structure and perpendicular to it is much stronger than in

Zone 1.

Variogram Parameters for Zone 2

#	Со	C1	R1	C2	R2	Bearing	Dip	Tilt	Major AF	Minor AF
1	0.4	.20	40'	.40	167.'	5	0	30	1.0	3
2	0.4	.20	30'	.40	167.'	5	0	30	1.0	3
3	0.2	.4	30'	.4	140.'	5	0	30	1.0	3.75
4	0.2	.45	25'	.35	150.'	5	0	30	1.25	5
5	0.2	.55	25'	.25	140.'	5	0	30	1.20	4.66
6	0.4	.4	15'	.20	100'	5	0	30	1.0	4.0
7	0.4	.4	15'	.20	100'	5	0	30	1.0	4.0
8	0.8	.20	30'	0	0	5	0	30	1.0	1.0
9	1.0	0	0	0	0	5	0	30	1.0	1.0
10	1.0	0	0	0	0	0	0	0	1.0	1.0

Figure 2 shows the variogram for the 0.05 cutoff.

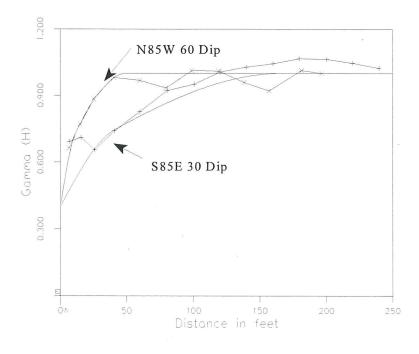


Figure 2. Zone 2 variogram for 0.05 opt cutoff.

2.3 Zone 3

The same cutoffs were used in zone 3 as in zones 1 and 2, with the exception that the highest cutoff used was 2.00 opt. The mineralization in zone 3 has a strong vertical continuity.

Variogram Parameters for Zone 3

#	Co	C1	R1	C2	R2	Bearing	Dip	Tilt	Major AF	Minor AF
1	0.4	.25	30'	.35	120.'	0	90	0	1.33	1
2	0.4	.25	30'	.35	120.'	0	90	0	1.33	1
3	0.3	.7	130	0	0	0	90	0	2.0	1
4	0.3	.7	130	0	0	0	90	0	2.0	1
5	0.3	.7	130	0	0	0	90	0	2.0	1
6	0.3	.6	115	0	0	0	90	0	2.0	1.0
7	0.7	.3	60'	0	0	0	90	0	2.0	1.0
8	0.8	.20	30'	0	0	0	90	0	1.0	1.0

The zone 3 variogram for cutoff 0.05 opt is shown below.

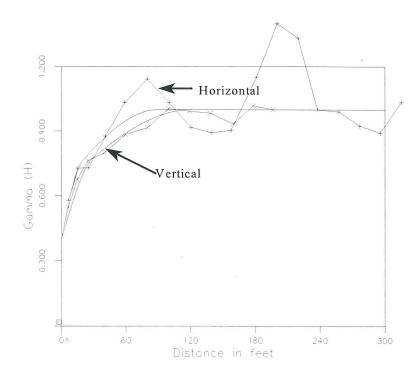


Figure 3. Zone 3 variogram for 0.05 opt cutoff.

2.4 Zone 4

The cutoffs used in zone 4 are different than in the other zones, because there are fewer high values in this zone.

Number	Cutoff Value	Cumulative Percent
1	0.025	63.7%
2	0.050	77.2%
3	0.100	83.1%
4	0.150	88.4%
5	0.250	93.3%
6	0.500	98.5%

Variogram Parameters for Zone 4

#	^e Co	C1	R1	Bearing	Dip	Tilt	Major AF	Minor AF
1	0.4	.60	160'	0	0	0	1.0	2.66
2	0.4	.60	80'	0	0	0	1.0	2.66
3	0.4	.60	80'	0	0	0	1.0	2.66
4	0.4	.60	80'	0	0	0	1.0	2.66
5	0.4	.60	80'	0	0	0	1.0	2.66
6	1.0	0	0	0	0	0	1.0	1.0

The zone 4 variogram for cutoff 0.025 opt is shown below.

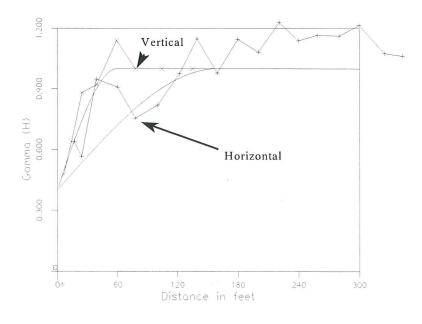


Figure 4. Zone 4 variograms for 0.025 opt cutoff.

3.0 Search Parameters Used

The maximum search radius used in all kriging runs was 150 ft and the vertical search distance was limited to 60 ft. The maximum number of samples used per block was 30 and the minimum used was 10.

Charlie 623-6967

facsimile TRANSMITTAL

to:

Steve Ristorcelli

fax#:

702-856-6053

re:

Geostat comments

date:

September 13, 1996

pages:

3, including this cover sheet.

Steve

Here are my comments about the questions raised by Santa Fe.

Thanks

From the desk of.

H. Peter Knudserr Professor and Head, Mining Department Montana Tach 1300 West Park St. Butte, MT 59701 USA

> 1-406-496-4395 Fax: 1-406-496-4133

School of Mines Montana Tech Memorandum

September 13, 1996

To:

Charlie Muerhoff, Steve Ristorcelli

From:

Pete Knudsen . Dean

Re:

Geostat questions

5/12

Concerns expressed by Santa Fe

1. Use of assay data violates Santa Fe's standard practices Comment:

It is important that all samples have the same support, ie., length. It is acceptable to use assay data as long as they have the same lengths. There is always some samples that will have shorter lengths, usually at the end of the hole. These can be ignored if they are very small, or used in the analysis if they are at least one half the length of the other samples. What must be avoided is the use of short samples that were expressly taken to sample a high grade structure. This will lead to a bias.

The resolution to this problem is to composite use down-the-hole composites of 5 feet length.

2. A relative variogram or correlogram may be more appropriate.

Comment:

Correlograms were calculated and converted to variograms.

3. Block Size. Santa Fe seems to worry that the sub - blocking ability of SURPAC2 will change the "variance". Also, Santa Fe seems to feel the composite length must be the same as the block height.

Comment;

Kriging can be done with composites that are a different size than the block. Most software is not written for the case of the composites being longer than the block, but all of the software that I know of will correctly calculate the Kriging weights for samples that are a shorter length. What must be done is to use the correct block descritization. In the case of a 10 ft high block and 5 ft samples, the vertical descritization must be two

inside the blode, you can astract any to pte stimuling two layers

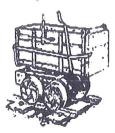
Santa Fe's worries about sub-blocking revolve about a 'change of support'. The purpose of Kriging is to make optimal estimates of the grade of each block. A block that is on the edge of an ore zone should correctly model the geometry of the zone. That is why sub-blocks are used. We are not violating any principle of geostatistics by keeping and using on a portion of a block. Assume the original kriged block is say 25'x25'x10' but only 25'x12'x10' of the block is in the zone. If we use the same composites to estimate the full block, and then use them again to krige only the partial block, the kriged estimates will be very similar. The kriging variance will be almost the same in each case, because the main determinate of the kriging variance is the samples and their locations. In each case the same samples are used, hence the kriging variance will be nearly identical.

Santa Fe also makes the assumption that if the block size should change, a new size composite should be computed. This assumption is not true.

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Maltin 1:00-7:00

182.3



MINE DEVELOPMENT ASSOCIATES

MINE ENGINEERING SERVICES SURPAC MINING SYSTEMS

DATE: September 11, 1996

TO: Charlie

FAX: 702-623-6967 FROM: Steven Ristorcelli

THIS TRANSMISSION CONSISTS OF __17 PAGES INCLUDING THIS COVER PAGE.

IF ALL PAGES ARE NOT RECEIVED, PHONE (702) 856-5700.

FAX NUMBER: (702) 856-6053

Charlie.

This fax is to paraphrase the conversation w/ Pete K. today and give you some more "support" data. Basically, the only valid point Santa Fe has is the estimation from variable length samples.

- lf there is a bias in the data, then there will be a bias in the kriging. The weighted averages by zone did not change significantly based on the fax I sent to you this morning. I am sending several sheets on the zones showing the statistics of all samples less than 2.5 ft in length (the point at which Pete K. starts to get concerned). I have looked at them and found that they are not terribly different from the stats of the corresponding zones in total. Don't forget, once we move out and cut the outliers it will result in lower means. As we stated, send Pete both files (assay and composite down hole by rock type) and he will be the judge as to whether we should use 5 ft composites or assays. Consider compositing to 5 ft just to avoid having to constantly deal with these sorts of headaches. I don't feel it will materially affect the outcome, just the perception. And finally, there is no reason to work with 10 ft composites over 5 ft composites. Kriging will put valid grades in 10 ft blocks from 5 ft samples.
- 2. Pete used correlograms.
- 3. The comment on sub-blocking by Santa Fe is not applicable and therefore does not warrant a comment. However, Santa Fe's note on this is nonsense. Sub-blocking is for geometry only.
- 4. On his comment no. 5 in the Conclusions, Pete just shrugged it off as nonsense. I have asked him to comment on it in writing for you or to call you today. My comments are: kriging takes into account and compensates for clustered data. Second, we used zones because there is a radical change in local means. The zoning takes this into account and therefore in all our estimation domains we do have "stationarity of mean". And of coarse, the second half of this paragraph is also moot because we used the correlogram.

	STAT. BASIC STATS	Descriptive by ZONE: G	Statistics	(all9999)	.stal		***************************************	,	
	Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sum	Minimum	. Maximum	Range
	AUAVG2 AGAVG LENGTH	67 67 67	.064701 2.535821 1.770149	021620 509497 1.624600	.151023 5.581139 1.915699	4.3350 169.9000 118.6000	0.000000 0.000000 .30000	2.90700 75.05000 2.50000	2.90700 75.05000 2.20000
ICI	MT 511		0.019						
!	STAT. BASIC STATS	Descriptive by ZONE: G_	Statistics 1:11	(all9999.	sta;				
1	Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtesis	
	AUAVG2 AGAVG LENGTH	.1252 155.8739 .3561	.35389 12.48495 .59671	.043235 1.525279 .072900	8.088548 5.624617 769735	.292836 .292836 .292836	65.90396 30.71450 22525	.577996 .577996 .577996	

211 total An 0.019 0.679 Ag Q:35 2.75 Length 4.78 1.07

STAT. BASIC STATS	•	Descriptive Statistics (all9999.sta) by ZONE: G_2:12									
Variable	Valid N	Mean	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum.	Range			
AUAVG2 AGAVG LENGTH	30 30 30	.134600 1.573667 : 1.886667	.074664 .279591 1.705125	.194536 2.367743 2.368208	4.03800 47.21000 56.60000	C.000000 C.000000 .600000	.80700 14.63000 2.50000	.80700 14.63000 1.90000			

STAT. BASIC STATS		Descriptive Statistics (all9999.sta) by ZONE: G_2:12							
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis		
AUAVG2 AGAVG LENGTH	.02576 12.01038 .23637	.160511 3.465599 .4861??	.029305 .632729 .088763	2.788296 3.105729 798526	.426892 .426892 .426892	10.20313 9.25076 .45625	.832746 .832746 .832746		

STAT.

STAT. BASIC STATS	Descriptive Statistics (al19999.sta) by ZONE: G_3:13							
Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sun	Minimum	Maximum	Range
AUAVG2 AGAVG LENGTE	22 22 22	.652545 5.195000 1.677273	.005558 1.032625 1.332494	1.299533 9.357375 2.022051	14.3560 114.2900 36.9000	.004000 .040000 .200000	7.08500 33.14000 2.50000	7.08100 33.10000 2.30000

	STAT. Descriptive Statistics (all9999.sta) BASIC by ZONE: G_3:13 STATS									
4	Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis		
-	AUAVG2 AGAVG LENGTH	2.12936 88.13321 .60470	1.459233 9.387929 .777623	.311110 2.001513 .165790	4.456865 2.260857 599855	.490962 .490962 .490962	20.47442 4.17403 -1.09765	.952780 .952780 .952780		

213 0.409 0.503 4.36 8.05 4.65 1.16

STAT. BASIC STATS	Descriptive by ZONE: G	Descriptive Statistics (all9999.sta) by ZONE: G_4:14									
Variable	Valid N	Mear	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range			
AUAVG2 AGAVG LENGTH	14 14 14	1.086714 6.994286 1.471429	.512210 099181 1.085482	1.66122 14.08775 1.85737	15.21400 97.92000 20.60000	.013000 .160000	2.65500 42.97000 2.50090	2.64200 42.81000 2.10000			

STAT. BASIC STATS	Descriptive Statist by ZONE: G_4:14	ics (all9999.	sta)			
Variable	Variance : Std.Dev	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis
AUAVG2 AGAVG LENGTH	.9901 .99503 150.9348 12.28555 .4468 .66844	3.283452	.475894 2.455401 .132272	.597380 .597380 .597380	-1.62392 5.81033 -1.03856	1.15405C 1.15405C 1.154C50

2 14 1.202 0.918 7.44 12.57 4.37 1.16

Ī	STAT.	Descriptive Statistics	(all9999.sta)
*	BASIC	by ZONE: G 5:15	
:	STATS	_	

Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
AUAVG2	3	19.34133	-41.6631	80.34579	58.02400	2.975000	47.57900	44.60400
AGAVG	3	22.56333	-13.7702	58.89682	67.69000	8.770000	37.90000	29.13000
LENGTH	3	1.56667	0874	3.22069	4.70000	1.000000	2.30000	1.30000

STAT. BASIC STATS	Descriptive by ZONE: G	escriptive Statistics (all9999.sta) y ZONE: G_5:15								
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtcsis	Std.Err. Kurtosis			
AUAVG2 AGAVG LENGTH	603.0756 213.9256 .4433	24.55760 14.62620 ! .66583	14.17834 8.44444 .38442	1.666996 .469546 1.055832	1.224745 1.224745 1.224745	 	 			

Z 15 7.292 10.178 15.08 13.07 4.35

STAT. BASIC STATS	Descriptive by ZONE: G	Descriptive Statistics (all9999.sta) by ZONE: G_6:21									
Variable	Valid N	Mear.	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range			
AUAVG2 AGAVG LENGTH	40 40 40	.014575 .456000 1.785000	.007683 058947 1.609150	.021467 .970947 1.960850	.58300 18.24000 71.40000	0.000000	.114000 7.950000 2.500000	.114000 7.950000 1.900000			

STAT. Descriptive Statistics (all9999.sta) BASIC by ZONE: G_6:21 STATS										
Variable	! Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis			
AUAVG2 AGAVG LENGTH	.000464 2.592542 .302333	.021549 1.610137 .549848	.003407 .254585 .086939	2.973792 4.319718 573342	.373783 .373783 .373783	11.20121 17.77601 81862	.732600 .732600 .732600			

STAT. BASIC STATS		Descriptive Statistics (all9999.sta) by ZONE: G_7:22									
Variable	Valid N	Mean	Confid. -95.000%	Confid. 95.000	Sun	Minimum	Maximum	Range			
AUAVG2 AGAVG LENGTH	17 17 17	.163529 2.248824 1.935294	.055634 932085 1.632783	.271425 5.429732 2.237805	2.78000 38.23000 32.90000	.001000 .040000 .600000	.82200 25.94000 2.50000	.82100 25.90000 1.90000			

STAT. BASIC STATS	Descriptive Statistics (all9999.sta) by ZONE: G_7:22								
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis		
AUAVG2 AGAVG LENGTH	.04404 38.27528 .34618	.209852 6.186701 .588368	.050897 1.500496 .142700	2.25489 3.94781 -1.05138	.549747 .549747 .549747	5.65850 15.93977 .09321	1.063198 1.063198 1.063198		

222 0.100 0.119 0.715 1.701 5.00

STAT. BASIC STATS	Description by ZONE: G							
Variable	Valid N	Mean	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range
AUAVG2 AGAVG LENGTH	11 11 11	.512091 1.232727 1.581818	.116777 .394708 1.074775	.907405 2.070746 2.088861	5.63300 13.56000 17.40000	.003000	2.055000 4.4400C0 2.40000	2.052000 4.380000 2.200000

STAT. Descriptive Statistics (all9999.sta) BASIC by ZONE: G_8:23 STATS										
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis			
AUAVG2 AGAVG LENGTH	.346252 1.556022 .569636	.588432 1.247406 .754743	.177419 .376107 .227563	2.012456 1.883283 932233	.660687 .660687 .660687	4.789305 4.160826 .C43244	1.279416 1.279416 1.279416			

Z 23 0.364 0.453 1.86 3.59 4.68

STAT. BASIC STATS		escriptive Statistics (all9999.sta) y ZONE: G_9:24									
Variable	Valid N	Mear.	Confid95.000%	Confid. 95.000	Som	Minimum	Maximum	Range			
AUAVG2 AGAVG LENGTH	2 2 2	.572000 .640000 2.000000	-5.52698 63062	6.670979 1.910620	1.144000 1.280000 4.000000	.092000 .540000 2.000000	1.052000 .740000 2.000000	.960000			

STAT. BASIC STATS	Descriptive by ZONE: G	Descriptive Statistics (all9999.sta) by ZONE: G_9:24										
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis					
AUAVG2 AGAVG LENGTH	.460800 .020000 0.000000	.678823 .141421 C.COOCOO	.480000 .100300 0.000000									

Z 24 1.260 0.992 3.561 4.046 4.778

STAT. BASIC STATS		escriptive Statistics (all9999.sta) ZONE: G_10:31										
Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range				
AUAVG2 AGAVG LENGTH	14 14 14	.024286 .150714 1.850000	.010981 .035227 1.581322	.037590 .266201 2.118678	.34000 2.11000 25.90000	.001000 .030000 .900000	.07300C .77000C 2.50000C	.072000 .740000 1.600000				

STAT. BASIC STATS	Descriptive by ZONE: G	e Statistics _10:31	s (all9999.	sta;			
Variable	Varíance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis
AUAVG2 AGAVG LENGTH	.000531 .040007 .216538	.023043 .200018 .465337	.006159 .053457 .124367	.882547 2.731652 863027	.597380 .597380 .597380	229038 7.714764 .506188	1.154050 1.154050 1.154050

STAT. BASIC STATS	Descriptive by ZONE: G	Statistics _11:32	s 'all9999.	all9999.sta)						
Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range		
AUAVG2 AGAVG LENGTH	5 5 5	.080200 .212000 1.660000	.023331 .113681 .757762	.137069 .310319 2.562238	.401000 1.060000 8.300000	.029000 .140000 .800000	.147000 .340000 2.500000	.118000 .200000 1.700000		

STAT. BASIC STATS		Descriptive Statistics (all9999.sta) by ZONE: G_11:32										
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis					
AUAVG2 AGAVG LENGTH	.002098 .006270 .528000	.045801 .079183 .726636	.020483 .035412 .324962	.688155 1.324727 273938	.912871 .912871 .912871	2059C 1.63298 -2.3444C	2.000000 2.000000 2.000000					

Z 32 0.015 0.063 0.471 1.444 4.767

STAT. BASIC STATS	p representative	criptive Statistics (all9999.sta) ZONE: G_12:33									
Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sun	Minimum	Maximum :	Range			
AUAVG2 AGAVG LENGTH	2 2 2	.447000 .695000 1.600000	-1.10316 89328 -3.48249	1.997157 2.283276 6.682482	.894C00 1.390C00 3.200C0	.325000 .570000	.569000 .820000 2.000000	.244000 .250000 .800000			

STAT. BASIC STATS	ASIC by ZONE: G_12:33										
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis				
AUAVG2 AGAVG LENGTH	.029768 .031250 .320000	.172534 .176777 .565685	.122000 .125000 .400000	 		——————————————————————————————————————					

STAT. Descriptive Statistics Gall9999.sta; BASIC by ZONE: G_13:34

Variable	Valid N	Mean	Confid95.000%	Confid. 95.000	Sun	Minimum	Maximum.	Range
AUAVG2	1	1.753000			1.753000	1.753000	1.753000	
AGAVG	1	2.440000			2.440000	2.44C00C	2.440000	
LENGTH	1	1.000000			1.000000	1.000000	1.000000	

STAT. BASIC STATS		Descriptive Statistics (all9999.sta) by ZONE: G_13:34										
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis					
AUAVG2 AGAVG LENGTH							 					

234 1.399 1.547 2.95 4.00 4.79

STAT. BASIC STATS	Descriptive Statistics 'all9999.sta' by ZONE: G_14:41									
Variable	Valid N	Mean	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range		
AUAVG2 AGAVG LENGTH	14 14 14	.027643 .205714 1.642857	004257 .068002 1.339259	.059542 .343427 .1.946455	.38700 2.88000 23.00000	0.000000 0.00000 .40000	.218000 .870000 2.500000	.218000 .870000 2.100000		

STAT. Descriptive Statistics (all9999.sta) BASIC by ZONE: G_14:41 STATS										
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis			
AUAVG2 AGAVG LENGTH	.003052 .056888 .276484	.055249 .238512 .525817	.014766 .063745 .140531	3.632359 2.067220 878563	.597380 .597380 .597380	13.42695 4.29740 1.31034	1.154050 1.154050 1.154050			

Z 41 0.017 0.028 0.18 0.363 4.62

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STAT. BASIC STATS	Descriptive Statistics (all9999.sta) by ZONE: G_15:43									
Variable	Valid N	Mean	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range		
AUAVG2	1	.49200C			.492000	.492000	.492000			
AGAVG	1	.81C00C			.810000	.810000	.810000			
LENGTH	1	1.100000			1.100000	1.100000	1.100000			

STAT. Descriptive Statistics (all9999.sta) BASIC by ZONE: G_15:43 STATS										
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis			
AUAVG2							-			
AGAVG										
LENGTH			i ,							

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STAT. BASIC STATS	Descriptive Statistics (all9999.sta) by ZONE: G_16:44									
Variable	Valid N	Mean	Confid. -95.000%	Confid. 95.000	Sum	Minimum	Maximum	Range		
AUAVG2	1	1.517000			1.517000	1.517000	1.517000			
AGAVG	1 .	3.940000			3.940000	3.94000C	3.940000			
LENGTH	:	2.300000			2.300000	2.300000	2.300000			

STAT. Descriptive Statistics (all9999.sta) BASIC by ZONE: G_16:44 STATS											
Variable	Variance	Std.Dev.	Standard Error	Skewness	Std.Err. Skewness	Kurtosis	Std.Err. Kurtosis				
AUAVG2											
AGAVG	***	***									
LENGTH					,						

facsimile TRANSMI

to:

Charlie Muerhoff

fax #:

702-623-6967

re:

Geostat comments

date:

September 13, 1996

pages:

3, including this cover sheet.

Charlie,

Here are my comments about the questions raised by Santa Fe.

Thanks

From the desk of...

H. Peter Knudsen
Professor and Head, Mining Department Montana Tech

1300 West Park St. Butte, MT 59701 USA

1-406-496-4395 Fex: 1-406-496-4133

School of Mines Montana Tech Memorandum

September 13, 1996

To:

Charlie Muerhoff, Steve Ristorcelli

From:

Pete Knudsen, Dean

Re:

Geostat questions

Concerns expressed by Santa Fe

1. Use of assay data violates Santa Fe's standard practices Comment:

It is important that all samples have the same support, ie., length. It is acceptable to use assay data as long as they have the same lengths. There is always some samples that will have shorter lengths, usually at the end of the hole. These can be ignored if they are very small, or used in the analysis if they are at least one half the length of the other samples. What must be avoided is the use of short samples that were expressly taken to sample a high grade structure. This will lead to a bias.

The resolution to this problem is to composite use down-the-hole composites of 5 feet length.

2. A relative variogram or correlogram may be more appropriate.

Comment:

Correlograms were calculated and converted to variograms.

3. Block Size. Santa Fe seems to worry that the sub - blocking ability of SURPAC2 will change the "variance". Also, Santa Fe seems to feel the composite length must be the same as the block height.

Comment:

Kriging can be done with composites that are a different size than the block. Most software is not written for the case of the composites being longer than the block, but all of the software that I know of will correctly calculate the Kriging weights for samples that are a shorter length. What must be done is to use the correct block descritization. In the case of a 10 ft high block and 5 ft samples, the vertical descritization must be two!

Santa Fe's worries about sub-blocking revolve about a 'change of support'. The purpose of Kriging is to make optimal estimates of the grade of each block. A block that is on the edge of an ore zone should correctly model the geometry of the zone. That is why sub-blocks are used. We are not violating any principle of geostatistics by keeping and using on a portion of a block. Assume the original kriged block is say 25'x25'x10' but only 25'x12'x10' of the block is in the zone. If we use the same composites to estimate the full block, and then use them again to krige only the partial block, the kriged estimates will be very similar. The kriging variance will be almost the same in each case, because the main determinate of the kriging variance is the samples and their locations. In each case the same samples are used, hence the kriging variance will be nearly identical.

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Santa Fe also makes the assumption that if the block size should change, a new size composite should be computed. This assumption is not true.