DISTRICT	Rosehud
DIST_NO	4010
COUNTY If different from written on document	Pershing
TITLE If not obvious	Rosebud Project, Pershing County, Nevada,
AUTHOR	Brewer, N. See list on p28
DATE OF DOC(S)	1991
MULTI_DIST Y / N2	
Additional Dist_Nos:	
QUAD_NAME	Sulphur 72
P_M_C_NAME (mine, claim & company names)	Roschad Mine: Lac Minerals (USA) Inc. Chance: Rosebad Project: Degestrom: Dreamland: Oscar, East Dreamland: North Egypinax: North Rosebad Peale Short Slot: South Ridge: Valley: White Alps: Wild Rose
COMMODITY	gold: silver
If not obvious	
NOTES	Project report; drill hole summarize; assays; gralogy; reserves, drill hole location map; cross section; property map
	NOTE: Scan dividers
Keep docs at about 250 pages i	f no oversized maps attached SS: DP 2/30/08
(for every 1 oversized page (>1) the amount of pages by ~25)	x17) with text reduce
Revised: 1/22/08	SCANNED:

CM W 40208

1990 ANNUAL PROGRESS REPORT ROSEBUD PROJECT PERSHING COUNTY, NEVADA

N. H. Brewer LAC Minerals (USA), Inc. March 1991



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1990 ANNUAL PROGRESS REPORT ROSEBUD PROJECT PERSHING COUNTY, NEVADA

I. Summary:

The Rosebud Project, is located in northern Pershing County, Nevada, and consists of an 8,400 acre claim block covering numerous volcanic-hosted epithermal gold-silver prospects (Figure 1).

In 1989, LAC discovered significant high grade gold mineralization in its third drill hole at Dozer Hill. By year-end 38 holes had delineated a northeast trending high grade mineralized zone some 700 feet long, open to the north. Six other target areas were also drilled for a project total of 28,866 feet in 56 holes.

The 1990 exploration program continued with initial step-out drilling along the trend at Dozer Hill. The first hole of the year, RL-57, was collared 150 feet northeast of the final 1989 intercept, and intersected 130 feet grading 0.216 opt Au, including 35 feet of 0.714 opt Au. With the trend confirmed, definition drilling continued on the Dozer Hill deposit as well as on seven other target areas on the property.

A total of 86,332 feet were drilled in 111 rotary and core holes during the year, bringing LAC's project totals to 115,198 feet in 167 holes. About 75% of this footage (85,241') has been drilled in 112 holes on the Dozer Hill deposit which is now 2,000 feet long, and averages 300 feet wide and 40 feet thick (Figure 6).

A sectional geologic resource was estimated for the Dozer Hill zone using nominal cut-offs of 0.02 and 0.05 opt Au. Results are as follows:

CUT-OFF AU OPT	CATEGORY	TONS	AU OPT	AU OUNCES	AU OPT	OUNCES (CUT)*
0.02	Probable	4,088,017	0.117	477,580	0.105	429,631
0.02	Possible	1,102,786	0.147	162,351	0.133	146,563
TOTALS:		5,190,803	0.123	639,931	0.111	576,194
0.05	Probable	1,591,720	0.236	375,388	0.210	333,942
0.05	Possible	676,659	0.220	148,721	0.194	131,250
TOTALS:		2,268,379	0.231	524,109	0.206	465,192

(* = High grades cut to 1.0 opt Au)

As currently outlined, about 55% of this resource is located on ground controlled by the LAC-Equinox Joint Venture and the remainder is on claims 100% owned by LAC.

A kriged reserve study indicates similar total contained ounces at each cut-off but the stripping ratio is too excessive for an economic open pit. A preliminary undiluted "underground mineable" reserve estimate using the higher cut-off is:

TONS	AU OPT	AU OZS.		AU OZS. (CUT)*	AG OPT	AG OZS.
1,245,350	0.284	354,000	0.248	308,800	3.20	3,985,200

^{*} High grade Au assays cut to 1.0 opt.

The resource is still open in several areas and current drill hole spacing is insufficient to condemn some internal portions of the trend especially in vicinity of RL-159C which intersected 170 feet grading 0.559 opt Au. Encouraging drill intercepts in RL-131C, 142, and especially RL-145 (45 feet of 0.202 opt Au) located southeast of the main trend could represent a mineralized cross-structure or perhaps a separate parallel ore zone.

Preliminary metallurgical tests on four core composites show that acceptable mill recoveries (85-90%) can be expected from the various ore types at Dozer Hill using conventional cyanidation processes.

Exploration drilling on other targets in 1990 resulted in a significant discovery on the Chance Target where the first hole intersected 160 feet averaging 0.043 opt Au. Only one of the subsequent eight holes encountered similar mineralization but good potential remains untested under gravel cover to the west.

Based on the similarities of the Dozer Hill occurrence to several other targets, a better understanding of the exploration model has recently evolved for the Rosebud District. Re-evaluation of the other prospect areas is ongoing and at least four of these have become high priority drill targets for 1991.

Beacon Hill Consultants, Ltd. is currently conducting a prefeasibility study of a possible underground mine scenario at Dozer Hill. Their report is expected on March 15th, and will include a preliminary reserve audit, conceptual mine plan, and a financial analysis.

Approval of the proposed 1991 program is contingent on the outcome of this study. The current proposed budget is \$1,200,000 (\$1,000,000 Net to LAC) to complete 30,000 feet of rotary and 15,000 feet of core drilling. The primary objectives will be:

- 1. increase the "probable" inventory at Dozer Hill to at least 2,000,000 tons at an average grade of 0.25 opt Au.
- 2. discover significant high grade mineralization in at least one other target area on the property.

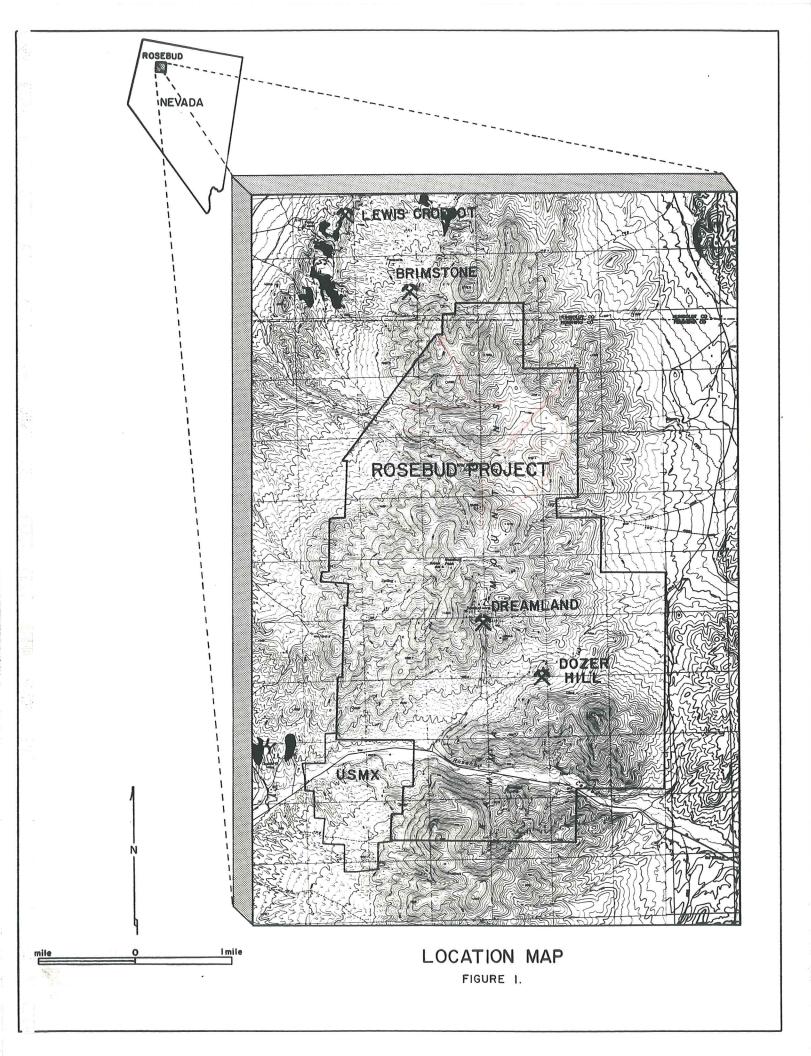
II. Introduction

The Rosebud Project is located in the northern Kamma Mountains, approximately 50 miles north of Lovelock, Pershing County, Nevada (Figure 1). The property covers at least 14 epithermal gold-silver prospects hosted in felsic to intermediate Miocene volcanics.

LAC's involvement in the property resulted from a regional reconnaissance program initiated by R.E. Bennett in 1987. Through various agreements and claim staking since 1988, LAC has been able to consolidate a sizable land position covering most of the prospective ground in the area. Following is a brief history of activity in the Rosebud District:

Table 1. Rosebud History

Table 1. Rose,	
1906 - 1947	Discovery and intermittent production from the Dreamland, Lucky Boy and Brown Palace mines. Recorded district production was 3,700 ozs Au and 116,000 ozs Ag.
Late 70's - Early 80's	Homestake and Asarco exploration. Asarco drilled 4 shallow holes in 1984 in the East Dreamland area. Best intercept was reported to be ~60 feet of 0.05 opt Au.
1984	Equinox Resources staked RB and Wild claims.
1985 - 1986	Freeport acquired land position including Equinox claims and completed 22 holes (9,995'). Best intercept was 30 feet of 0.098 opt Au (RB-9) in the East Dreamland area.
1987	Degerstrom staked GP claims. LAC began reconnaissance in the Kamma Mountains.
1988	LAC optioned Equinox, Degerstrom, Johnson (Dreamland), Bland/Peterson (White Alps-Lucky Boy) claims and began staking Bud claims. Exploration work included mapping, sampling, IP/R surveys, and regional airborne magnetics.
1989	Initial drilling program began in April. LAC's third hole, RL-3, intersected 55 feet of 0.119 opt Au southwest of Dozer Hill. Ongoing target development included detailed mapping, soil sampling, ground magnetics and VLF. Total 1989 drilling: 28,866 feet in 56 holes on 6 target areas.



1990	Continued drilling: 86,332 feet in 111 holes at Dozer Hill and 7 other targets. Geologic resource of +500,000 ozs Au outlined at Dozer Hill. First hole at Chance, RL-113, intersected 160 feet of 0.043 opt Au. Other work included preliminary metallurgical tests, petrography and probe studies, additional ground mag, IP/R, and
	detailed mapping and sampling.

Drilling in 1990 consisted of both reverse circulation rotary and core drilling. Direct drilling costs averaged \$10.30/foot RC and \$19.16/foot core. Following is a breakdown of the drilling by target area:

Target Area	Total Holes	Footage
Dozer Hill Chance E. Dreamland Valley N. Equinox Wild Rose White Alps Degerstrom	74 9 8 6 4 4 4 2	64,410* 5,580 2,705 4,737 2,660 2,040 3,000 1,200
Totals:	111	86,332

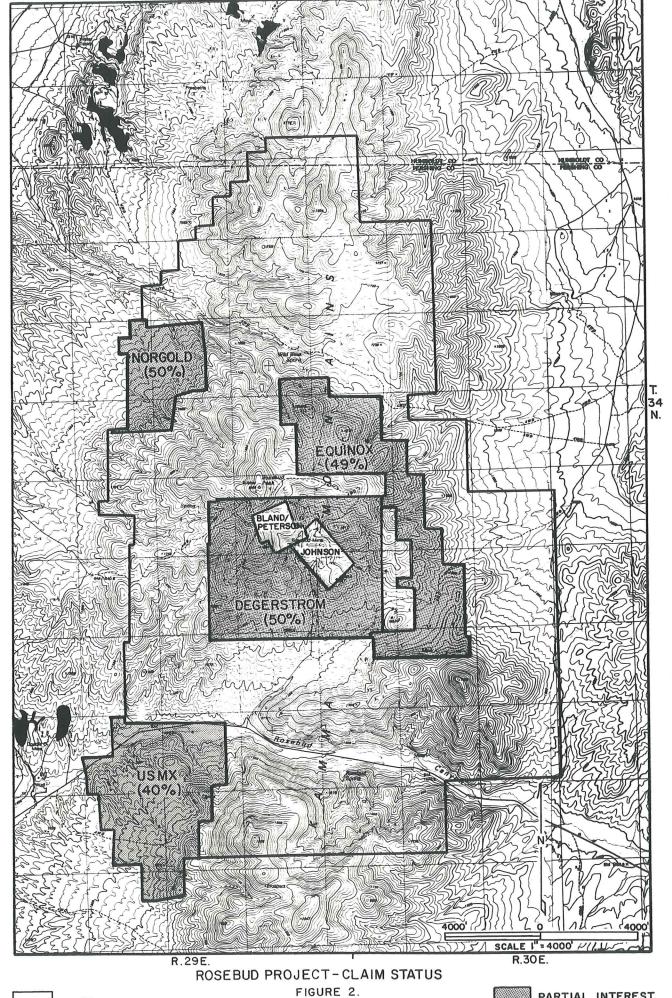
^{*} Includes 42,789 feet of core

Total 1990 project expenditures amount to \$2,117,627. The approved 1990 budget including two supplemental AFE's was \$2,113,000. Net-To-LAC expenditures were \$1,868,473 after JV reimbursements of \$200,000 from Equinox and \$49,154 from Norgold. Since 1988, approximately \$3,294,627 (\$3,045,473 Net-To-LAC) has been spent on the Rosebud Project.

III. Property Status

The Rosebud Property did not change in size substantially during 1990. The total claim block consists of 10 claim groups, 500 unpatented claims, and 3 patented claims covering approximately 8,400 acres on B.L.M. land (Figure 2). Important developments with respect to the various owners or agreements are summarized below.

Equinox: LAC vested with 51% in the JV by July, 1990. Actual expenditures exceeded the earn-in requirement of \$700,000 by approximately \$105,000. Equinox agreed to share \$65,000 of this over-run as an acceptable JV expense. The first JV work plan budget of \$364,000 was approved in August. Actual Plan 1 expenditures (thru January 31, 1991) were about \$315,000. Equinox has made cash contributions of \$200,000 to date. This gives them a credit of \$13,800 which will be applied to their share of the next work plan, approved at \$408,000.



100% LAC

<u>Degerstrom:</u> 1990 expenditures incurred on Degerstrom's GP claims amount to \$258,004. This brings the total LAC expenditures to \$418,542 since the effective date of the agreement, October 28, 1988. The earn-in requirement for 50% is \$500,000 in 4 years.

Norgold: In order to settle a claim conflict between 13 Chance lodes and 12 SS lodes, a 50/50 joint exploration agreement was signed with Norgold Resources on August 15, 1990. This agreement called for a jointly funded expenditure of up to \$100,000 to evaluate the E. Chance area in late 1990. As part of the agreement 2 additional claims, WH 1 and 2, were staked to cover an open fraction and included in the JV area.

Total expenditures amounted to \$98,307. Along with the final report submitted to Norgold on February 13, 1991 (Brewer 1991a), LAC declared its intention to form a joint venture. The minimum work commitment for 1991 is \$50,000 to be funded entirely by LAC.

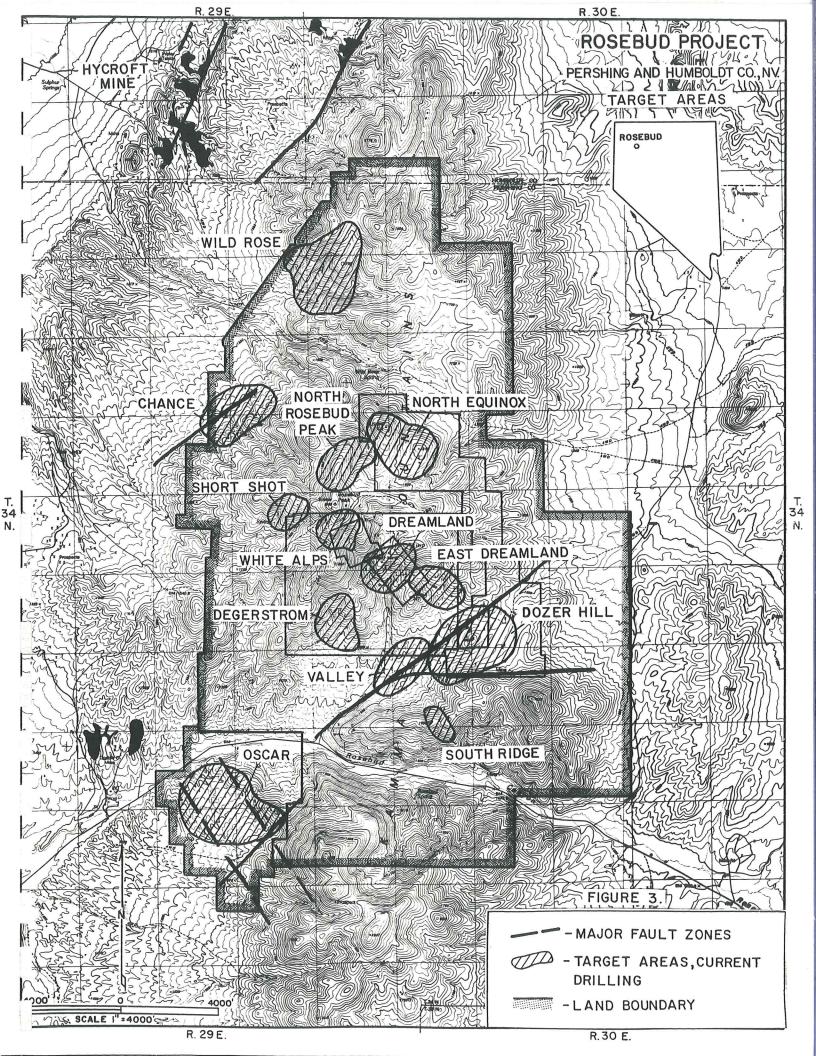
Under the agreement, LAC has a first right of refusal on Norgold's West Chance claims until August 15, 1991. In February, 1991, Bema Gold announced its intention to acquire Norgold Resources.

<u>USMX:</u> In August, 1990, LAC signed a Letter of Intent to lease the Oscar Property from USMX. This property consists of 35 claims adjacent to the southwest boundary of the Rosebud claim block. In anticipation of a signed agreement, LAC spent \$59,360 evaluating the claims in late 1990. To date, negotiations are still proceeding and a final agreement is expected this spring.

Johnson: The option agreement with Johnson on his 4 Dreamland claims was due to expire in July 1991, requiring an \$82,000 purchase payment. This agreement was renegotiated in January, allowing LAC to extend the option period for two more years for higher annual payments of \$10,000. The buy-out price will remain the same.

IV. Geology And Mineralization

The Rosebud property is underlain by Miocene age volcanics which host numerous structurally-controlled epithermal gold-silver prospects (Figure 3). The volcanic stratigraphy consists of a thick series of fine-grained siliceous tuffs intercalated with medium to coarse fragmental units of similar composition and a distinctive marker unit of bedded clay-rich pyroclastic and epiclastic rocks. In the Dozer Hill area, black carbonaceous metasediments of Jurassic-Triassic age have been drilled below the volcanics. Tertiary gravels derived both from the basement and Tertiary volcanic rocks occur locally along the flanks of the Kamma Mountains.



Extensional tectonics have tilted and dissected the range creating a complex pattern of low-angle and high-angle faults. Most of these structures display apparent left-lateral, oblique-slip movement. The most prominent of these structures is the Rosebud Shear Zone which trends N60E across the southern portion of the property and appears to have at least 2000 feet of left-lateral and 500 feet of normal (north side down) displacement.

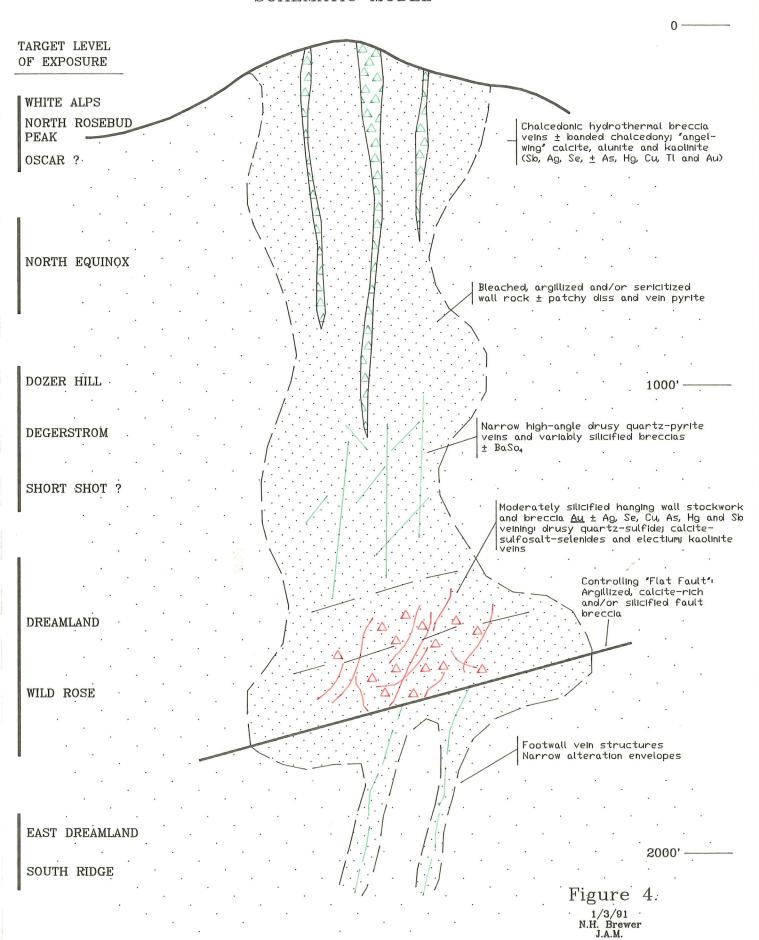
At a prospect scale, low-angle structures are the most important control for significant mineralization. Figure 4 illustrates the currently favored exploration model. Based on the occurrences at Dozer Hill, Dreamland, and Wild Rose, gold-silver mineralization appears to favor the immediate fractured and brecciated hanging wall of a low-angle structure (< 45 degrees), or within the structure itself. Below these structures alteration and mineralization generally dies out quickly except for local narrow and sometimes ore-grade footwall cracks (e.g. South Ridge and East Dreamland). High level expressions of the system include weakly anomalous to barren dense chalcedonic breccias, banded chalcedony veins and "angel wing" silica after calcite. Examples of this are the White Alps knob, North Rosebud Peak, North Equinox structure (Hill 212), and silicified outcrops along the South Ridge and Degerstrom faults.

Host rocks can be any of the fine grained siliceous units with good cracking characteristics such as the Chocolate Tuff at Dreamland, Lower Bud Tuff at Dozer Hill, or the Wild Rose Tuff and Pyroclastics at Wild Rose and Chance. The only obvious poor hosts are bedded Bud lithic lapilli tuff and Badger debris flow breccias. However, the presence of these less permeable lithologies above a favorable structural setting may have enhanced the intensity of alteration and gold grades by acting as an "aquaclude" in some places.

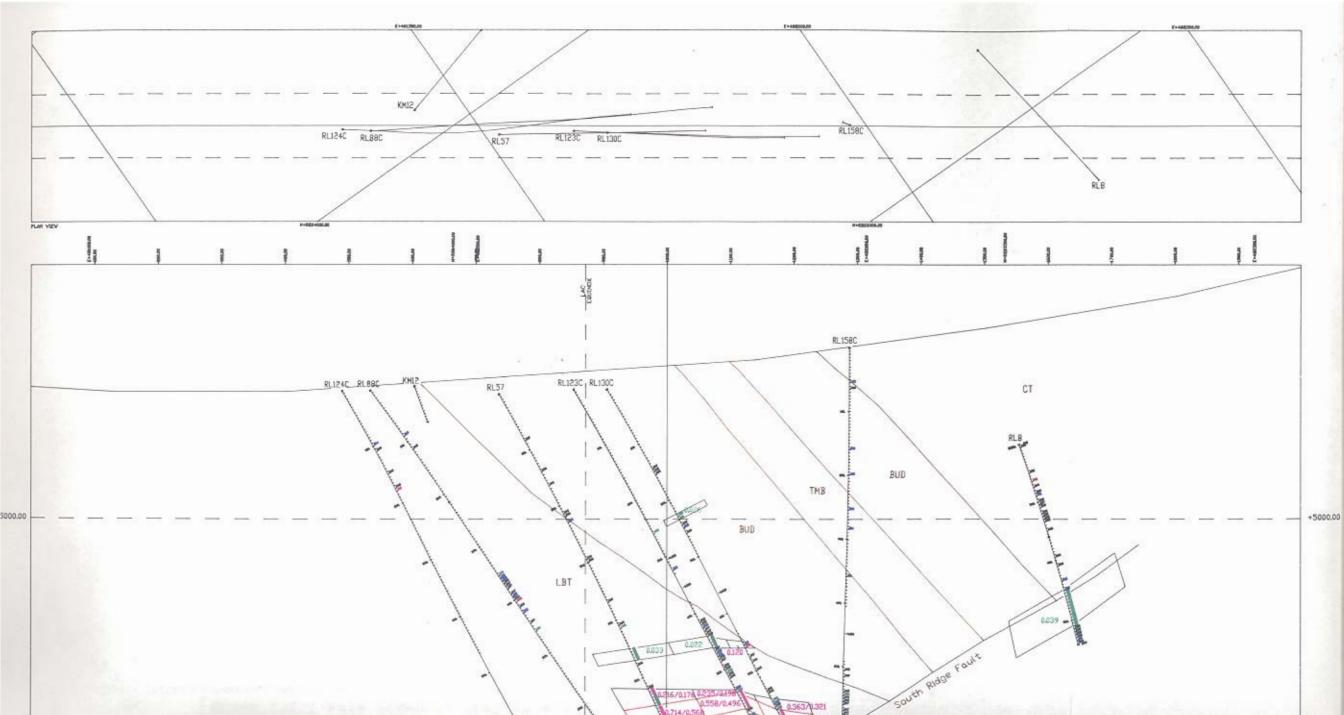
The mineralization at Dozer Hill is mainly confined to the Lower Bud Tuff (LBT) in the hanging wall of the north-dipping low-angle South Ridge Fault (Figure 5). Table 2 summarizes the stratigraphic section as seen in the Dozer Hill area.

The ore is characterized by a crude stockwork of quartz, calcite, clay, pyrite and sulfosalt-bearing veinlets cross-cutting variably bleached and clay-altered (sericitized) tuffs. Gold and silver minerals including electrum, aurian silver, and silver-bearing selenides and sulfosalts are confined to narrow discontinuous veinlets which are generally less than a centimeter in width. One of these selectively assayed from RL-159C contained in excess of 6.0 opt Au and 9.9 opt Ag. Samples of unveined wall rock generally contain little or no precious metals values.

ROSEBUD EPITHERMAL SYSTEM SCHEMATIC MODEL



The following two pages are really one page (Figure 5) you will need to tape them together if need be.



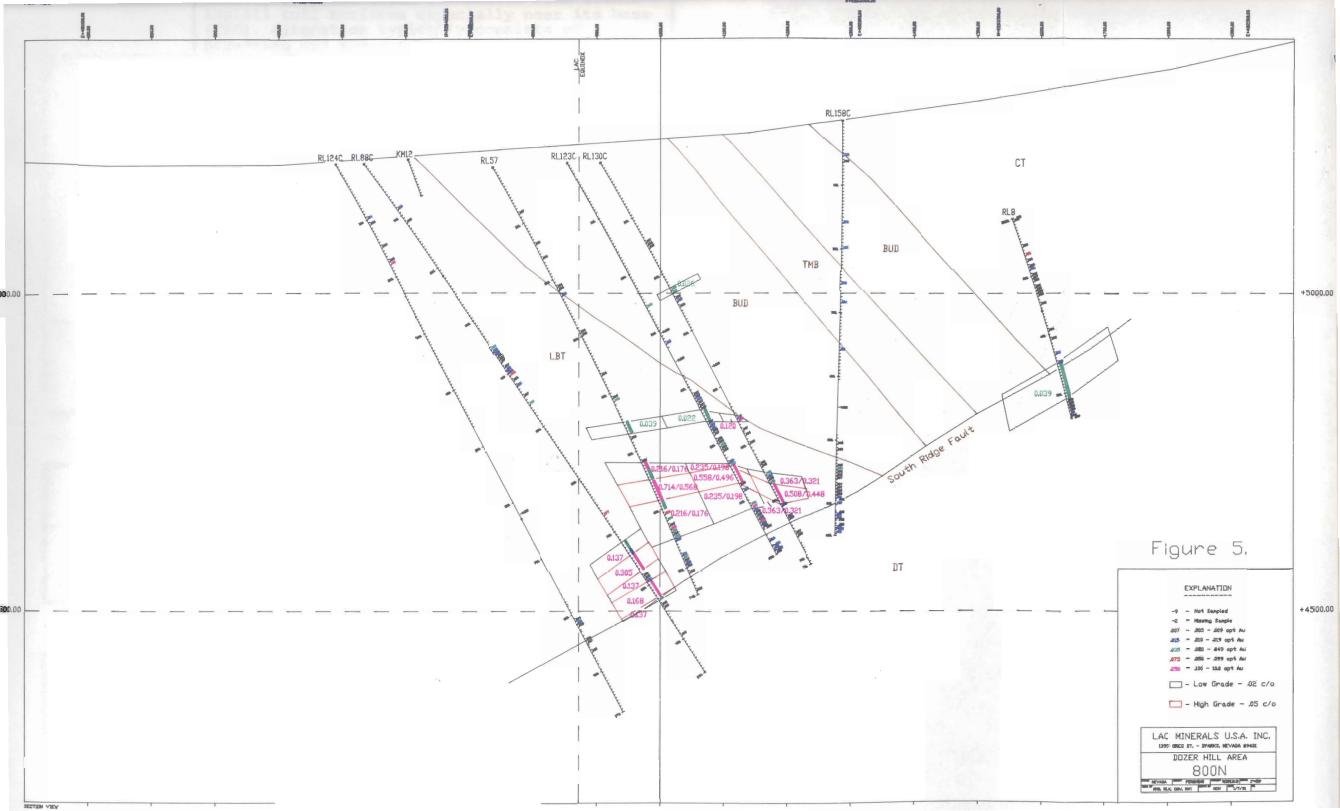


Table 2. Stratigraphic Column - Dozer Hill Area, Rosebud Project

Abbreviation	Description					
CT	Chocolate Tuff: Maroon and grey moderately welded fine grained sanidine-bearing tuff, lithic tuff and volcanic breccia (CIC,TCP). Locally includes green glauconite-rich lithic lapilli tuff horizons especially near its base (C2C). Alteration typically consists of bleaching and moderate to strong argillization.					
BUD	Bud Breccia:					
	Upper Bud - Green to locally brown crudely bedded, poorly sorted lithic lapilli tuff and volcanic breccia. Variably glauconitic. Bleached when altered.					
	TMB - Grey to locally brown fine-grained porhyritic tuff marker bed. Contains 3-5% euhedral feldspar phenocrysts (up to 3mm) wh are commonly replaced by clay or pyrite when altered.					
	Lower Bud - Usually green well bedded lithic lapilli tuff and epiclastic rocks with abundant green glauconite.					
LBT	Lower Bud Tuff: Red-brown (RBUR), tan and grey lithic tuff and fine-grained to banded tuff. When mineralized, it is typically bleached and argillized with a distinctive flesh and/or pale green grey appearance.					

-----South Ridge Fault-----

DT	<u>Dozer Tuff:</u> Pale Green to grey fine-grained densely welded tuff. Lacks visible phenocrysts, Bleached when altered.					
TRANS	Transitional Sediments: Locally occuring basal Tertiary sediments composed of thinly bedded grey to black siltstone and sandstone derived from Mesozoic basement rocks.					

-----Unconformity-----

JTR	Jurassic-Triassic Metasediments: Black carbonaceous phyllite and argillite with common metamorphic quartz veins and local thin felsic
,	dikes.

As currently defined, the deposit has a roughly tabular geometry which is 1800 to 2000 feet long, and averages 300 feet wide and 40 feet thick (Figure 6). The mineralized zone gently plunges at about 20 to 25 degrees from southwest to northeast along a N35E axis oblique to the dip of the South Ridge Fault (Figure 7). At the southwestern end, the top of significant grade is within 200 feet of the surface and, at the northeastern end, it is about 900 feet deep.

The tabular geometry itself gradually changes from being largely concordant with the enclosing host rocks at the southwestern end (15-20 degrees SE apparent dip) to conforming to the dip of the controlling low-angle fault northeast of about Section 400N (25 degree NW apparent dip).

High angle mineralized structures are present especially in the hanging wall to the deposit but these appear to be narrow and discontinuous in grade. Most of the gold-bearing structures in outcrop at Dozer Hill trend N25-45E and dip 65 to 85 degrees NW. Steeply dipping feeder structures are suspected below the deposit but none have yet been recognized. The presence of east-west cross structures is suggested by grade-thickness contours, ground magnetics data and the anomalously thick ore intercept in RL-159C.

Based on a statistical analysis of trace element geochemistry from Dozer Hill drill pulps, ore-grade Au values show closest correlation to Cu, Hg, Se, Ag, As, and Sb, in that order. Highest peripheral trace element correlations are Sb, Ag, Se, \pm Cu, Hg, As, Tl and Au. Quantifiable zonation is unclear except that low gold values on the surface do not preclude significant grades at depth.

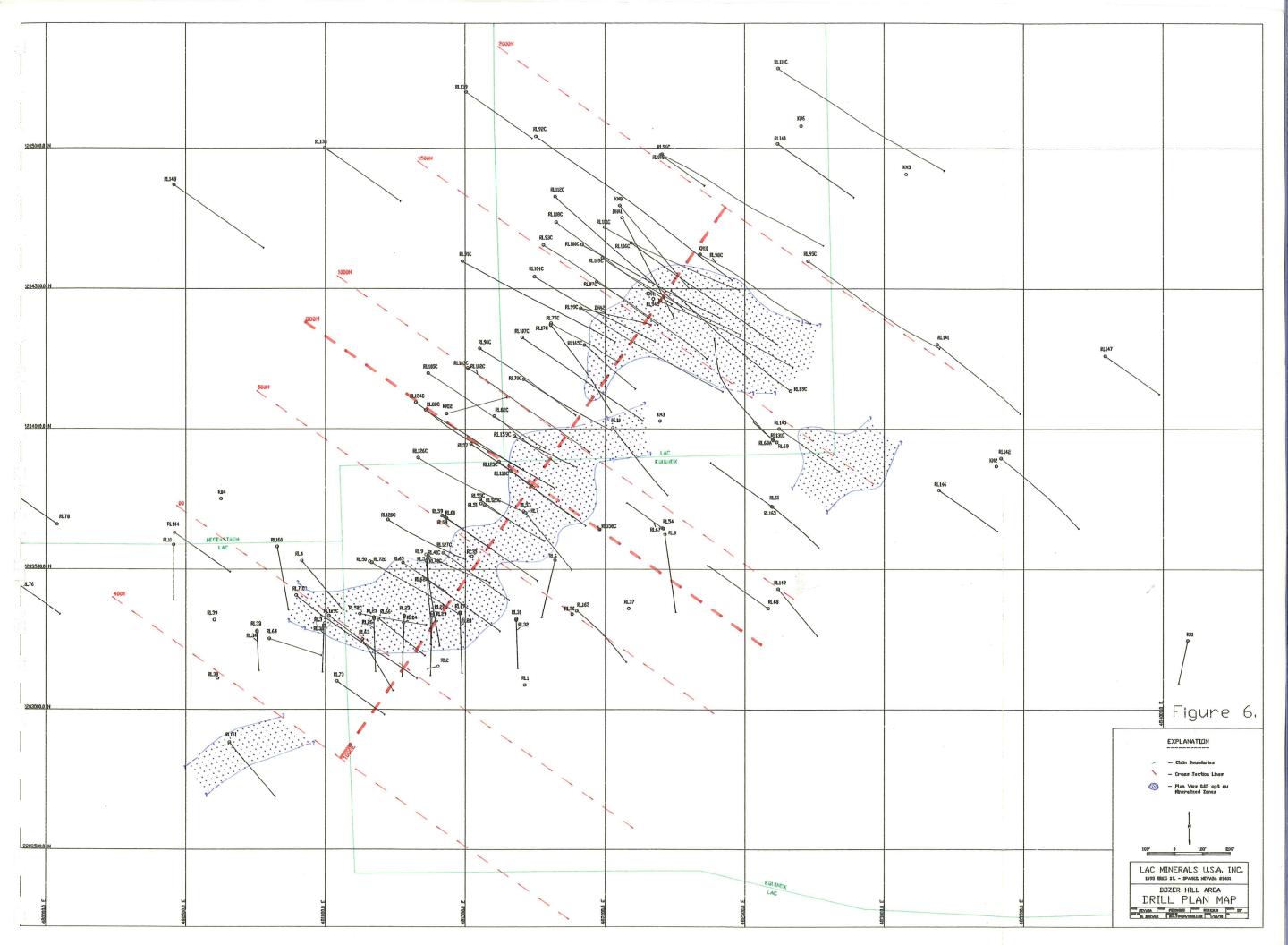
V. Results of the 1990 Program

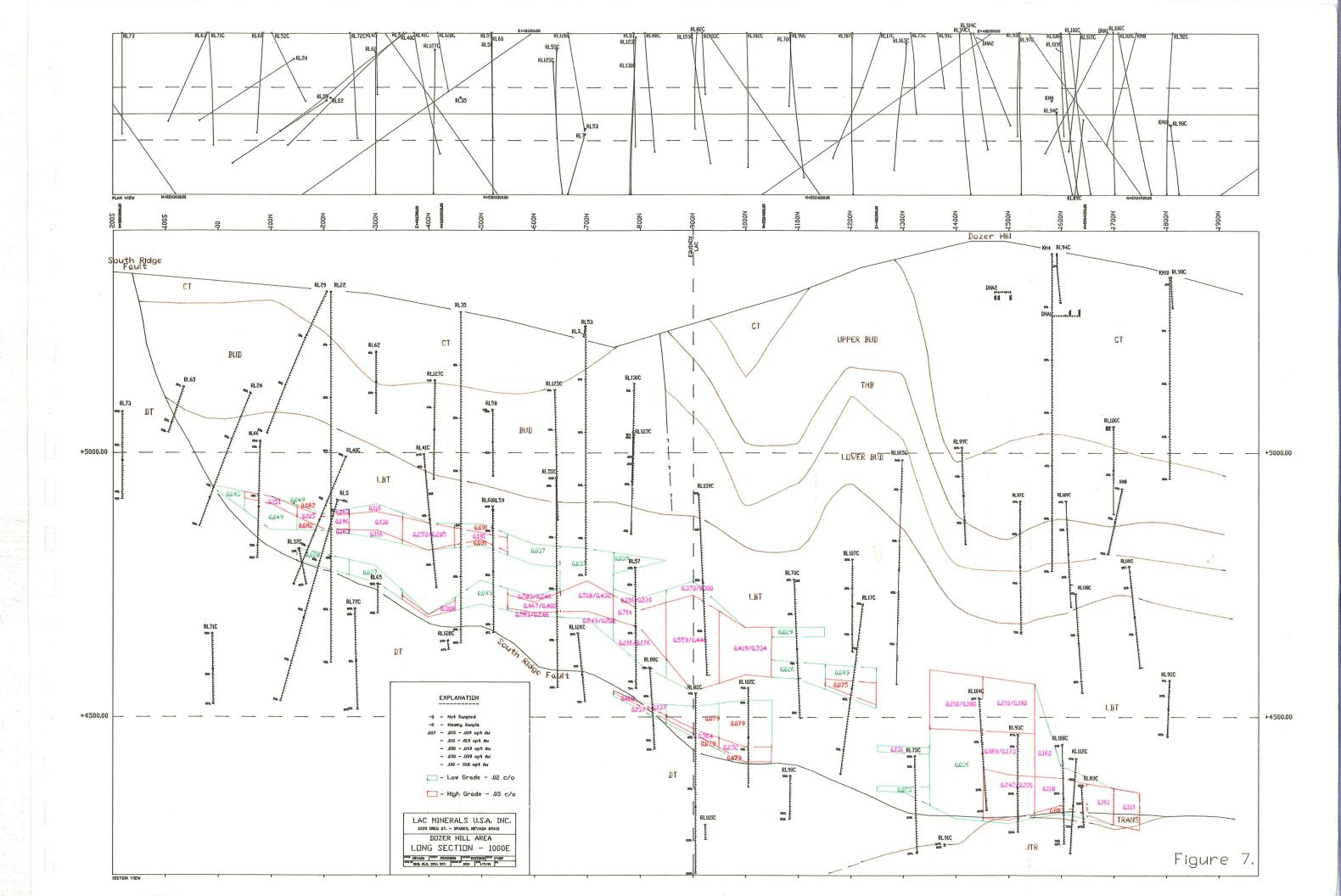
A. Dozer Hill:

The 1990 exploration program focussed primarily on continued drilling in the Dozer Hill area which outlined a significant geologic resource of high grade gold-silver mineralization. During 1990, a total of 74 core and reverse circulation holes totalling 64,410 feet were completed on the Dozer Hill Target. Drill hole locations are shown on Figure 6. Significant intercepts for all holes including Freeport's drilling and LAC's 1989 program are listed in Appendices 1, 2, and 3.

The initial drill hole in 1990, RL-57, intersected 130 feet grading 0.216 opt Au including 35 feet averaging 0.714 opt Au. This hole confirmed the northeast trend of high grade mineralization defined in late 1989. Subsequent drilling has delineated a potentially economic gold-silver resource (Figure 6).

The resource is still open in several areas and current drill hole spacing is insufficient to condemn some internal portions of the





trend especially in vicinity of RL-159C which intersected 170 feet grading 0.559 opt Au. Drill intercepts in RL-131C, 142, and 145 southeast of the main trend could represent a mineralized cross-structure or perhaps a separate parallel zone. A narrow intercept in RL-161, southwest of the main ore zone is also encouraging (Figure 6).

Resource Estimates

A manually generated geologic resource estimate was made for the Dozer Hill deposit utilizing a suite of 1"=50' scale cross-sections created in PCXPLOR (Table 3). These sections are spaced at 100' intervals and oriented N55W-S55E across the deposit trend.

Nominal cut-offs of 0.02 and 0.05 opt Au were selected with a minimum drill width of 8' and a nominal maximum internal waste of 10-15'. Intercept grade composites were generated by the One-D Optimizer routine and/or manually calculated. Cut grades were also calculated for blocks containing assays in excess of 1 opt Au. Twelve holes in the database contain a total of 19 assay intervals greater than 1.0 opt Au with a maximum value of 3.101 opt Au.

Tonnage factors were assigned to the various rock types based upon 21 bulk density measurements made by McClelland Laboratories on representative pieces of core. Ten samples of the main ore host, altered LBT, have tonnage factors which range from 13.8 to 15.6 cu.ft./ton and average 14.44 cu.ft./ton. Over 80% of the resource occurs in this material.

The assumptions and methods used to generate this resource estimate are described in a memo by N.H. Brewer and M.C. Hultgren, 1/26/91.

Table 3. Sectional Geologic Resource Estimates (January 1991).

CUT-OFF AU OPT	CATEGORY	TONS	AU OPT	AU OUNCES	AU OPT (CUT)*	OUNCES (CUT)*
0.02	Probable	4,088,017	0.117	477,580	0.105	429,631
0.02	Possible	1,102,786	0.147	162,351	0.133	146,563
TOTALS:		5,190,803	0.123	639,931	0.111	576,194
0.05	Probable	1,591,720	0.236	375,388	0.210	333,942
0.05	Possible	676,659	0.220	148,721	0.194	131,250
TOTALS:		2,268,379	0.231	524,109	0.206	465,192

(* = High grades cut to 1.0 opt Au)

As currently outlined, about 55% of this resource is located on ground controlled by the LAC-Equinox Joint Venture and the remainder is on claims 100% owned by LAC.

Bruce Davis (Bond Denver) completed a preliminary block model and

kriged reserve study on the deposit in January 1991 (see BD memos 1/31/91 and 2/19/91). Results show a similar global inventory using the 0.02 and 0.05 opt cut-offs but stripping ratios are too excessive for an economic open pit scenario:

Table 4. Kriged Mineral Inventory (February 1991)

CUT-OFF AU OPT	TONS	AU OPT	AU OUNCES	AG OPT	AG OUNCES
0.02	7,195,000	0.092	661,940	0.42	3,021,900
0.05	3,049,600	0.176	536,730	0.59	1,799,264

Although the kriged inventory shows higher tonnage and lower grade, the total contained ounces of Au are within 3.7 and 2.5% respectively of the sectional estimates for these cut-offs.

With assistance from Hans de Ruiter (LAC Kirkland Lake) the following potentially underground mineable reserve was extracted from the "Probable" geologic resource at the 0.05 opt Au cut-off: (see HDR Memo 2/1/91)

Table 5. "Underground Mineable" Ore Reserve (Undiluted).

TONS	AU OPT	AU OZS.	A CONTRACTOR OF THE PARTY OF TH	AU OZS. (CUT)*	AG OPT	AG OZS.
1,245,350	0.284	354,000	0.248	308,800	3.20	3,985,200

^{*} High grade Au assays cut to 1.0 opt.

Approximately 25% of the ounces in Table 5 are contained in the block around RL-159C on Section 900N. However, most "Possible" blocks or isolated intercepts off the main trend, such as RL-145 (45 feet @ 0.202 opt Au), are not included.

Metallurgy

Preliminary metallurgical tests have been completed by McClelland Labs on four core composites from seven drill holes. Although more tests are necessary, these results show that acceptable mill recoveries (85-90%) can be expected from the various ore types at Dozer Hill using conventional processes (Table 6). Detailed reports by McClelland Labs (3/5/90 & 2/19/91) document the procedures and complete results.

The initial work involved bottle roll leach tests and flotation tests on a 4-hole composite from the south half of the deposit averaging a combined 247 feet of 0.135 opt Au and 3.07 opt Ag (RL-40C, 41C, 52C, & 55C). The flotation test results were negative but bottle roll cyanide leach recoveries were excellent (97%).

Another round of metallurgical tests were run on core composites from holes RL-88C, RL-100C, and RL-104C beginning in late 1990.

Bottle roll results were similarly good for RL-88C (87.4%) but disappointing for RL-100C (27.9%). Because of the suspicion that RL-100C contained "preg-robbing" constituents (i.e. adsorbing clays), additional agitated leach, CIL/cyanidation and gravity tests were run on the RL-100C sample, and for comparison, on a similar grade composite from RL-104C, a nearby hole. Results for these tests are summarized below:

Table 6. Metallurgical Test Results Summary.

Drill Hole Comp.	Head Assay Au/Ag opt*	Calc. Head Au/Ag opt	Bottle Roll % 10 M 96 hrs Au/Ag	Bottle Roll % 200 M 48 hrs Au/Ag	Agit'd Leach Rec % 72 hr Au/Ag	CIL/ CN Rec % 72 hr Au/Ag	Grav Conc % 65 M Au/Ag
RL-40C, 41C,52C & 55C	0.116/ 2.96	0.124/ 2.38	85.5 /62.6	96.6 /59.7	N/A	N/A	N/A
RL-88C	0.421/ 1.41	0.419/ 1.30	87.4 /60.0	87.4 / 75.6	N/A	N/A	N/A
RL-100C	0.227/ 13.05	0.203/ 13.24	34.8/ 7.1	27.9/ 5.7	45.3/ 13.7	85.5 /53.4	64.0/ 10.8
RL-104C	0.176/ 0.27	0.179/ 0.38	N/A	N/A	83.2 /50.0	81.9/ 79.2	79.2/ 59.1

^{*} Average of all head grade determinations.

For the bottle roll tests cyanide consumption was low (0.16-0.45 lb/ton) and lime addition normal (5.0-8.2 lb/ton). Cyanide consumptions were considerably higher (1.2-4.21 lb/ton) and lime requirements ranged from 11.3 to 11.9 lb/ton for the mechanically agitated direct and CIL cyanidation tests.

Ore Mineralogy and Alteration

To assist in characterizing the alteration and mineralization at Dozer Hill as well as help in understanding the metallurgical results, Bond Gold's Geochemistry Department in Denver has completed several microprobe, XRD, fluid inclusion and petrographic studies of various core samples from the deposit (Bond Gold Geochemistry Reports 8/90, 1/91, & 2/91). Results show a gradual change in the vein mineralogies and paragenesis between the south and the north ends of the ore zone.

Samples from holes RL-41C, 52C, and 55C located in the southern portion of the deposit (Sections 400N, 100N and 600N respectively) were pervasively sericitized (illitic) prior to being cross-cut by at least two sets of veinlets. The earlier set appears to be barren of precious metals and consists of quartz with lesser pyrite/marcasite, arsenopyrite, sphalerite and galena. Local patches of disseminated sulfides in the wall rock are attributed to

this event. Bladed marcasite crystals usually show variable degrees of replacement by pyrite.

The later set of veinlets contains Mn/Fe-bearing calcite together with trace amounts of silver-rich Sb-sulfosalts, sulfides, selenides and native metal. Gold was seen only as a component of aurian silver (<20% Au) and electrum (<30% Au). The latest stage consists of kaolinite which occurs as veinlets and local replacements of calcite.

Samples from RL-100C at the north end of the deposit (Section 1700N) show an earlier set of quartz plus sulfide veinlets similar to the south end but these also contain electrum (55% Au). A second set consists of quartz plus arsenopyrite, galena, sphalerite and electrum in addition to silver-rich sulfosalts and selenides. Calcite is absent. Electrum occurs in grains up to 60x100 microns in size. Late kaolinite cuts and corrodes quartz and appears to have replaced most of the wall rock feldspars.

In hole RL-88C, which was drilled in the central portion of the deposit (Section 800N), the mineralogy appears to be transitional. Later calcite veins contain silver-rich minerals and electrum similar to the south end, but electrum (avg 48% Au) also occurs in early quartz-pyrite veins. Also, the calcite veins contain significantly more quartz which may suggest a transition to the later calcite-deficient quartz veins present in the north end.

Fluid inclusion work was carried out on coarse barite crystals from the surface at Dozer Hill and quartz and calcite veinlets in RL-55C. Results suggest that all three minerals formed from dilute solutions with temperatures in the range of 140 to 180 degrees C.

Assays

All samples have been assayed for Au and Ag at GSI in Sparks, Nevada using their 1 assay ton fire assay/AA finish method. Check assays on higher grade material have been gravimetric. Additional Au checks have been run on re-splits of selected intervals at Bondar-Clegg, Vancouver and Barringer Labs in Sparks.

During this process of check assaying, it was found that GSI's prep, at least since hole RL-97C, was mostly well below their declared standard of 90% passing -10mesh. Bondar-Clegg re-prepped the rejects prior to making a second pulp. In general, averaged drill composites show a 5-10% increase in gold grade using the Bondar-Clegg results, but the sample-to-sample and assay-to-assay variability is often quite high, especially in the higher grade (+0.2 opt) material suggesting a "nugget effect" sampling problem. Because of this variability, all assays regardless of lab or pulp have been given equal weight and averaged in the database prior to calculating the resource estimates.

Metallic screen assays were run at GSI on selected intervals from several drill holes at Dozer Hill. These show generally higher

this event. Bladed marcasite crystals usually show variable degrees of replacement by pyrite.

The later set of veinlets contains Mn/Fe-bearing calcite together with trace amounts of silver-rich Sb-sulfosalts, sulfides, selenides and native metal. Gold was seen only as a component of aurian silver (<20% Au) and electrum (<30% Au). The latest stage consists of kaolinite which occurs as veinlets and local replacements of calcite.

Samples from RL-100C at the north end of the deposit (Section 1700N) show an earlier set of quartz plus sulfide veinlets similar to the south end but these also contain electrum (55% Au). A second set consists of quartz plus arsenopyrite, galena, sphalerite and electrum in addition to silver-rich sulfosalts and selenides. Calcite is absent. Electrum occurs in grains up to 60x100 microns in size. Late kaolinite cuts and corrodes quartz and appears to have replaced most of the wall rock feldspars.

In hole RL-88C, which was drilled in the central portion of the deposit (Section 800N), the mineralogy appears to be transitional. Later calcite veins contain silver-rich minerals and electrum similar to the south end, but electrum (avg 48% Au) also occurs in early quartz-pyrite veins. Also, the calcite veins contain significantly more quartz which may suggest a transition to the later calcite-deficient quartz veins present in the north end.

Fluid inclusion work was carried out on coarse barite crystals from the surface at Dozer Hill and quartz and calcite veinlets in RL-55C. Results suggest that all three minerals formed from dilute solutions with temperatures in the range of 140 to 180 degrees C.

<u>Assays</u>

All samples have been assayed for Au and Ag at GSI in Sparks, Nevada using their 1 assay ton fire assay/AA finish method. Check assays on higher grade material have been gravimetric. Additional Au checks have been run on re-splits of selected intervals at Bondar-Clegg, Vancouver and Barringer Labs in Sparks.

During this process of check assaying, it was found that GSI's prep, at least since hole RL-97C, was mostly well below their declared standard of 90% passing -10mesh. Bondar-Clegg re-prepped the rejects prior to making a second pulp. In general, averaged drill composites show a 5-10% increase in gold grade using the Bondar-Clegg results, but the sample-to-sample and assay-to-assay variability is often quite high, especially in the higher grade (+0.2 opt) material suggesting a "nugget effect" sampling problem. Because of this variability, all assays regardless of lab or pulp have been given equal weight and averaged in the database prior to calculating the resource estimates.

Metallic screen assays were run at GSI on selected intervals from several drill holes at Dozer Hill. These show generally higher

grades than the respective 1AT assays. Some samples contained considerably more gold in the coarse (+150 mesh) fraction.

Geophysics

With help from the Geophysics Department at Bond Gold in Denver, ground magnetics data for the Dozer Hill grid has been reprocessed and integrated with coarser data from the southern portion of the main NW-SE grid at Rosebud.

The northeast trending mineralized zone at Dozer Hill occurs within a broad area of relatively low magnetics and low magnetic relief. Derivitive products reveal several interesting but subtle trends which may reflect structures that either control or displace the mineralized zone.

A northeast trending weak magnetic high is coincident with the trace of the ore zone under Dozer Hill itself. This feature appears to be truncated at the northeast end of known mineralization by a possible northwest trending cross fault. Offsets in the magnetic data suggested that movement on this fault was right-lateral but subsequent drill holes have failed to encounter additional mineralization. The holes have not adequately tested a possible left-lateral displacement.

A stronger east-west magnetic feature crosses the mineralized trend in the vicinity of Sections 800N and 900N where spectacular intercepts have been drilled. This possible cross structure also coincides with the intercepts in RL-131C, 142, and 145 southeast of Dozer Hill. Further drilling is planned in this area in 1991 and may help explain the significance of this feature.

B. Other Targets:

The 1990 program included 37 drill holes totalling 21,922 feet in 7 other target areas outside of Dozer Hill. Combined with 1989 drilling, 10 separate areas have now received at least a minimum first pass of drilling.

Recent mapping at Dreamland combined with the model which has evolved from Dozer Hill has resulted in a clearer understanding of the epithermal system and controls for mineralization at Rosebud (Figure 4). Consequently, most of the other target areas are currently being re-evaluated and several, including Degerstrom, Chance, Dreamland and Oscar appear to have excellent untested potential.

Table 7 summarizes the highlights of the more important of these prospect areas. Locations are shown on Figure 3. Separate reports document the exploration program at Chance (Brewer 1991b) and geologic mapping at Dreamland (Walck 1991) and Oscar (Fuchs 1991). Additional mapping, sampling and re-interpretation is planned for several of these targets prior to drilling in 1991.

Table 7. Rosebud District Exploration Targets.

TARGET AREA	DESCRIPTION	RESULTS & RECOMMENDATIONS
Chance	Bleached & silicified zone in fgt along N65E range front.Ground mag, IP, soils surveys also indicate E-W cross structure(s).Rock spls contain up to 0.034 opt Au, +high Hg,Sb, ±As, &Tl	9 holes (5,580') in 1990.Best intercept: 160' @ 0.043 Au (RL113) assoc. with strong quartz-pyrite breccias ±400' vertically below alt'd. outcrops along range front. F/U holes to date have been disappointing but good potential remains esp. under pediment gravels. Minimum 5 holes (3000') recommended for 1991.
Degerstrom	Strongly silicified NNW trending low-angle fault in bleached Chocolate Tuff dips west under large area of silified breccia o/c's and NNE trending swarm of sil'd breccia veins. Anomalous soils (up to 824 ppb Au) define both NW and NE trends. Strong IP anomaly coincident with vein swarm in the H/W of low-angle fault.	4 drill holes in 1989 & 2 in 1990 tested near surface of low angle fault and highest soil geochem in the F/W. Best hole: 35' @ 0.034 (RL-48). None of the holes tested the IP anomaly or sil'd breccias in the H/W. At least 5 holes (3000') recommended in 1991.
Dreamland	Old mine area produced Au-Ag ore from high grade E-W vertical breccia veins and south-dipping low angle structure(s) within strongly bleached and acid-leached area. E-W cross faults limit potential to the S. but may down-drop the zone under Badger to the N.	4 Freeport holes and 2 LAC holes in 1989 did not recognize low angle control and drilled mostly barren F/W. U/G sampling suggests remnant dip slope above low-angle structure may have potential for small (~50,000 oz) resource. 8-10 holes (3000-3500') are recommended for 1991

Table 7. Continued: Rosebud District Exploration Targets.

TARGET AREA	DESCRIPTION	RESULTS & RECOMMENDATIONS
East Dreamland	Numerous steep narrow structures in variably bleached low area east of Dreamland coincident with large soil anomaly and local ore grade rock geochem. Area now recognized as F/W of main low angle structure in Dreamland. Highest Au grade (+1.5 opt) in Mother Lode vein on SE side of the target area.	4 Asarco holes, 3 Freeport holes and 11 LAC holes have tested this area for extension of Dreamland mineralization. Best holes: ~60' @ 0.05 opt (Asarco) and 30' @ 0.09 opt (RB-9). Most LAC holes encountered narrow altered zones in fresh Chocolate Tuff at depth. No further work recommended.
N. Equinox	Large steep S. dipping chalcedonic breccia zone in Chocolate Tuff trends N75W across hill at USMM 212. Weak surface geochem and strong IP anomaly coicident with surface trace. NNE trending low-angle structure now recognized dipping west under the area.	4 holes in 1990 tested the high-angle silicified structure and IP anomaly. Best hole: 35' @ 0.012 opt (RL-86). IP anomaly caused by intense quartz-pyrite breccia. Samples of H/W to low-angle fault are pending. More drilling to test low-angle/high angle intersection may be recommended after further work in 1991.
N. Rosebud Peak	Strong N-S trending silicified breccias along ridge N. of Rosebud Peak with weakly anomalous rock geochem (100-200 ppb) ± local "angel wing" calcite and banded chalcedony veining. West dipping low-angle structures found in canyon along east side of the ridge.	No drilling to date. Rock samples of low angle structures pending. Possibly 4 holes recommended for 1991 after additional surface work.

Table 7. Continued: Rosebud District Exploration Targets.

TARGET AREA	DESCRIPTION	RESULTS & RECOMMENDATIONS
Oscar	Dense chalcedonic breccias ± pyrite in Tertiary gravels in H/W to shallow NW dipping Oscar Fault along projection of Rosebud Shear Zone. Ground mag, IP, soil and rock geochem suggest good exploration potential NW and immediately W of the main silicified knob. Steep E-W structures cut altered gravels near the county road with strong coicident geochem.	12 holes by St. Joe & USMX have mainly tested silicified knob area. Holes encountered thick sections of anomalous Ag values ± Au, Hg, As, & Sb. A minimum of 3000-4000' recommended to test other targets away from the obvious silicified knob area, pending a signed agreement with USMX this year.
Short Shot	Large bleached area west of Rosebud Peak cut by numerous N to NE trending silicified structures. Some of these dip W at ± 45 degrees. Anomalous soils (+50 ppb) and rocks (+500 ppb & up to 1500 ppm Sb) collected in 1988 & 1989.	No drilling to date. Further mapping and sampling recommended before drilling.
South Ridge	Strong NW trending soil anomaly (100-3500 ppb Au) in bleached Dozer Tuff adjacent to shallow west-dipping Saddle Fault. Rock spls from road cuts and Saddle Shaft prospect contain silicified veinlets with up to 1.8 ppm Au.	4 holes in 1989 test the soil anomaly. Best intercept: 10' @ 0.028 opt Au. Results show Au grades and alteration confined to narrow "cracks" in otherwise mainly fresh Dozer Tuff. No further work recommended.

Table 7. Continued: Rosebud District Exploration Targets.

TARGET AREA	DESCRIPTION	RESULTS & RECOMMENDATIONS
Valley	Largely covered area straddles the Rosebud Shear Zone in the valley SW of Dozer Hill. Poorly exposed bleached zones along north dipping E-W structures in Badger Fm. and Chocolate Tuff. are coincident with strong IP anomaly. Rock samples carry up to 323 ppb Au.	2 Freeport holes and 7 LAC holes. Best intercepts: 50' @ 0.014 Au (RL-56), and 15' @ 0.032 Au (RL-77). 7 holes contain abundant anomalous Au & Ag values <u>+</u> weak-moderate dissem. and vein pyrite. No further work planned at this time.
White Alps	Prominent chalcedonic quartz-alunite knob along a major N60E structure with pervasively bleached H/W on the SE face of Rosebud Peak. Weak to moderate soil and rock geochem.	1 Freeport hole, 4 LAC holes in 1989 and 4 F/U holes in 1990. Best intercept: 20' @ 0.052 opt Au (RL-19). F/U drilling in 1990 was negative. No further work is recommended at this time.
Wild Rose	Strong silicified breccias ± pyrite and alunite in immed. H/W of NW dipping low-angle structure. Pervasive bleaching, large soil anomaly and strong IP anomaly. Higher-angle structures on the range front and in the F/W of the low angle structure also carry anomalous Au (100-200 ppb).	4 holes drilled in 1990 Best intercept: 20' @ 0.015 opt (RL-120) & 40' @ 0.010 opt Au (RL- 157). Terrain did not allow proper drill test of the H/W of the low- angle structure. Best drill results were from holes on the range front structure. Warrants further work but low priority at this time.

VI. Proposed 1991 Program

The proposed 1991 exploration program at Rosebud is contingent on the results of a contract pre-feasibility study being conducted by Beacon Hill Consultants Ltd. of Vancouver. A budget of \$1,200,000 (\$1,000,000 Net to LAC) has been proposed (Table 8). This program includes \$408,000 under the Equinox joint venture and a \$50,000 minimum work commitment under the Norgold (Chance) joint venture.

The 1991 objectives are to:

- 1) identify a "probable" resource of at least 2,000,000 tons with a 0.25 opt Au average grade at Dozer Hill.
- 2) discover significant high grade mineralization in at least one other target area on the property.

Drilling recommendations are 3-fold:

Phase 1 - 15,000' of RCD drilling at Dozer Hill beginning in early April. This will offset intercepts in RL-145 and RL-161 as well as test other open areas around the main ore zone. About 10,000' of this drilling will be on JV ground.

Phase 2 - 15,000' of core drilling at Dozer Hill beginning in mid-April. Initial targets will be around RL-159C as well as some selected in-fill holes on the main trend such as on Section 700N. Some of these holes will also be drilled for RQD information. If phase 1 is successful, DDH footage will be used to follow-up and confirm ounces in these areas.

<u>Phase 3</u> - 15,000' of track-mounted RCD drilling to test other target areas including: Chance, Oscar, Degerstrom, Dreamland and possibly others. This phase is scheduled to begin in June after phase 1 is completed and additional surface work is done.

Table 8. Proposed 1991 Budget.

Item	Amount
Salaries	\$ 137,900
Contract Labor	15,000
Travel Expenses	20,000
Air Charter	2,000
Roads & Trails	10,000
Miscellaneous	6,700
Rent (Core Shed, etc.)	13,000
Leased Vehicles	12,000
Professional Fees - Consultants	50,000
Professional Fees - Other	36,000
Surveying	17,000
Drilling - Core (15,000' @ \$20/ft)	300,000
Drill Assays - 8,000 @ \$14	112,000
Drilling - Rotary (30,000' @ \$10/ft)	300,000
Surface Sampling Assays	10,000
Claim Staking	5,000
Bonus/Option Payments	67,000
Lease/Rental Payments	20,000
Permitting	20,000
Filing Fees	9,600
Geophysics - Other	10,000
Metallurgy	15,000
Vehicles: Maint & Repair	5,000
Field Supplies	6,800
SUBTOTAL	\$1,200,000
Equinox Contribution (49% of JV Budget)	(200,000)
TOTAL (Net To LAC)	\$1,000,000

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- B. Davis

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J.A. Mueller

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- A. Trodden

Core/Field/Warehouse

- F.M. Wright
- K.E. Kinsella
- T. Bennett

HOLE NO.	T.D.	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
DOZER HILL:					
RL-1	565	VERT.	15-20'/5' 25-30'/5' 275-280'/5' 325-335'/10' 345-375'/30' 385-390'/5'	0.036 0.096 0.046 0.015 0.016 0.019	-0.10 0.11 -0.10 -0.10 0.08 -0.10
RL-2	820	VERT.	50-55'/5' 315-320'/5' 385-390'/5'	0.013 0.010 0.016	-0.10 0.27 0.15
RL-3	505	VERT.	35-40'/5' 95-100'/5' 175-180'/5' 220-355'/135' including 220-275'/55' 225-250'/25'	0.011 0.015 0.010 0.064 0.119 0.224	-0.10 -0.10 -0.10 0.15 0.26 <i>0.47</i>
RL-4	585	S40E/-60	5-10'/5' 155-160'/5' 175-180'/5' 195-200'/5' 205-230'/25' 270-275'/5' 285-290'/5' 310-315'/5' 320-325'/5'	0.012 0.010 0.010 0.016 0.040 0.016 0.026 0.047 0.012	-0.10 -0.10 -0.10 0.10 0.55 -0.10 -0.10 -0.10
RL-5	780	S05E/-58	225-230'/5' 360-365'/5' 370-525'/155' including 375-435'/60' 525-780'/255' (Poss. Contam. 435- (Prob. Contam. 525-		0.10 0.11 3.13 4.24 1.86
RL-6	492 Lost	S13W/-59	80-85'/5' 180-185'/5'	0.013 0.023	-0.10 -0.10

HOLE NO.	T.D.	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-6 Cont'd			445-485'/40'	0.016	0.11
RL-7	620	S39E/-58	40-45'/5'	0.020	-0.10
RL-8	680	S08E/-58	30-35'/5' 110-115'/5' 150-160'/10' 260-265'/5' 285-290'/5' 430-435'/5' 445-510'/65' 530-535'/5' 575-585'/10' 600-605'/5'	0.014 0.089 0.012 0.067 0.011 0.015 0.036 0.011 0.013 0.012	-0.10 0.12 -0.10 -0.10 0.10 0.34 -0.10 0.11 -0.10
RL-9	700	VERT.	125-130'/5 305-310'/5'	0.014 0.049	-0.10 0.80
RL-10C	832 (232' core)	S36E/-58	325-330'/5' 335-340'/5' 400-405'/5' 425-430'/5' 455-460'/5' 475-480'/5' 510-595'/85' including 525-540'/15'	0.011 0.014 0.041 0.014 0.011 0.012 0.020	-0.10 -0.10 0.10 -0.10 0.10 -0.10 0.02
RL-11	480	S00E/-60	465-480'/15'	0.036	0.07
E. DREAML	AND:				
RL-12	405	N05E/-58	30-45'/15' 365-370'/5'	0.027 0.013	1.51 -0.10
RL-13	385	N00E/-60	NIL		
RL-14	285	N00E/-60	NIL		
DREAMLAN	D:			*	
RL-15	445	N19W/-60	NJL		

HOLE NO.	T.D.	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-16	300	NO5E/-66	NIL		.======
DOZER HII	L:				
RL-17C	1065 (460' core)	S36E/-67	215-225'/10' 260-265'/5' 510-515'/5' 530-535'/5' 639-654'/15' 722.5-726'/3.5' 740-795'/55' including 765-790'/25' 833-838.5'/5.5'	0.013 0.034 0.013 0.046 0.02 0.016 0.049 0.075 0.047	0.01 0.19 0.18 0.24 0.07 -0.1 0.16
WHITE ALF	PS:				
RL-18	465 Lost	N49W/-61	275-285'/10'	0.021	1.87
RL-19	445 Lost	N70W/-60	20-25'/5' 75-80'/5' 120-135'/15' 195-215'/20'	0.016 0.013 0.016 0.052	0.25 0.52 1.13 1.04
RL-20	625	VERT.	150-155'/5' 375-380'/5' 395-400'/5'	0.010 0.011 0.016	1.24 0.50 0.36
RL-21	645	N41W/-58	550-555'/5' 560-565'/5' 570-575'/5'	0.015 0.012 0.011	-0.10 -0.10 -0.10
DOZER HIL	L:				
RL-22	700	VERT.	265-270'/5' 355-360'/5' 370-375'/5' 395-540'/145' including 395-450'/55' 410-445'/35' 565-580'/15'	0.041 0.023 0.017 0.075 0.159 0.231 0.012	0.16 -0.10 0.27 1.93 4.62 7.04 0.09

HOLE NO.	T.D.	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-23	660	VERT.	175-180'/5' 340-345'/5' 360-420'/60' including	0.013 0.014 0.028	0.13 -0.10 0.85
			390-405'/15' 445-490'/45' 525-535'/10' 555-560'/5'	0.084 0.023 0.029 0.014	1.77 -0.10 0.13 0.50
RL-24	480	S02W/-58	35-40'/5' 110-115'/5' 395-410'/15' 435-450'/15' 465-480'/15'	0.024 0.033 0.034 0.013 0.026	-0.10 -0.10 0.60 0.12 0.33
RL-25	640	VERT.	0-5'/5' 70-75'/5' 270-345'/75' including	0.030 0.017 0.051	0.44 -0.10 0.24
			325-340'/15' 360-365'/5' 420-425'/5' 435-485'/50' 515-520'/5' 535-540'/5' 560-570'/10' 620-625'/5'	0.149 0.012 0.014 0.019 0.013 0.010 0.020 0.010	0.79 -0.10 -0.10 0.05 0.18 0.14 0.09 -0.10
RL-26	405	S02E/-58	50-55'/5' 90-95'/5' 300-310'/10'	0.033 0.015 0.012	0.18 0.13 0.45
RL-27	580	VERT.	405-520'/115' including 435-480'/45' 555-560'/5' 575-580'/5'	0.076 0.130 0.010 0.032	1.15 2.69 -0.10 -0.10
RL-28	485	S02E/-58	245-250/5' 265-275'/10' 410-415'/5'	0.061 0.016 0.010	0.96 0.54 -0.10

HOLE NO.	T.D.	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-29	505	S02W/-59	290-295'/5'	0.010	-0.10
RL-30	365	S02W/-59	20-25'/5' 110-115'/5'	0.010 0.028	-0.10 -0.10
RL-31	512	VERT.	265-270'/5' 395-400'/5' 480-490'/10'	0.018 0.048 0.011	-0.10 0.23 0.38
RL-32	405	S02E/-60	110-115'/5' 160-165'/5' 245-250'/5'	0.046 0.011 0.034	-0.10 -0.10 0.15
RL-33	465	VERT.	110-115'/5' 120-170'/50' including	0.012 0.022	0.58 0.38
			135-145'/10' 185-190'/5' 200-215'/15' 225-240'/15' 285-290'/5' 445-450'/5'	0.062 0.010 0.010 0.016 0.010 0.014 0.020	1.40 0.42 0.42 0.08 -0.10 -0.10
RL-34	300	S03E/-59	NIL		<i>š</i>
RL-35	625 Lost	VERT.	205-210'/5' 315-320'/5' 345-350'/5' 385-435'/50' including 405-420'/15' 475-545'/70'	0.013 0.013 0.011 0.056 0.120 0.020	0.28 -0.10 -0.10 0.87 1.41 0.44
RL-36	500	VERT.	580-585'/5' 75-80'/5' 130-135'/5'	0.019 0.010 0.012	-0.10 -0.10 -0.10
RL-37	495	VERT.	435-465'30' 20-30'/10' 35-40'/5' 75-80'/5'	0.026 0.025 0.011 0.018	0.05 -0.10 -0.10 -0.10

HOLE NO.	T.D.	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-37 Cont'd.			175-180'/5' 200-205'/5' 225-230'/5' 305-315'/10' 325-340'/15' 400-410'/10' 460-485'/25'	0.013 0.013 0.015 0.033 0.014 0.025 0.033	-0.10 -0.10 -0.10 0.28 -0.10 -0.10
RL-38	296 Lost	VERT.	NIL		
RL-39	370	VERT.	55-60'/5' 125-130'/5' 135-140'/5' 155-160'/5'	0.015 0.011 0.014 0.010	-0.10 -0.10 -0.10 0.11
RL-40C	610	S04E/-58	395-400'/5' 411-466.5'/55.5' including 439.5-463'/23.5' 510.5-513.5'/3'	0.020 0.055 <i>0.105</i> 0.010	0.46 1.31 <i>2.06</i> -0.10
RL-41C	624	S65E/-67	416.5-483'/66.5' including 416.5-436'/19.5' 474-483'/9' 523-528'/5' 553-558'/5' 563-573'/10' 573-576.5'/3.5'	0.233 0.271 1.090 0.013 0.013 0.308 0.016	7.26 7.3.18 28.88 -0.10 0.16 2.77 -0.10
SOUTH RIDGE:					
RL-42	450	VERT.	NIL		
RL-43	310	N76E/-60	NIL		
RL-44	430	S44W/-60	40-55'/15'	0.017	0.02
RL-45	490	S46W/-61	55-65'/10' 240-245'/5'	0.028 0.014	0.02 0.04

HOLE NO.	T.D.	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
DERGERSTROM:					
RL-46	430	N31E/-61	70-90'/20'	0.013	-0.10
RL-47	490	N81E/-61	165-170'/5'	0.010	-0.10
RL-48	440	VERT.	30-55'/25'	0.034	0.10
RL-49	545	S25E/-61	500-505'/5'	0.010	0.14
DOZER HILL:					
RL-50	510	VERT.	145-150'/5' 185-190'/5' 200-205'/5'	0.025 0.015 0.030	0.11 0.12 -0.10
RL-51	510	VERT.	305-310'/5' 335-345'/10' 390-395'/5' 400-405'/5'	0.018 <i>0.113</i> 0.015 0.017	0.11 <i>0.32</i> 0.31 0.13
RL-52C	570	S79E/-64	367-453'/86' including <i>387-428'/41'</i> 399-423'/24'	0.069 0.132 0.155	0.98 - 1.97 2.56
RL-53	470	VERT.	325-330'/5' 335-340'/5' 360-470'/110' 405-470'/65'	0.010 0.010 0.028 0.037	-0.10 -0.10 0.25 0.32
RL-54	625	VERT.	170-175'/5' 215-220'/5' 240-245'/5' 255-265'/10' 280-305'/25' 325-330'/5' 365-370'/5' 395-400'/5'	0.017 0.011 0.018 0.022 0.015 0.018 0.014 0.015	0.25 0.10 0.14 -0.10 -0.10 -0.10 -0.10

Appendix 1:

ROSEBUD PROJECT 1989 DRILLING SUMMARY

HOLE NO.	T.D. II	BEARING/ NCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-55C	692	S52E/-76	290-300'/10'	0.057	-0.10
			335-340'/5'	0.044	0.25
			355-360'/5'	0.021	0.16
			378-382'/4'	0.010	-0.10
			396-447'/51'	0.034	0.07
			including	0.070	
			396-412'/16'	0.050	0.06
			427 – 447'/20'	0.047	0.12
			455-460'/5'	0.024	0.13
			514-549'/35'	0.259	2.05
			including		
			524-544'/20'	0.467	3.36
VALLEY:					
RL-56	450	VERT.	55-105'/50'	0.014	0.82
			145-150'/5'	0.015	-0.10
			285-295'/10'	0.046	-0.10
========	=======	=======	===========	=======	======
SUBTOTALS:					
<u>1989</u>	28,866 Feet		56 Holes		
1990	692 Feet		(2 core ext. in 1990)		
TOTAL:	 29,558 Feet		56 Holes	,	
I O I / L.	20,000 1 661		Ju i luies		

Note:

Intercepts composited @ >5'/0.010 opt Au
 Dozer Hill composites @ 0.05 opt Au cut-off in bold-italics
 "C" suffix on Hole No. = core hole

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
DOZER HILL:					
RL-57	745	S55E/-61	225-230'/5' 410-415'/5' 450-470'/20' 520-650'/130' including 550-585'/35' 675-695'/20'	0.016 0.028 0.039 0.220 <i>0.714</i> 0.016	-0.10 -0.10 -0.10 0.35 -0.10
RL-58	645	S55E/-45	185-190'/5' 255-270'/15' 320-325'/5' 355-365'/10' 430-435'/5' 480-490'/10' 505-600'/95'	0.011 0.016 0.010 0.026 0.035 0.014 0.025	-0.10 0.05 -0.10 0.16 0.14 -0.10 0.41
RL-59	405 Lost	S55E/-63	245-250'/5' 285-290'/5' 300-320'/20' 345-385'/40'	0.015 0.011 0.014 0.017	0.48 -0.10 0.13 0.03
RL-60	615	S55E/-63	330-335'/5' 380-450'/70' including 415-430'/15' 475-480'/5' 505-575'/70'	0.017 0.074 0.261 0.015 0.036	2.20 0.44 1.85 -0.10 1.08
RL-61	945	N55W/-63	325-355'/30' 385-410'/25' 425-440'/15' 460-465'/5' 510-515'/5' 620-625'/5' 675-780'/105' including 705-720'/15' 800-830'/30' 855-860'/5' 890-900'/10' 915-920'/5'	0.015 0.030 0.014 0.014 0.023 0.010 0.024 0.066 0.015 0.010 0.083 0.024	0.02 0.05 0.07 -0.10 -0.10 0.12 0.08 0.11 0.07 -0.10 0.12 -0.10

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-61 Cont'd.			930-935'/5'	0.031	-0.10
RL-62	510	S55E/-45	165-175'/10' 290-295'/5' 345-355'/10' 440-445'/5'	0.035 0.011 0.014 0.026	0.06 -0.10 0.15 0.32
RL-63	325	S31E/-45	485-490'/5' 495-500'/5' 115-120'/5' 170-180'/10'	0.026 0.016 0.052 0.050	-0.10 -0.10 -0.10 0.51
RL-64	335	S70E/-50	175-190'/15'	0.013	-0.10
RL-65	580	S55E/-65	335-420'/85' including	0.038	0.75
			355-375'/20' 450-560'/110'	<i>0.076</i> 0.020	0.43 0.25
RL-66	525	S52E/-61	370-375'/5' 380-385'/5' 400-480'/80' including 400-415'/15'	0.011 0.010 0.045 <i>0.151</i>	-0.10 -0.10 1.69
RL-67	805	N55W/-69	140-145'/5' 210-215'/5' 230-235'/5' 450-455'/5' 560-595'/35' 615-640'/25' 685-700'/15' 750-790'/40'	0.010 0.011 0.015 0.013 0.020 0.022 0.012 0.013	-0.10 -0.10 -0.10 3.31 0.03 -0.10 -0.10
RL-68	715	N55W/-60	175-180'/5' 450-455'/5' 525-530'/5' 535-540'/5' 555-605'/50'	0.012 0.031 0.011 0.011 0.016	-0.10 0.11 -0.10 -0.10 0.02
RL-69	240 Lost	N55W/-62	225-230'/5'	0.012	-0.10
RL-69A (17	1179 '4' core)	N55W/-62	100-105'/5' 245-250'/5'	0.010 0.010	0.18 0.93

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-69A Cont'd.			445-455'/10' 670-680'/10' 700-715'/15' 725-735'/10' 760-1000'/240' including	0.014 0.093 0.079 0.013 0.043	0.17 0.24 0.06 1.64 0.22
			775-845'/70' 930-955'/25' 1162-1166'/4' 1171-1176'/5'	0.082 0.070 0.011 0.018	0.19 0.28 1.08 0.13
RL-70C	1012	S55E/-69	580-585'/5' 635-660'/25' 685-741'/56' 800-805'/5' 810-815'/5' 855-865'/10'	0.019 0.032 0.022 0.010 0.010 0.053	-0.10 0.04 0.03 0.13 0.12 -0.10
RL-71C	887	S51E/-53	197-202'/5' 262-328'/66' including <i>272-314.5/42.5'</i> 397-402'/5'	0.010 0.110 <i>0.156</i> 0.010	-0.10 0.57 0.80 0.13
RL-72C	802	S59E/-63	20-25'/5' 200-205'/5' 295-305'/10' 325-345'/20' 460-464'/4' 509-513'/4' 532-550'/18'	0.010 0.010 0.039 0.058 0.022 0.011 0.043	0.26 0.10 0.10 0.10 0.10 0.10 0.12
RL-73	415	S55E/-50	220-225'/5'	0.011	-0.10
VALLEY:				-	
RL-74	945	N55W/-60	140-145'/5' 270-275'/5' 320-325'/5' 415-420'/10' 455-460'/5' 495-500'/5' 525-530'/5' 635-665'/30'	0.013 0.015 0.095 0.039 0.021 0.012 0.079 0.014	-0.10 -0.10 -0.10 -0.10 -0.10 0.11 0.44 -0.10

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-74 Cont'd.			675-680'/5' 705-715'/10' 835-840'/5' 855-860'/5' 875-880'/5' 910-915'/5'	0.011 0.022 0.017 0.030 0.031 0.016	-0.10 -0.10 -0.10 -0.10 -0.10 -0.10
DOZER HILL:					
RL-75C	1071	S55E/-72	95-100'/5' 305-315'/10' 325-335'/10' 400-415'/15' 500-520'/20' 530-535'/5' 695-720'/25' 735-745'/10' 775-820'/45' including 775-785'/10' 855-860'/5' 865-870'/5' 880.5-892'/11.5' 922-932'/10' 952-972'/20' 1047-1052'/5' 1062-1067'/5'	0.010 0.126 0.019 0.040 0.023 0.038 0.025 0.052 0.076 0.218 0.087 0.149 0.012 0.131 0.018 0.016 0.012 0.016	0.13 -0.10 -0.10 0.22 0.05 0.33 0.22 0.20 0.05 0.13 0.08 0.20 0.39 0.17 -0.10 0.03 -0.10 -0.10
VALLEY:					
RL-76	625	S55E/-60	100-105'/5' 160-165'/5' 175-180'/5' 335-355'/20'	0.012 0.016 0.011 0.014	0.69 -0.10 -0.10 -0.10
RL-77	765	N55W/-60	125-130'/5' 140-155'/15' 165-170'/5' 235-245'/10' 495-500'/5' 570-600'/30' 665-675'/10'	0.027 0.032 0.011 0.032 0.012 0.012 0.016	0.34 0.05 -0.10 0.16 0.11 0.07 -0.10

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-78	745	N55W/-60	230-235'/5' 300-305'/5' 420-430'/10' 515-525'/10'	0.014 0.017 0.011 0.016	0.16 0.21 -0.10 0.26
WHITE ALPS:					
RL-79	705	N44W/-70	260-265'/5' 290-300'/10' 490-505'/15'	0.012 0.011 0.014	0.13 0.89 1.47
RL-80	675	N54W/-45	265-270'/5' 295-300'/5'	0.010 0.012	0.77 1.11
RL-81	805	N45W/-45	nil		
DOZER HILL:					
RL-82C	1065	S55E/-65	345-350'/5' 435-455'/20' 507-531'/24' 594-599'/5' 604-609'/5' 644-682'/38' 698-703'/5' 718-723'/5' 733-817'/84' including 798-807'/9' 837-842'/5'	0.019 0.020 0.019 0.012 0.010 0.453 0.017 0.014 0.061	-0.10 -0.10 -0.10 -0.10 -0.10 <i>0.57</i> -0.10 0.72 0.13
WHITE ALPS:		***			
RL-83 N. EQUINOX:	815	N15W/-60	410-415'/5'	0.010	-0.10
RL-84	620 Lost	N30E/-45	nil	,	
RL-85	530 Lost	N01W/-75	405-420'/15' 425-430'/5'	0.010 0.010	0.07 0.13

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-86	665	N00E/-60	65-80'/15' 105-110'/5' 140-175'/35' 200-205'/5' 265-270'/5' 305-310'/5' 410-415'/5'	0.010 0.011 0.012 0.015 0.035 0.012 0.011	0.19 -0.10 -0.10 0.18 -0.10 -0.10
RL-87	845	N30W/-60	nil		
DOZER HILL:					
RL-88C	962	S55E/-53	85-90'/5' 350-360'/10' 390-405'/15' 420-425/5' 455-460'/5' 665-670'/5' 720-775'/55' including 745-775'/30' 795-825.7'30.7'	0.013 0.015 0.025 0.012 0.020 0.077 0.176 0.305 0.168	0.10 -0.10 0.08 0.17 -0.10 0.37 0.78 1.18 3.89
RL-89C	1152	N54W/-60	115-120'/5' 400-405'/5' 460-470'/10' 540-545'/5' 585-590'/5' 837-841.8/4.8' 852-862'/10' 882-887'/5' 892-1098.2'/206.2 including 941-1092'/151' 1024-1092'/68' 1132-1135'/3' 1149-1152'/3'	0.015 0.031 0.037 0.015 0.018 0.012 0.056 0.010 0.142 0.181 0.314 0.024 0.011	0.20 0.12 0.01 -0.10 -0.10 -0.10 1.30 -0.10 0.24 0.28 0.54 1.35 1.21
RL-90C	1012	S55E/-63	5-10'/5' 55-75'/20' 225-230'/5' 295-340'/45' 355-365'/10' 445-450'/5'	0.010 0.013 0.012 0.020 0.012 0.019	-0.10 0.08 -0.10 0.09 0.10 0.31

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-90C Cont'd.			503-507.7'/4.7' 533-543'/10' 583-587'/4' 839-859.8/20.8' 873-883'/10' 897-906'/9'	0.072 0.020 0.016 0.031 0.014 0.017	0.15 0.27 -0.10 0.15 -0.10 -0.10
RL-91C	1150	S55E/-60	145-150'/5' 295-300'/5' 711-713.9'/2.9' 985-995'/10' 1033.5-1035.5/2'	0.049 0.022 0.012 0.010 0.021 0.045	0.14 -0.10 -0.10 -0.10 -0.10
RL-92C	1281	S55E/-49	175-180'/5' 190-195'/5' 210-220'/10' 270-290'/20' 685-690'/5' 1046-1055/9' 1070-1075/5' 1180-1190'/10' 1215-1220/5' 1230-1270/40' including 1240-1257.5/17.5		0.21 0.26 -0.10 -0.10 0.10 -0.10 0.05 0.10 0.36
RL-93C	1082	S55E/-60	45-50'/5' 130-140'/10' 150-165'/15' 195-200'/5' 425-430'/5' 460-462'/2' 560-563'/3' 830-835'/5' 860-865'/5' 876-880'/4' 920-1050'/130' including 945-1044'/99' 1010-1030'/20'	0.054 0.031 0.020 0.035 0.047 0.015 0.101 0.023 0.021 0.032 0.013 0.189 0.242 0.649	0.45 -0.10 0.08 0.14 0.30 0.21 0.42 0.27 -0.10 -0.10 0.43

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-94C	1199	S55E/-60	100-105'/5' 450-455'/5' 585-590'/5' 600-605'/5' 635-640'/5' 670-675'/5' 695-700'/5' 845-855'/10' 890-903'/13' 915-975'/60' including 940-965'/25' 995-1010'/15' 1020-1025'/5' 1045-1065'/20' including	0.032 0.054 0.010 0.014 0.013 0.019 0.012 0.019 0.013 0.061 0.112 0.044 0.022 0.205	-0.10 0.13 1.33 -0.10 -0.10 0.12 0.10 0.17 0.11 0.20 0.38 1.45 0.28 0.50
			<i>1050 – 1060'/10'</i> 1140 – 1145'/5' 1195 – 1199'/4'	0.367 0.083 0.038	0.60 2.22 0.48
RL-95C	1270	S55E/-60	560-565'/5' 966-977'/11' 1192.6-1193.1'/0 .5'	0.013 0.017 0.014	-0.10 -0.10 -0.10
RL-96C	1192	S55E/-60	60-70'/10' 145-175'/30' 860-865'/5' 1147-1152'/5'	0.013 0.060 0.023 0.020	0.17 -0.10 0.72
RL-97C	1252	S55E/-63	1177-1182'/5' 240-245'/5' 445-450'/5' 833-995'/162' including 833-850'/17'	0.012 0.017 0.011 0.056	0.20 -0.10 0.18 0.51
RL-98C	1061	S55E/-63.5	913-940'/27' 270-275'/5' 910-945'/35'	0.100 0.160 0.018	0.82 0.64 0.86
RL-99C	1242	S55E/-58.5	955-960'/5' 235-240'/5' 320-330'/10' 365-370'/5' 395-400'/5' 512-517'/5'	0.010 0.039 0.056 0.010 0.016 0.024	-0.10 -0.10 0.08 -0.10 0.18 -0.10

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-99C Cont	d.		837-842'/5' 862-867'/5' 892-1062/170'	0.053 0.021 0.015	-0.10 -0.10 0.50
			including 965-980'/15'	0.030	0.11
RL-100C	1168.5	S55E/-60	350-355'/5' 887-916'/29' <i>930.5-1027/96.5'</i>	0.026 0.075 0.215	0.12 -0.10 11.78
			including 930.5-965/34.5' 976-1001.5/25.5' 1011.5-1022/10.5' 1072-1087/15' 1127-1132/5'	0.284 0.240 0.252 0.033 0.015	0.38 1.50 96.32 2.84 2.62
RL-101C	1123.5	S54E/-59	577-582'/5' 587-597'/10' 612-617'/5' 662-667'/5' 687-692'/5' 732.6-735.8/3.2 762-777'/15' 807-813'/6' 904-909'/5' 977-982'/5' 997-1063.8/66.8' including 1023-1044'/21'	0.036 0.017 0.044 0.012 0.139 0.136 0.091 0.010 0.010 0.023 0.045	0.27 0.10 0.29 0.44 -0.10 0.46 0.23 0.11 -0.10 -0.10 1.08
RL-102C	1092	S56E/-59.5	35-40'/5' 195-205'/10' 275-280'/5' 375-380'/5' 410-415'/5' 430-451'/11' 456-461'/5' 492-497'/5' 507-552'/45' 567-582'/15' 670-676'/6' 760.5-766'/5.5' 801.5-920'/118.5 including	0.010 0.014 0.051 0.023 0.020 0.012 0.017 0.019 0.020 0.028 0.011 0.013 0.066	-0.10 0.14 1.38 0.28 -0.10 -0.10 -0.10 0.10 0.05 0.12 0.10 0.11

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-102C Cont'd	d.		892-920'/28'	0.232	0.27
RL-103	295	VERT.	45-50'/5' 190-195'/5' 240-245'/5'	0.011 0.022 0.013	-0.10 -0.10 -0.10
RL-104C	1087	S55E/-60	527-567'/40' 742-922'/180' including	0.014 0.136	0.02 0.26
			742-872'/130' 754-782'/28' 807-872'/65' 937-954.5/17.5'	0.210 0.323 0.206 0.030	0.34 0.56 0.39 0.28
			967-982'/15' 1007-1026.3'/19.3'	0.011 0.060	0.04 0.07
RL-105C	1062	S55E/-60	110-115'/5' 120-125'/5' 145-150'/5' 200-205'/5' 594-599'/5' 809-814'/5' 823-828'/5' 838-842'/4'	0.017 0.011 0.021 0.022 0.011 0.029 0.013 0.012	-0.10 0.23 -0.10 -0.10 0.13 1.52 0.16 0.16
RL-106C	1237	S51E/-60	287-292'/5' 302-307'/5' 327-332'/5' 347-352'/5' 411.5-417'/5.5' 702-707'/5' 983-992'/9' 1007-1012'/5' 1022-1067'/45' including 1047-1067'/20' 1087-1102'/15' 1147-1152'/5' 1162-1212'/50' including 1187-1202'/15'	0.032 0.013 0.014 0.031 0.035 0.011 0.148 0.024 0.038 0.023 0.010 0.064	-0.10 -0.10 -0.10 -0.10 -0.10 -0.10 2.12 0.51 0.16 0.22 0.12 -0.10 5.62
RL-107C	1030	S52E/-55	275-280'/5' 305-320'/15'	0.016 0.058	0.21 -0.10

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-107C Cont'c	I.		345-350'/5' 395-420'/25' 667-672/5' 678-682'/4' 777-782/5' 840-845'/5' 850-855'/5' 905.5-910.5/5'	0.030 0.044 0.016 0.025 0.023 0.025 0.014 0.013	-0.10 0.16 0.20 -0.10 1.30 -0.10 0.19 -0.10
RL-108C	1107	S51E/-60	437-442'/5' 472-477'/5' 937-942'/5' 972-1037/65' including 992-1027/35' 1037-1107/70' including 1062-1082/20'	0.021 0.016 0.019 0.103 0.137 0.012	-0.10 0.24 0.12 0.24 0.41 3.51 9.01
RL-109C	1247	S51E/-60	889-1015.5/126.5' including 967-988'/21' 1062-1068/6' 1102-1107/5' 1122-1132/10' 1201.5-1205.5/4' 1232-1237/5'	0.050 0.162 0.011 0.033 0.013 0.016 0.014	1.17 2.19 -0.10 -0.10 1.36 6.32 -0.10
RL-110C VALLEY:	1232	S55E/-55	185-190'/5' 195-200'/5' 245-250'/5' 355-360'/5' 380-385'/5' 390-395'/5' 1193.5-1202/8.5'	0.010 0.021 0.016 0.010 0.013 0.012 0.048	-0.10 2.72 0.44 0.18 0.12 -0.10 0.11
RL-111C	957	S00E/-45	252-257'/5' 587-592'/5' 879-884'/5' 907-912'/5' 922-927'/5'	0.039 0.012 0.034 0.025 0.068	0.21 0.28 -0.10 -0.10 0.11

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
DOZER HILL:					
RL-112C	1229.5	S45E/-58	35-40'/5' 85-110'/25' 475-508'/33' 517-522'/5' 522-527'/5' 546-552'/6' 857-862'/5' 927-937'/10' 947-952'/5' 972-977'/5' 997-1002'/5' 1017-1022/5' 1027-1069/42' including 1032-1052'/20' 1085.8-1094.5/8.7' 1105-1130.5/25.5' 1145.5-1156/10.5 1171.9-1199/27.1	0.010 0.036 0.013 0.019 0.012 0.028 0.073 0.043 0.022 0.021 0.038 0.010 0.068 0.013 0.014 0.012 0.027	0.10 0.38 0.15 0.26 0.29 0.11 -0.10 0.47 -0.10 0.19 -0.10 -0.10 0.72 1.24 8.14 1.04 2.12 1.23
CHANCE TAP	RGET:				
RL-113	800	S10W/-45	325-350'/25' 395-700'/305' including 510-670'/160' including 530-565'/35' 710-715'/5' 720-725'/5' 740-755'/15' 785-795'/10'	0.020 0.029 0.043 0.086 0.013 0.012 0.018 0.036	0.09 0.03 0.03 0.06 -0.10 -0.10 -0.10
RL-114	800	S10W/-45	nil		
RL-115	715	S10W/-60	nil		
RL-116	510	S10W/-60	500-505'/5'	0.010	0.15
RL-117	600	S10W/-60	nil		

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
WILD ROSE:	=====			=======	======
RL-118	640	N35E/-45	nil		
RL-119	500	S00E/-45	nil		
RL-120	495	N19E/-60	40-45'/5' 110-125'/15' 155-175'/20' 265-270'/5'	0.035 0.015 0.015 0.042	-0.10 0.09 0.06 0.27
EAST DREAMLA	ND:		200 27070	0.042	0.27
RL-121	300	N20W/-45	nil		
RL-122	400	N20W/-65	245-265'/20' 325-350'/25'	0.015 0.019	5.62 -0.10
DOZER HILL:					
RL-123C	698	S55E/-60	255-260'/5' 421.5-477/55.5' 502-507'/5' 532-572'/40' including 542-572'/30' 582-587'/5' 607-617'/10' 632-667'/15'	0.025 0.015 0.022 0.405 0.558 0.012 0.078 0.031	-0.10 0.22 0.20 7.21 9.57 -0.10 0.12 0.24
			671-692'/11'	0.011	0.16
RL-124C	972	S55E/-60	95-100'/5' 175-180'/5' 812-817'/5'	0.014 0.110 0.010	-0.10 0.38 -0.10
RL-125C	662	S55E/-65	160-165'/5' 285-295'/10' 432-437'/5' 457-462'/5' 457-542'/85' including	0.013 0.015 0.015 0.019 0.149	-0.10 0.06 0.12 1.14 4.24
	*		487-527'/40' 572-596'/24' including 572-582'/10'	0.373 0.056 0.110	8.39 1.05 1.18

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-126C	781	S55E/-60	85-90'/5' 105-110'/5' 210-215'/5' 280-285'/5' 310-315'/5' 515-520'/5'	0.012 0.026 0.016 0.030 0.010 0.011	0.22 0.16 -0.10 0.21 0.30 0.18
RL-127C	610.5	S55E/-60	385-390'/5' 407-412'/5' 487-492'/5' 502-542'/40' including 502-517'/15' 550-555'/5'	0.010 0.011 0.020 0.092 0.176 0.014	-0.10 0.19 0.10 1.72 1.43 0.27
RL-128C	667	S55E/-60	220-225'/5' 334-337.5'/3.5' 346-351'/5'	0.013 0.010 0.012	0.14 -0.10 0.26
RL-129C	442	S54E/-60	80-85'/5' 110-115'/5' 263-267'/4' 302.5-392/89.5' including 321.5-362/40.5'	0.016 0.012 0.012 0.106 0.216	0.22 -0.10 0.22 0.15
RL-130C	712	S55E/-59	225-250'/25' 452-462'/10' 551.1-612/60.9' including <i>572-607'/35'</i>	0.016 0.120 0.282 <i>0.508</i>	0.71 0.11 2.86 4.68
RL-131C	1078	VERTICAL	0-5'/5' 280-285'/5' 290-295'/5' 667-672'/5' 677-681'/4' 760-807'/47' including 765-770'/5' 848-852'/4' 897-901.5'/4.5' 965.5-971'/5.5'	0.020 0.031 0.047 0.011 0.015 0.200 1.670 0.038 0.097 0.021	-0.10 0.14 0.13 2.00 5.07 0.03 1.37 -0.10 0.12 0.24

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT			
EAST DREAML	EAST DREAMLAND:							
RL-132	200	N20E/-45	nil					
RL-133	300	N00E/-45	70-75'/5' 95-100'/5'	0.011 0.015	0.19 -0.10			
RL-134	145	N20E/-45	10-15'/5'	0.013	0.51			
RL-135	300	N20E/-45	95-100'/5'	0.013	0.35			
RL-136	660	N45W/-45	135-140'/5' 295-300'/5' 405-420'/15'	0.010 0.016 0.010	0.19 -0.10 0.27			
RL-137	400	S10E/-45	nil					
DOZER HILL:								
RL-138	1040	S55E/-60	50-55'/5' 70-85'/15' 220-225'/5' 290-295'/5' 380-385'/5' 645-650'/5'	0.017 0.011 0.012 0.010 0.010 0.020	-0.10 -0.10 0.20 -0.10 -0.10			
RL-139	800	S55E/-60	145-160'/15' 195-200'/5' 215-220'/5' 230-240'/10' 335-360'/25' 395-405'/10' 430-435'/5'	0.023 0.011 0.010 0.017 0.011 0.077 0.024	-0.10 0.13 -0.10 0.17 0.02 0.16 0.12			
RL-140	1050	S55E/-60	105-110'/5' 135-140'/5' 270-275'/5'	0.021 0.017 0.015	-0.10 -0.10 -0.10			
RL-141	1155	S55E/-60	775-780'/5' 930-940'/10' 985-995'/10' 1010-1025/15'	0.047 0.028 0.019 0.018	0.16 1.22 0.35 0.45			
RL-142	845	S55E/-60	260-265'/5'	0.012	-0.10			

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-142 Cont'd.			320-325'/5'	0.010	0.46
			335-345'/10'	0.040	0.44
			375-380'/5'	0.041	0.56
			385-390'/5'	0.010	-0.10
			405-410'/5'	0.010	0.21
			555-580'/25'	0.029	0.08
			620-625'/5'	0.012	-0.10
			685-710'/25'	0.032	0.29
RL-143	1005	S55E/-60	375-380'/5'	0.013	1.03
RL-144	625	S55E/-60	115-125'/10'	0.016	0.05
			590-595'/5'	0.015	-0.10
			605-610'/5'	0.011	-0.10
RL-145	700	S55E/-60	140-145'/5'	0.017	-0.10
			420-430'/10'	0.030	2.70
			445-450'/5'	0.011	0.35
			465-470'/5'	0.012	-0.10
			505-510'/5'	0.029	-0.10
			540-550'/10'	0.013	1.12
			605-610'/5'	0.047	1.85
			615-620'/5'	0.035	0.91
			640-700'/60'	0.158	0.08
			including		
			640-685'/45'	0.202	× 0.10
RL-146	665	S55E/-60	160-180'/20'	0.046	2.09
			270-275'/5'	0.016	-0.10
			325-330'/5'	0.062	-0.10
			345-350'/5'	0.012	-0.10
			450-470'/20'	0.014	0.03
			490-495'/5'	0.011	-0.10
			575-595'/20'	0.029	0.68
*			610-630'/20'	0.011	0.19
RL-147	605	S55E/-60	335-340'/5'	0.028	-0.10
			365-370'/5'	0.020	-0.10
RL-148	645	S55E/-45	125-130'/5'	0.028	0.18
			375-380'/5'	0.010	0.35
			525-530'/5'	0.012	-0.10
			630-635'/5'	0.012	0.12

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-149	545	S40E/-60	260-265'/5' 305-335'/30' 400-430'/30'	0.010 0.019 0.014	-0.10 0.06 -0.10
VALLEY:					
RL-150	700	S55E/-60	585-600'/15'	0.018	0.17
DEGERSTROM:					
RL-151	500	N30E/-60	170-180'/10' 205-210'/5'	0.013 0.030	0.09 0.27
N 2203 850 E 477 47		20 5/08.8	240-250'/10' 275-290'/15'	0.040 0.011	0.27 0.09 0.25
RL-152 N Z 203,		N50E/-45	nil		
CHANCE: E 4	77,733	,3 elv 5008.5			
RL-153	600	VERTICAL	425-525'/100' including	0.036	0.08
			455-505'/50' 540-545'/5' 560-565'/5' 580-585'/5'	0.059 0.032 0.018 0.011	0.06 -0.10 0.21 -0.10
RL-154	645	S20E/-45	55-65'/10'	0.013	-0.10
RL-155	505	S20E/-45	nil		
RL-156	405	S20E/-45	5-15'/10'	0.032	0.19
WILD ROSE:					
RL-157	405	N20E/-60	60-65'/5' 320-360'/40'	0.012 0.010	-0.10 -0.10
DOZER HILL:					
RL-158C	650	VERTICAL	50-55'/5' 155-160'/5' 195-200'/5' 250-255'/5' 280-285'/5'	0.015 0.012 0.015 0.012 0.014	-0.10 0.18 -0.10 -0.10 -0.10

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-158C Cont'd	I.		354-359'/5' 542-547'/5' 595-602'/7' 614-624'/10' 634-647'/13'	0.011 0.018 0.027 0.011 0.015	-0.10 -0.10 2.64 0.19 0.30
RL-159C	852	S55E/-70	170-175'/5' 225-240'/15' 260-270'/10' 362-367'/5' 387-392'/5' 412-417'/5' 427-432'/5' 452-467'/15' 502-777/275' including 527-697'/170' 732-777'/45'	0.033 0.017 0.040 0.038 0.012 0.013 0.028 0.017 0.370 0.559 0.112	-0.10 0.08 0.16 -0.10 -0.10 -0.10 0.05 0.10 1.44 0.23
RL-160	400	S10E/-50	150-225'/75' 350-355'/5'	0.024 0.018	0.24 -0.10
RL-161	405	S45E/-45	105-145'/40' including 105-115'/10'	0.035	0.09
RL-162	445	S55E/-45	10-15'/5' 90-95'/5' 105-125'/20' 190-200'/10' 340-345'/5' 360-365'/5'	0.011 0.027 0.026 0.035 0.024 0.018	0.23 -0.10 -0.10 0.05 -0.10 -0.10
RL-163	600	S55E/-60	75-80'/5' 175-180'/5' 275-280'/5' 285-290'/5' 300-305'/5' 345-365'/20' 375-380'/5' 425-430'/5' 495-500'/5' 520-530'/10' 550-570'/20'	0.014 0.017 0.028 0.013 0.016 0.022 0.020 0.011 0.013 0.011 0.028	0.24 -0.10 0.21 0.20 0.16 -0.10 0.71 -0.10 0.14 0.78 2.44

Appendix 2:

ROSEBUD PROJECT 1990 DRILLING SUMMARY

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
RL-163 Cont'd			585-595'/10'	0.025	-0.10
RL-164	545	VERTICAL	nil		
RL-165C	1032	S55E/-75	384-389'/5' 603.5-608.5/5' 649-655'/6 723-731'/8' 802-829.5/27.5' 844-854'/10' 859.5-870.5/11' 906-911'/5' 937-947'/10'	0.053 0.031 0.031 0.011 0.017 0.014 0.027 0.024 0.019	-0.10 0.26 0.35 0.07 0.03 0.06 0.14 0.15 0.12
RL-166	1100	S55E/-68	80-85'/5' 95-115'/20' 750-755'/5' 840-855'/15' 1095-1100/5'	0.015 0.027 0.022 0.028 0.015	-0.10 -0.10 -0.10 0.37 -0.10
RL-167	800	VERTICAL	185-205'/20'	0.013	0.20
SUB-TOTALS:					
	85,640 Feet 692 Feet		111 Holes (2 extensions)		

TOTALS:

86,332 Feet

1989 - 1990 PROJECT TOTALS:

115,198 Feet

167 holes

Note:

- Intercepts composited @ >5'/0.010 opt Au
 Dozer Hill composites @ 0.050 opt Au cut-off in bold italics.
 "C" suffix on Hole No. = core

ROSEBUD PROJECT FREEPORT DRILLING SUMMARY 1985-1986

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT			
Phase I (1985)	Phase I (1985):							
KM-1	605	S12W/-75	NIL					
KM-2	605	VERT.	100-105'/5' 390-400'/10' 590-605'/15'	0.020 0.014 0.012	~ 0.05 1.04 0.29			
KM-3	600	VERT.	15-25'/10' 115-120'/5' 430-435'/5' 450-470'/20' 490-495'/5' 555-560'/5' 575-585'/10' 595-600'/5'	0.094 0.093 0.026 0.011 0.011 0.011 0.018 0.013	0.06 0.39 0.05 0.06 0.15 0.04 0.07			
KM-4	600	VERT.	160-170'/10' 175-180'/5' 250-255'/5' 530-540'/10'	0.018 0.021 0.041 0.117	0.07 ~ 0.04 ~ 0.03 0.03			
KM-5	400	VERT.	NIL		d ^{'d'}			
KM-6	400	VERT.	275-280'/5'	0.025	0.02			
KM-7	340	VERT.	NIL					
KM-8	600	S40E/-50	235-240'/5' 265-270'/5' 285-290'/5' 320-325'/5' 540-550'/10' 560-565'/5' 590-600'/10'	0.019 0.010 0.039 0.076 0.016 0.049 0.019	0.08 0.04 0.03 ~ 0.05 0.07 ~ 0.04 -0.02			
KM-9	365	VERT.	165-170'/5' 180-190'/10' 325-335'/10' 350-365'/15'	0.016 0.018 0.053 0.027	ND ND ND ND			

Appendix 3:

ROSEBUD PROJECT FREEPORT DRILLING SUMMARY 1985-1986

HOLE NO.	T.D. FEET	BEARING/ INCLINATION	INTERCEPT FROM-TO/WIDTH	AU OPT	AG OPT
KM-10	380	VERT.	70–75'/5'	0.025	ND
KM-11	405	S46E/-60	180-185'/5'	0.046	ND
KM-12	445	N75E/-60	NIL		
Phase 2 (1986	S):				
RB-1	500	N05E/-70	255-260'/5' 355-360'/5'	0.019 0.032	ND ND
RB-2	660	N05E/-60	0-5'/5'	0.013	ND
RB-3	460	N35W/-70	NIL		
RB-4	405	VERT.	25-30'/5' 75-80'/5' 120-125'/5'	0.010 0.010 0.013	ND ND ND
RB-5	425	VERT.	0-5'/5' 35-40'/5' 115-135'/20' 175-190'/15' 205-220'/15'	0.042 0.010 0.027 0.014 0.015	ND ND ND ND ND
RB-6	405	VERT.	NIL		
RB-7	305	S07E/-60	NIL		
RB-8	300	VERT.	NIL		
RB-9	305	VERT.	75-105'/30' including 75-90'/15'	0.099 0.186	ND ND
RB-10	485 =====	S85E/-60	NIL ========	======	

TOTAL:

9,995 Feet

22 Holes