Mining District File Summary Sheet

DISTRICT	Rosehud
DIST_NO	4010
COUNTY If different from written on document	Pershing
TITLE If not obvious	Report to LAC Minerals on the Rosebud Pre-Feasibility, Pershing County, Nevada, July 1992
AUTHOR	Bhacti Engineering Associates, Inc.
DATE OF DOC(S) MULTI_DIST Y / N2 Additional Dist_Nos:	1992
QUAD_NAME	Sulphur 72'
P_M_C_NAME (mine, claim & company names)	Roschud Mine; Lac Minerals (USA), Ire; Bharti Engineering Associates Inc South Zone, East Zone; North Zone
COMMODITY If not obvious	gold, silver
NOTES	Property report: geology; reserves: cost analysis
	NOTE: Scandividers
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Revised: 1/22/08	Initials Date



REPORT

TO

LAC MINERALS

ON

THE

ROSEBUD PRE-FEASIBILITY
PERSHING COUNTY, NEVADA

JULY 1992



Bharit Digineering Associates Inc.

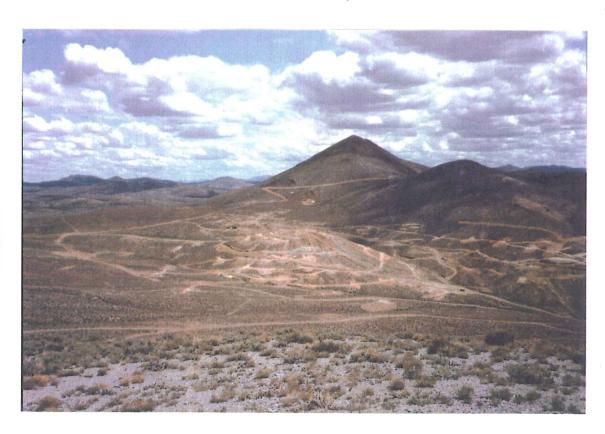
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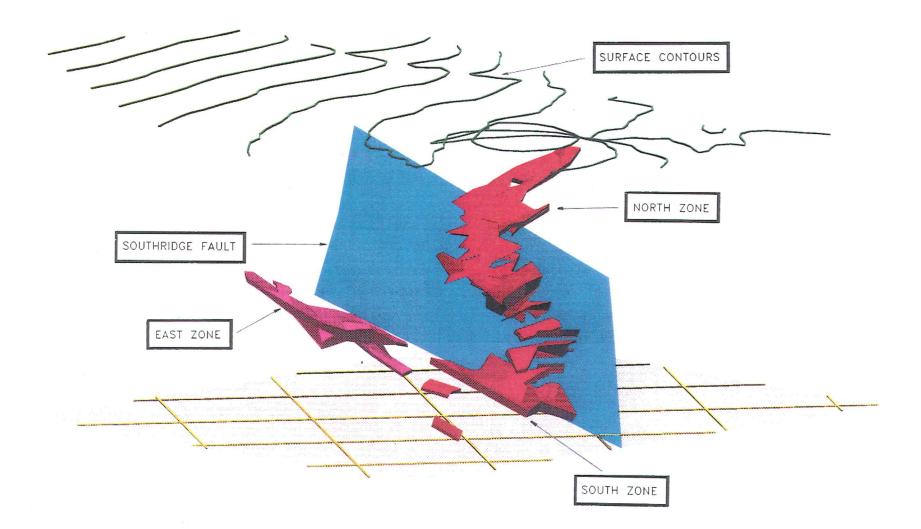
July 1992

TABLE OF CONTENTS

EXECUTIVE SUMMARY

1.0	INTRO	DUCTION	1
	1.1 1.2 1.3 1.4	Study Purpose and Scope Location and Topography Previous Studies Basis for Study	1 2 2 6
2.0	GEOLO	DGY	7
	2.1	Geological Setting	7
	2.2	Mineralization	8 9
	2.3	Major Structure	9
3.0	GEOTI	ECHNICAL ASSESSMENT	11
	3.1	Guidelines for Mine Design	13
4.0	ORE R	RESERVES	16
	4.1	Geological Reserves	16
	4.2	Mining Reserves	17
	4.3	Cut-Off Grades	19
	4.4	Grade Control	21
	4.5	Exploration Program	22
5.0	MININ	IG PLAN	23
			23
	5.1	Mining Methods	23
		5.1.1 Factors Affecting Selection	24
	5 0	5.1.2 Design Considerations	25
	5.2	Cut & Fill	26
		5.2.1 Stope Layout	26
		5.2.2 Stope Access5.2.3 Stoping Method	27
	5.3	General Mine Layout	29
	5.5	5.3.1 Underground Haulage	31
	5.4	Mine Extraction Sequence	31
	5.5	Production Rate	31
	5.6	Construction Services	33
	5.7	Ventilation System	34
	5.8	Maintenance & Power	34
	5.9	Mine Drainage	35
	5.10	Equipment	35

6.0	MILL .	AND SURFACE INFRASTRUCTURE	37
	6.1 6.2 6.3	Mill Surface Infrastructure Tailings Disposal	37 37 39
7.0	MANI	POWER RESOURCES	40
	7.1 7.2 7.3 7.4 7.5	Mining Maintenance Department Mill Administration Productivity	40 43 43 44 44
8.0	PROJ	ECT SCHEDULE	47
	8.1 8.2 8.3	Rate of Production and Resource Development Development Program Other Schedule	47 47 47
9.0	OPER	ATING AND CAPITAL COSTS	48
	9.1 9.2 9.3	Operating Costs Capital Costs Comparison of Rosebud Costs with Other Operations	48 50 50
10.0	ECON	NOMIC ANALYSIS	52
11.0	LIST	OF DOCUMENTS REVIEWED	56
		APPENDICES	
1		PREVIOUS STUDIES	
П		GEOTECHNICAL DATA	
Ш		ORE RESERVES AND DILUTION	
IV		OPERATING AND CAPITAL COSTS	
٧		CASHFLOW ANALYSIS	



EXECUTIVE SUMMARY

The Rosebud project is located in an old mining district in Pershing County, Nevada. Following an encouraging reconnaissance program, Lac acquired control of a large package of land in 1988 and identified a gold and silver bearing zone through diamond drilling. The primary ore zone has a strike length of 2000 ft., an average width of 300 ft. and a mean thickness of 40 ft. and lies between elevations of 4400 ft. to 4800 ft. (depths of 800 to 400 ft. below surface). The main ore zone has been divided into three separate zones called the North, South and East.

A number of studies have been carried out on the Rosebud project over the last few years. With the recently completed diamond drilling and reevaluation of the ore reserves, Bharti Engineering Associates Inc. (BEA) were retained to carry out a prefeasibility study on the project.

The terms of reference for the study included a review of the previous information and data with emphasis on geotechnical aspects and mine design, establishing the mineable ore reserves using appropriate dilution and recoveries and preparing an overall production schedule, operating and capital costs and, on this basis, carrying out a financial evaluation for Rosebud. No additional work was carried out on the design of the surface infrastructure or milling at this time and the information used in this report is based on data obtained from previous studies and supplied by Lac personnel.

All costs are in constant 1992 U.S. dollars, unless indicated otherwise.

Geotechnical Assessment

The geotechnical assessment consisted of a site visit to log diamond drill core, examine previous geotechnical reports and information and the underground exposures at an old, abandoned mine near Rosebud which was still accessible for inspection. The ground conditions at Rosebud depend on the degree of alteration, which varies throughout the three main zones. Unsupported spans of up to 40 ft. are possible in the unaltered East Zone while stope spans as narrow as 15 ft. will have to be maintained in the altered sections in some areas in the South Zone. Ground support will be required as mining progresses.

The overall conclusion of the geotechnical evaluation is that, although ground conditions will vary, proven methods such as cut-and-fill and blasthole can be employed with the proper ground support and an optimum mining sequence.

Mineable Reserves

The mineable reserves were calculated at a 0.10 and 0.15 oz/t cut-off. The mineable reserves are based on the original geological reserves supplied by Lac's Reno offices. Mineable outlines were identified at a minimum mining width of 10 ft. The undiluted mineable reserves were then calculated by Lac's Reno office with BEA finalizing the mineable reserves by incorporating dilution and recoveries.

		@ 0.10 OZ/T C	0.15 OZ/T CUT-0FF		
ZONE	DILUTION	MINEABLE TONS	GRADE OZ/T	MINEABLE TONS	GRADE OZ/T
South	28%	950,000	0.212	774,000	0.239
East	23%	460,000	0.284	388,000	0.298
North	31%	194,000	0.158	168,000	0.221
TOTAL		1,603,000	0.226	1,330,100	0.247

The project cut-off grade was established at 0.10 oz/t. For mine design and project economics, the base case evaluated was at a mineable reserve of 1.6 million tons @ 0.226 oz/t.

Mine Design

Several mining methods were examined including drift and fill, cut and fill and blasthole. The cut and fill mining method with high density full stream tailings backfill was selected as the most appropriate method. This method has the flexibility to adjust stope dimensions and the mining configuration to suit the relatively complex geometry of the different zones at Rosebud.

The basic approach would be to use transverse cut-and-fill mining with primary and secondary stopes with stope widths varying from 10 ft. in the Upper South Zone to as wide as 30 ft. in the Lower South Zone. Typical cut heights would be 15 ft. The stopes would be accessed using ramp entry and slash with backfill being placed within 3 ft. of the stope backs.

High density hydraulic fill has been selected because it permits full stream tailings to be placed at close to 80% density and, therefore, reduces the need for fill fences and drain towers. In addition, over 50% of the waste rock from stoping would be placed back in the mined out stopes. This approach is considered better than the previous concept of using a slinger truck with waste rock, which is more expensive and also requires careful scheduling and crushing of the waste rock. Conventional hydraulic fill cannot be used because the classified portion of the fines is not adequate to replace the mined out ore.

The orebody would be accessed by a ramp from surface with the ore hauled in 15 ton trucks and delivered to the mill on surface. An economic comparison of the ramp vs. shaft option indicates that the ramp provides more flexibility and requires less time at comparable cost.

The optimum production rate is considered 1000 tpd on two shifts, 5 days/week with the mill operating at 750 tpd, 350 days/year. The limited mineable reserve precludes a higher production rate that can realistically be sustained. This is based on a mineable reserve of 1.6 million tons at a 0.10 oz/t cut-off. The option of mining at 750 tpd at a higher cut-off of \$0.15 oz/t (mineable reserves 1.3 million tons) on 2 shifts, 5 days a week was also evaluated.

Mill and Surface Infrastructure

The mill design would be identical to that used in previous studies and was discussed with George Hope of Lac Minerals. The estimated capital costs for the mill are \$9.5 million with recoveries of between 84.5% in the North Zone to 91.0% in the South and East Zones. The current mill design calls for extraction using a carbon and leach plant with gravity separation. The operating costs are estimated at \$13.50/ton.

The surface infrastructure is similar to that proposed by Dynatec in a February 1992 study. Tailings disposal will take place southwest of the plant and mine portal with an estimated storage capacity of about one million tons. A three pond configuration will be used for the tailings dam.

Manpower, Costs and Productivities

The total estimated mine workforce is as follows:

Department	Number
Mining	78
Maintenance	17
Milling	25
Administration	12
GRAND TOTAL	132

The overall mining productivity (tons/manshift delivered to the mill) is slightly over 11. This compares well to existing experience at small Canadian operations.

The mine operating costs were estimated from basic principles using an in-house BEA program. The labour rates and material costs used were obtained from Lac's Bullfrog mine. Operating costs for the mill and tailings were obtained from George Hope of Lac and previous studies. The estimated capital costs were based on current equipment costs and estimates previously used for the mill and surface infrastructure. All costs are in constant 1992 U.S. dollars. The capital and operating costs are summarized below:

OPERATING COST SUMMARY

MINING COSTS

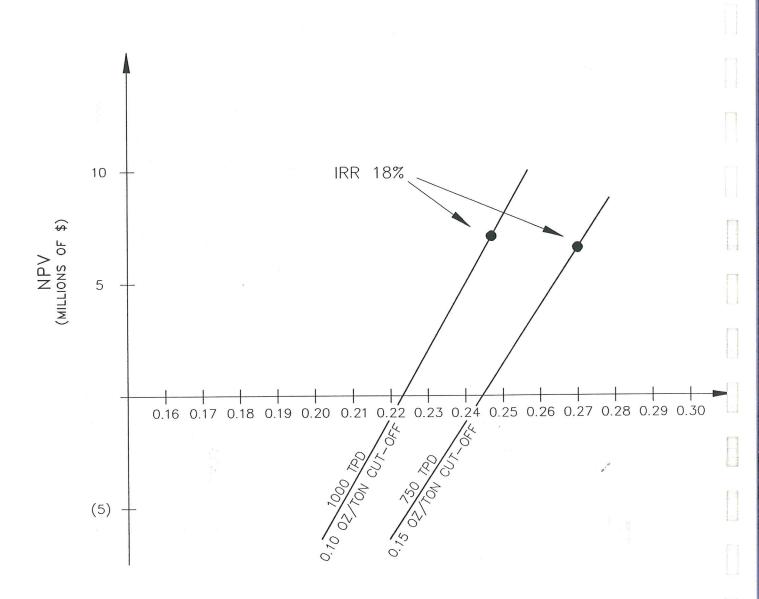
	Pre- Production	Production		
Item	Cost	Cost	Cost/Ton	
Labour	\$6,539,000	\$26,596,000	\$15.20	
Materials	\$2,780,000	\$7,464,000	\$4.27	
Equipment	\$1,550,000	\$11,886,000	\$6.79	
Other Charges	\$2,775,000	\$16,464,000	\$9.40	
Total	\$13,644,000	\$62,410,000	<i>\$35.66</i>	

TOTAL SITE COSTS

	Cost/t
Mining	\$35.66
Milling	\$13.50
Tailings	\$0.40
Administration	\$1.80
TOTAL	\$51.36/ton

Although the mine operating costs for Rosebud were calculated independently, they are similar to current operating costs at Bullfrog's underground mine (\$38.16/ton).

NPV vs. Mined Grade



MINED GRADE (OZ./TON)

CAPITAL COSTS (TOTAL COST \$000's)

	Capital Cost \$000's	Total Life \$000'S
Development Pre-production (9000 ft. ramp, 1,000 ft. raise)	5,084	8,171
Mining Equipment	7,218	7,218
Plant (Mill)	9,500	9,500
Tailings Dam	2,500	2,500
Infrastructure and Surface Equipment	2,958	2,958
Diamond Drilling	1,000	1,000
Environmental and Permitting	500	500
EPCM 10%	3,100	3,100
Closure	-	500
TOTAL	\$31,860	\$35,447

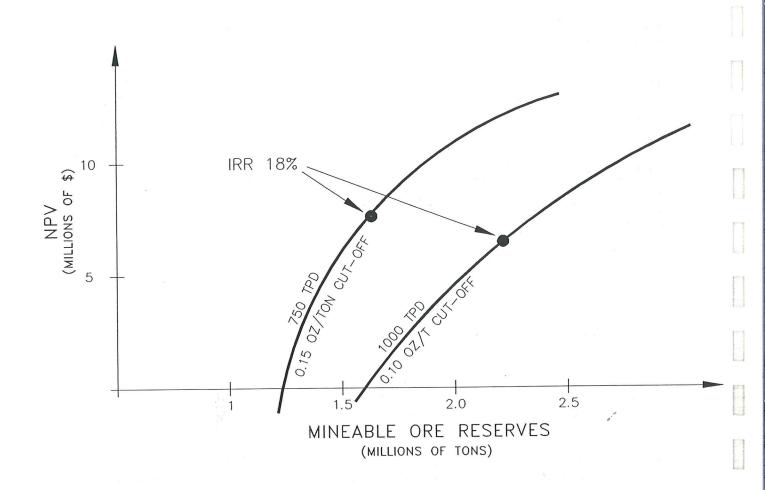
Financial Evaluation

A total of 24 different options were evaluated for the Rosebud project. All alternatives were carried out at a base case gold price of \$360/oz at a 10% discount rate. All costs and analyses are in constant 1992 U.S. dollars. Depreciation and taxes were not included. The following alternatives were examined:

- ♦ Base case options of 1,000 tpd (250,000 tpy) and 750 tpd (187,500 tpy) at cut-off grades of 0.10 and 0.15 oz/t respectively. Both these options are considered realistic and achievable using current mineable reserves at the two cut-off grades.
- Sensitivities were carried out to cut-off grades, gold price and total mineable tonnage.
- Sensitivities were also carried out on the 750 tpd option to project capital and operating costs.
- An evaluation of the impact of the maximum possible production rate (350,000 tpy at 0.10 oz/t cut-off and 262,000 tpy at 0.15 oz/t cut-off) was also conducted although these production rates may be difficult to achieve and sustain at the current level of mineable reserves.

The complete economic analyses are presented in Section 10.0 of the report and backup spreadsheets are included in Appendix V. The main conclusions of the financial evaluation and sensitivities are as follows:

NPV vs. Mineable Reserves



MINIMUM MINEABLE ORE RESERVE FOR 18% IRR 1.6 MILLION TONS @ 0.15 OZ/T CUT-OFF 2.2 MILLION TONS @ 0.10 OZ/T CUT-OFF

- 1. Sensitivities to changes in grade, gold price and ore reserves are shown on the attached figures for production rates of 1000 tpd and 750 tpd at cut-off grades of 0.10 and 0.15 oz./ton, respectively. Project economics are significantly enhanced by increasing the ore reserves by between 300,000 to 600,000 tons and improve dramatically when the ore reserves are increased by an additional one million tons at the current mineable grades.
 - Grade changes and gold price also affect the NPV and can change it from \$7 million to a negative NPV of over \$6 million.
- 2. The base case options of 750 tpd and 1000 tpd at the two cut-off grades are marginal and have an NPV of less than \$1 million and an internal rate of return (IRR) of 11%. These options therefore cannot form the basis on which to proceed at Rosebud.

Split Between Lac and Equinox

The split on capital and gold produced between Lac and Equinox, based on the 1000 tpd option at the 0.10 oz/t cut-off, is as follows:

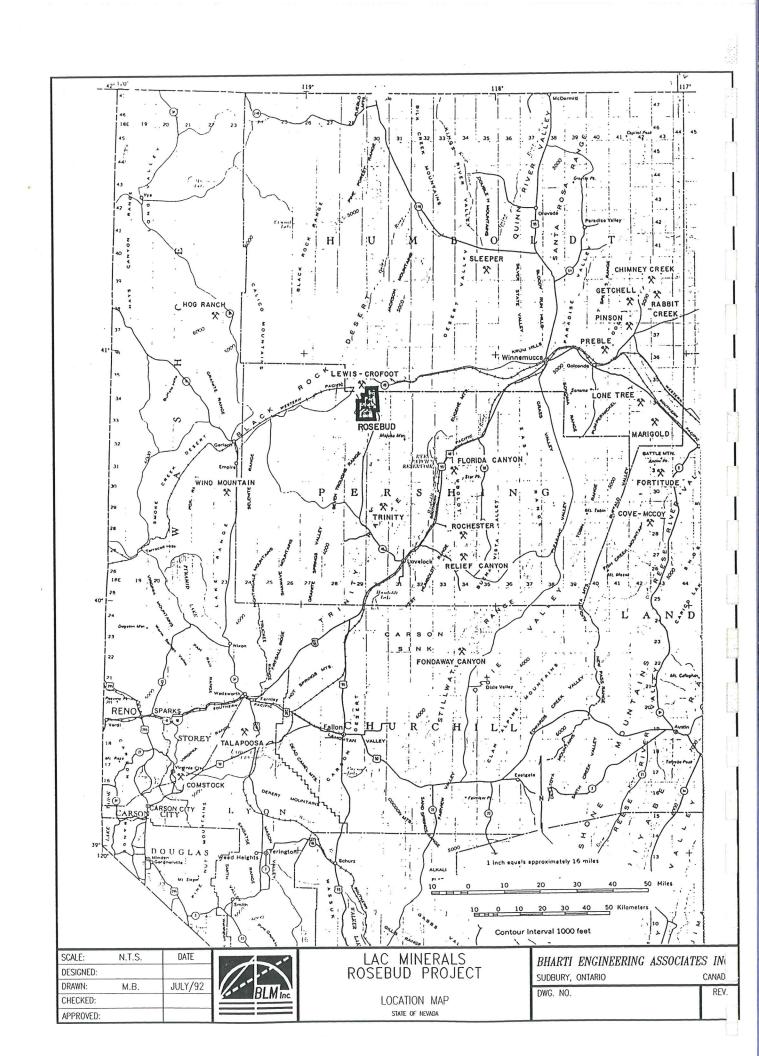
SPLIT BETWEEN EQUINOX AND LAC @ 1000 tpd (250,000 tpy), 0.10 oz/t cut-off				
	LAC	EQUINOX	TOTAL	
Pre-production Capital (Millions of \$)	20.7	11.2	31.9	
Gold Produced - total over mine life - avg. oz/year	233,815 29,227	128,279 16,034	362,094 45,262	
Mineable Reserves			1,603,000	

Conclusions and Recommendations

The main conclusion of the prefeasibility study is that the Rosebud project does have potential, but requires increased ore reserves and/or higher mineable grades. Lac geologists have a high degree of confidence in the estimated mineable grade. BEA believes the grade may be somewhat conservative because of the dilution used and opportunities may exist to further enhance the ore grade as mining progresses. Both the capital and operating costs have been estimated from basic principles and are considered reliable and accurate to a range narrower than the +/-25% level generally used for prefeasibility studies.

In order to obtain an acceptable rate of return of at least 18%, the terms of reference for any follow-up work at Rosebud should be based on:

- ♦ A production rate of 1000 tpd and 250,000 tpy at a 0.10 oz/t cut-off.
- A mineable reserve base of between 2-3 million tons (an increase of about one million tons over the current mineable reserves).
- The price of gold being maintained at least in the \$350 to \$360/oz range and preferably being in the \$400/oz range.





1.0 INTRODUCTION

The Rosebud prospect is situated in an old mining district in Pershing County, Nevada. Various periods of mining activity have been experienced in the area, mainly during the 1910's and the 1930's. However, the output of gold was limited to no more than a few thousand ounces which were extracted from narrow high grade veins.

Lac Minerals (USA) Inc. following an encouraging reconnaissance program, acquired control of a large package of land in 1988 through both negotiation with various claim holders and placing claim stakes. Subsequent exploration work involving both reverse circulation boreholes and diamond drill boreholes has identified a gold and silver bearing resource known as the Rosebud Property. The primary ore zone has a strike length of 2,000 ft., an average width of 300 ft. and a mean thickness of 40 ft. and lies between the elevations of 4,400 ft. and 4,800 ft., corresponding to depths of 800 ft. and 400 ft. respectively. Gold has been intersected in other parts of the property (Figure 1).

A number of studies have been carried out in the intervening years covering hydrological, geotechnical, metallurgical and financial aspects of the prospect. With the recently completed diamond drilling from surface, Lac Minerals Limited wish to establish whether the resource, as currently defined, can be profitably extracted through the development of an underground mine. Bharti Engineering Associates Inc. (BEA) have been engaged to perform a pre-feasibility study of the Rosebud project.

1.1 STUDY PURPOSE AND SCOPE

The specific terms of reference and scope for the study were defined by Mr. Bill Quesnel of Lac Minerals, as outlined below.

- 1. Review previous information and studies carried out on the Rosebud project with particular emphasis on the geotechnical aspects.
- 2. Examine the previous geotechnical work completed by Lac personnel and consultants and supplement it with additional analyses, as appropriate.
- 3. Review the existing geological ore reserves, establish appropriate dilution and recoveries based on the proposed mine plan and ground conditions and establish a mineable reserve at different cut-off grades.
- 4. Prepare a mine plan and overall approach for recovery of the Rosebud resource including the optimum production rate, cutoff grade, mining methods, manpower and equipment requirements and operating and capital costs.

- 5. Summarize the surface infrastructure, milling and other site property costs based on previous studies carried out by Lac Minerals and consultants after discussions with appropriate Lac personnel.
- 6. Based on the above data, establish total site operating and capital costs and conduct economic analyses to determine project economies, including sensitivities and define the framework required for Rosebud to be a viable project.
- 7. Recommend a follow-up program for Rosebud.

The work performed by BEA included a site visit during the week of May 21 by Stan Bharti and Dave West (BEA) with Bill Quesnel and Richard Hong (Lac Minerals) and to Lac's Reno offices to review the geological and ore reserve information, examine the available diamond drill core, analyze the previous geotechnical work carried out and obtain a general appreciation of the minesite. Messrs Bharti and Quesnel also visited Lac's Rosebud Mine in Nevada. The purpose of the visit was to obtain current labour rates and material costs applicable to Rosebud and to examine the ground conditions at Bullfrog. Dave West and Richard Hong also conducted additional geotechnical analyses and core logging at Lovelock, Nevada on the Rosebud project at this time.

1.2 LOCATION AND TOPOGRAPHY

The Rosebud property is located at the base of Rosebud Peak, at 5,000 ft. to 5,500 ft. above sea level, with limited scrub vegetation, some 55 miles north of the town of Lovelock, Pershing County, Nevada. The topography of the site is characterised by medium relief terrain. The Rosebud deposit is situated on Bureau of Land Management land within the claim boundaries of Lac Minerals (USA) Inc., Equinox Resources Limited and Degerstrom. Gold mining has been carried out only sporadically since the early part of the century. Access to the project site is gained via a gravel road from Lovelock. The main Western Pacific rail line lies adjacent to the Hicroft mine, positioned approximately 10 miles to the north of the Rosebud property. The Southern Pacific rail line services the town of Lovelock in the south.

1.3 PREVIOUS STUDIES

Several previous studies dating back to 1990 have been carried out on the Rosebud project. A list of the documents supplied by Lac Minerals is attached at the end of this report (Section 10.0). A summary of the previous documentation, which was reviewed by BEA, is attached in Appendix I and briefly discussed below.

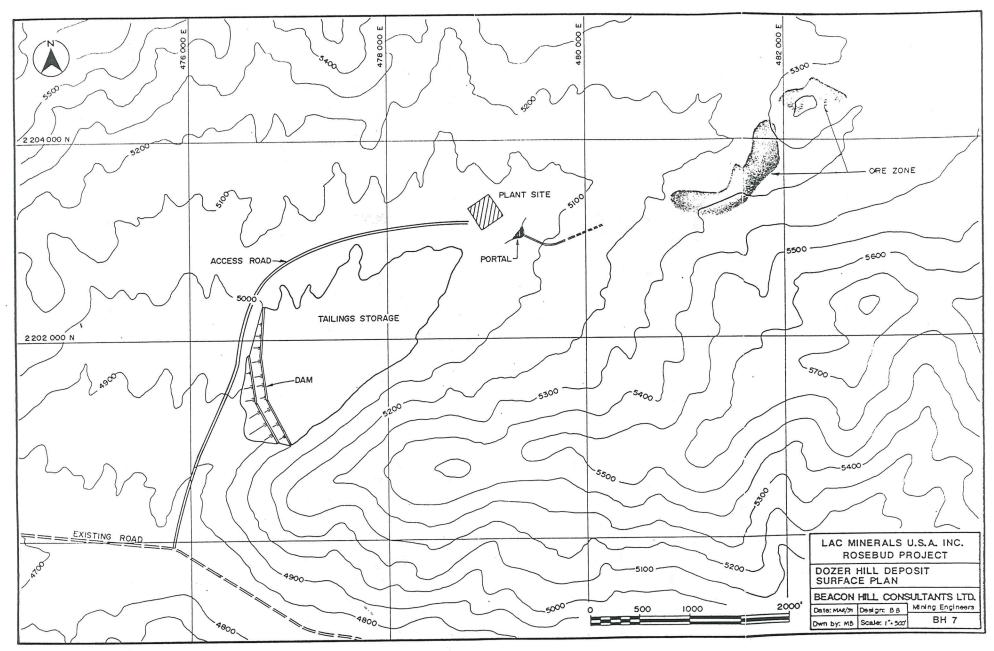


Figure 1

ENVIRONMENTAL STUDIES

Hallam Knight Piesold Limited have reviewed the environmental work and believe that project permitting should be approached on the basis of a full Environmental Impact Statement (EIS) for both the state and federal requirements. A Plan of Operations for underground exploration activities has already been submitted by Lac to the U.S. Department of the Interior (Bureau of Land Management). No major difficulties with environmental permitting are anticipated.

GEOTECHNICAL STUDIES

Several geotechnical and hydrogeological studies have been carried out by Piteau, Golder Associates, Hydro-Geo Consultants and in-house by Lac personnel.

These studies show that the ground varies from unaltered competent ground (fair to good condition) to very poor with an average fracture count of up to 2 per ft. and as high as 4 fractures per ft. in heavily altered zones. Selective methods are likely to be used with extensive ground support.

RESERVES AND EXPLORATION

Several estimates on the geological and mineable reserves have been carried out. The most recent work was completed by Lac Minerals (USA) Inc. from their Reno offices. The reserves are based on the ground jointly owned by Lac and Equinox. The estimated reserves are as follows:

- ♦ 5.2 million tons @ 0.11 oz/ton @ a 0.02 oz/ton cutoff
- ♦ 2.2 million tons @ 0.21 oz/ton @ a 0.05 oz/ton cutoff

These estimates do not include any dilution or ore losses.

Beacon Hill Consultants of Vancouver estimated the probable mining reserves in March 1991, with an allowance for 15% dilution, at 1.15 million tons at a grade of 0.24 oz/ton. The most recent calculations of the Rosebud reserves (January 3, 1992) indicate an in-situ resource of approximately 2 million tons at 0.25 oz./ton.

Previous studies have also recommended that an exploration program be carried out by developing a ramp and two drifts. This would permit diamond drilling and obtaining a bulk sample from the underground workings.

MINING

Beacon Hill Consultants (March 1991) selected drift and fill mining as the most appropriate technique given the assessment of rock quality and the configuration of the orebody. Drift and fill is highly selective and provides the most effective ground support for the stopes with widths of 13 feet. The stopes would be filled using a Slingerbelt truck with minus 2 inches crushed rock with 5% cement content. The general mine layout would incorporate both a ramp for haulage and a shaft for hoisting once truck haulage becomes uneconomic. A production level of 500 tons/day would need 4 or 5 active faces.

Two production scenarios have been evaluated by Beacon Hill:

DEPARTMENT	SCENARIO 1	SCENARIO 2	SHIFT SYSTEM
Mining	700 tpd	1,400 tpd	2 shifts per day 5 days per week
Milling	500 tpd	1,000 tpd	3 shifts per day 7 days per week

The report concluded that viability of the Rosebud project would depend on:

- Control of dilution to maintain ore grade.
- 2. Choice of selective mining methods to cater for changes in width of orebody.
- 3. Installation of appropriate ground support, coupled with a well engineered mine extraction sequence to manage the changing ground conditions.

MILLING

Limited metallurgical testwork carried out by Lac indicates that gold can be successfully extracted with a Carbon-in-Leach plant with gravity separation. Metallurgical recovery is expected to range between 85% and 90%.

Initial tests indicate that the ore is very amenable to cyanidation with good recovery and low cyanide consumption. Subsequent work pointed towards leaching problems, possibly brought about, in part,

by the presence of gold encapsulated in sulphides. Antimony may also create difficulties with recovery of gold.

A SAG mill would be needed for the 1,000 tons/day milling operation. Water requirements are gauged to be 200 gpm.

Tailings disposal would take place southwest of the plant and mine portal with storage of 3 million tons (related to a mill throughput of 350,000 tons/year), demanding an area of 1,530 acre-ft., incorporating a three pond configuration.

CAPITAL AND OPERATING COSTS

Operating costs have been estimated from \$70/ton to \$57/ton for the 500 tpd option and 1,000 tpd option, respectively, in 1991 \$ (Beacon Hill). The capital costs range from \$27.2 million to \$35.2 million for the 500 tpd option and the 1,000 tpd option, respectively (1991 \$).

DISCOUNTED CASHFLOW

Beacon Hill Consultants found the project to be:

most sensitive to grade and gold price less sensitive to operating costs least sensitive to capital expenditure.

The Beacon Hill Consultants alternative cases for evaluation were based upon a gold price of \$375 per oz. and metallurgical recovery of 89%.

The 500 tpd option would be uneconomic, and to be viable would require a:

10% increase in grade10% reduction in capital expenditure, and20% decrease in operating costs.

The 1,000 tpd option would be economic, but is based upon a doubling of the reserves.

Beacon Hill Consultants assessed the value of the property by two methods which indicated a range of 6 million to 10 million. The market value method (accurate to +/-25%), assumes gold at 10/0z. of gold and land at 500/acre.

A recent evaluation (January 17, 1992, Hans De Ruiter - Lac), using an uncut high grade (0.31 oz. Au per ton) and assuming a metallurgical recovery of 92% indicates a significant improvement in the financial return of the project, given the 50% increase in grade (from the cut grade of 0.226 oz. Au per ton), at a gold price of \$350/oz. and a 15% discount rate. The economics are summarized below:

High Grade:

26% IRR and \$7 million NPV

Cut Grade:

(4%) IRR and (\$13 million) NPV

1.4 BASIS FOR THE STUDY

The basis for the present study is to review and evaluate the geotechnical and mining aspects of Rosebud on the following basis:

- 1. Lac Minerals (USA) Inc. (Reno office) would provide the undiluted ore reserves and calculate the mineable ore reserves based on BEA mining outlines.
- 2. Only cut grades would be used in the analysis. The uncut grades could significantly bias the results, since one portion of Rosebud contains an exceptionally high component of the ounces.
- 3. The milling information (operating and capital costs and recoveries) would be provided by George Hope of Lac Minerals.
- 4. The cost of the surface facilities and the general layout would be based on previous studies by Beacon Hill and Dynatec.
- 5. The labour rates and material costs would be based on Lac's Bullfrog mine.
- 6. All costs are in constant 1992 \$. Metal prices to be used were obtained from Paul Martin of Lac and are \$360/oz for gold and \$4/oz for silver.
- 7. All costs shown are in U.S. dollars.

2.0 GEOLOGY

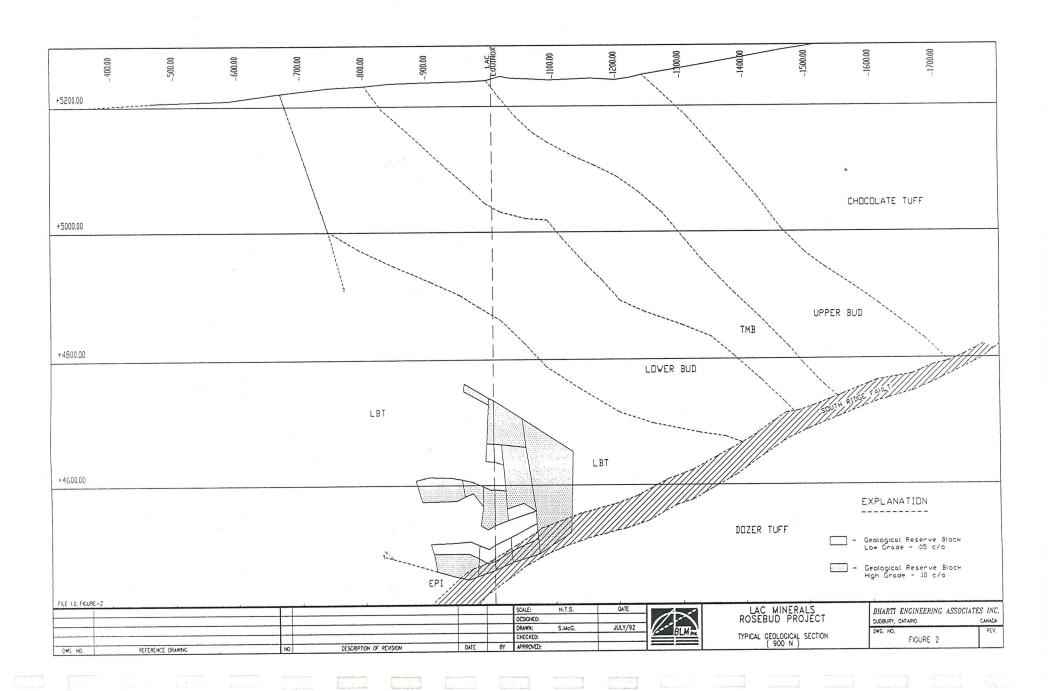
2.1 GEOLOGICAL SETTING

The predominant rocks in the Rosebud area, the Kamma Mountain Group, are of Tertiary age and consist of a thick sequence of rhyolite and latite flows, tuffs, and pyroclastic rocks. The Kamma Mount Group has been informally divided into seven units.

The basal unit, the Dozer Tuff, consists of a pale green to grey fine-grained densely welded rhyodacitic tuff or flow which is in excess of 1,000 ft. thick. The Dozer Tuff is present in the subsurface throughout the project area in the immediate footwall of the South Ridge Fault. Some mineralization of this unit occurs in the East Zone, approximately 50 ft. below the South Ridge Fault. The unit is generally massive, bleached and pervasively silicified.

The Lower Bud Tuff (LBT) overlies the Dozer Tuff and comprises dense red-brown to tan-grey volcanoclastic rocks and fine-grained to banded tuffs and flows, and locally, is as thick as 900 ft. The LBT is the primary host for mineralization in the South and North Zones. Clay and sericitic alteration is widespread in the South Zone, but less prominent elsewhere. The principle alteration product is thought to be kaolinite. Bleaching and clay alteration are frequently present in the zone of mineralization, but vary substantially in intensity. Subparallel waxy green clay seams, typically 1/4-inch in thickness and spaced at intervals of several inches, occur as alteration products infilling fractures locally within the LBT, and may be indicative of fault zones. These seams constitute low strength zones within the LBT and are locally referred to as "duck butter". Their preferred orientation is unknown. The distribution of duck butter zones to mineralized zones is poorly defined, but they constitute a relatively small percentage of the LBT. Duck butter zones typically occur over intervals of 10 feet. Natural fracture surfaces observed elsewhere in the unit do not generally contain clay alteration products or low strength materials.

The Bud Volcanoclastic unit is composed of a bedded lithic Lapilli Tuff, rich in green celadonitic clay and interbedded epiclastic tuff. This unit ranges from less than 100 ft. to 600 ft. thick and is of limited lateral extent across the project area. Upper and lower members of the Bud Volcanoclastic unit are separated by a Tuff Marker Bed (TMB). The TMB is a grey fine-grained porphyritic tuff that has a higher strength than the Bud. The TMB unit ranges in thickness from 50 ft. to 250 ft. A lack of mineralization is interpreted to result from a plastic response to hydrothermal alteration which prevented fracturing and pathways for mineralizing solutions.



The Chocolate Tuff overlies the Bud and is a maroon to grey, moderately to densely welded, latitic to rhyolitic flow-banded tuff with interbedded volcanic breccia. This unit ranges in thickness from 500 ft. to 800 ft. in the project area. It is generally distinguished from the LBT only by its stratigraphic location, its geological and mechanical characteristics are essentially identical to the LBT.

The Badger Formation unconformably overlies the Chocolate Tuff, and represents the waning stages of Kamma volcanism. It consists of a series of volcanic conglomerates, sandstones, and some intermediate flows.

Quaternary sediments occur as alluvial fan deposits surrounding Dozer Hill and flanking the Kamma Mountain volcanic sequence. Alluvial deposits occur along the axis of the Rosebud Canyon. The alluvial deposits are typically less than 50 ft. thick.

The lenticular orebodies at Rosebud occur primarily within a sequence of Miocene volcanic and pyroclastic rocks (Lower Bud Tuff), which have variable strength, degree of alteration and fracturing. Alteration by silicification and by bleaching and argillicification have both strengthened and weakened the rock mass. A shallow dipping thrust fault, the South Ridge Fault, defines the bottom of the Lower Bud Tuff. The South Ridge Fault is characterized by a zone of intensely sheared and altered rock of low quality, ranging in thickness from 5 feet to 60 feet. The Dozer Tuff zone, generally less altered and more competent than the Lower Bud Tuff, lies below the fault. The Bud Tuff overlies the Lower Bud Tuff, and like the Dozer Tuff, is more competent than the Lower Bud Tuff.

There appears to be no clear relationship between the ore zones and rock mass quality. No structural information is available within the mine area. The water table lies 200 feet below surface. Otherwise groundwater conditions within the rock mass or along faults are unknown.

For exploration purposes, the mineralogical lenses have been subdivided into the South Zone, North Zone and East Zone. The extent of each lens has been clearly defined by surface drilling, however, additional mineralization may lie to the east of the East Zone (Figure 2).

2.2 MINERALIZATION

Gold concentrations occur at the nearby Dreamland and the Hycroft properties, in large, irregular, very non-homogeneous areas of gold mineralisation, each comprising several tens of millions of tons with gold content averaging from 0.01 oz Au/t to 0.03 oz Au/t. Higher grade pods exist within these areas with resources ranging from a few thousand tons to a few million tons with gold grades from 0.1 oz

Au/t to 0.4 oz Au/t, similar to the Aurora, Rawhide, Borealis and Bodie deposits.

Mineralization in the Rosebud deposit is characterized by up to four stages of discontinuous stockwork veins of quartz, calcite and clay. Sulphide content ranges from three to five percent as pyrite, marcasite, and trace amounts of chalcopyrite and sphalerite. Such levels of sulphides will require treatment with lime in the surface recovery process. Gold and silver minerals include electrum, aurian silver, naumannite, and argentite. These veins crosscut bleached, clay-altered and sericitized flows and tuffs.

2.3 MAJOR STRUCTURE

The regional structure of the area is dominated by north to northeast trending normal faults that are down-thrown to the west. Also, extensional tectonism has created a complex series of significant structures which consist of northeast to east trending, high and low angle faults, including the Rosebud Shear Zone and the South Ridge Fault. The Rosebud Shear Zone trends in an eastnortheast direction. This steeply dipping fault system is up to 300 ft. wide. The South Ridge Fault is a complex eastnortheast trending (N 60 E) zone that ranges in thickness from 5 ft. to 60 ft. The zone dips northward at less than 45 degrees and exhibits apparent left lateral, oblique slip movement. This fault has been mapped throughout the project area; however, its length and extent of displacement are still under investigation.

In the vicinity of the South Zone, the South Ridge Fault (SRF) consists of 10 ft. to 20 ft. of weak green clay gouge containing clastic fragments of calcite. Rubble zones are described over 20 to 80 percent of the diamond drill intersections of the fault zone at this location. Mineralization in the South Zone lies predominantly within the hangingwall of the fault, any limited mineralization that occurs within the fault zone is generally of low grade.

Towards the north of the South Zone, clay and silica alteration replace calcite in the fault zone. The fault thickness increases to a total thickness in the order of 40 to 50 ft. and is characterized by interlayed silicified breccia and gouge. Two separate fault zones are commonly identified, with each zone comprising a silicified (hydrothermal) breccia overlying a gouge zone. Hydrothermal breccia constitutes a massive, competent, high strength component of the fault unit. Again, mineralization occurs predominantly within the hangingwall of the fault within the LBT, with only sparse, low grade mineralization occurring within the South Ridge Fault.

The South Ridge Fault is typically about 20 ft. wide in the North ore zone, and is characterized by a

predominance of very competent hydrothermal breccia (typically about 70 percent of the fault zone) interlayered with soft clay gouge and rubble contained within a clay matrix. Mineralization occurs predominantly within the hangingwall of the fault, with little mineralization within the fault zone at this location.

In the East Zone, the South Ridge Fault thickens to approximately 60 vertical feet. The fault zone consists of competent hydrothermal breccia. Mineralization occurs within the fault zone and in the footwall Dozer Tuff.

A number of northwest-southeast trending structures have been inferred from diamond drill interpretation resulting from sharp changes in the elevation of marker beds throughout the stratigraphic sequence. To date no borehole has clearly defined any of these cross-cutting structures as the holes have been drilled either to the southeast or vertically. However it is believed that these structures have influenced the distribution of ore and may provide active conduits for groundwater flow. Additional drilling is required to adequately define and locate these structures.

A limited number of rubble and gouge zones have been observed from the geological and geotechnical logs. These zones occur sporadically throughout all the lithologic units, and possibly represent former local centres of brittle and plastic deformation in response to hydrothermal alteration. Both the rubble and gouge zones form discontinuous areas of weakness within the rock mass. Both types are of limited thickness, typically one to two feet, the orientation and continuity of these zones are poorly defined.

3.0 GEOTECHNICAL ASSESSMENT

An in-depth geotechnical assessment of the Rosebud project was carried out to ensure that the subsequent mine design could be optimized and the selected mining method, ground support requirements and overall sequencing were realistic enough to be able to produce a reliable production schedule and operating costs. The geotechnical work involved the following:

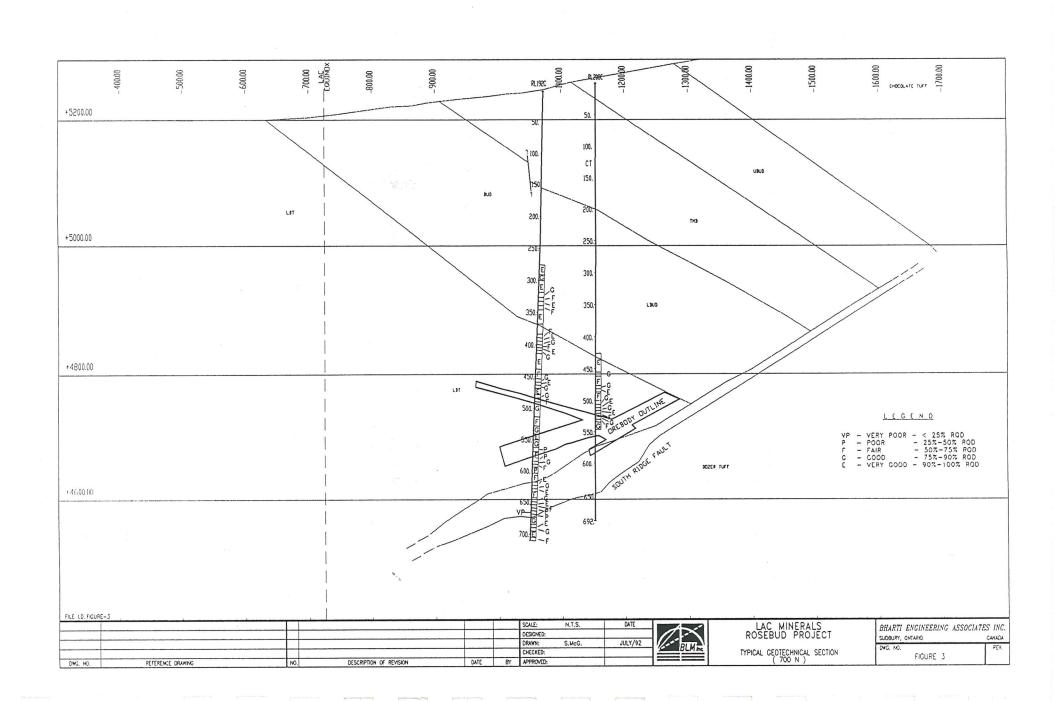
- 1. A review of all the previous documents and studies carried out by several consultants on both the hydrology and rock mechanics.
- 2. A review of the work completed by Lac Minerals personnel from the Kirkland Lake office on geotechnical logging and analysis of the data.
- 3. A site visit by the BEA geotechnical engineer, together with Lac personnel, to examine the available core and carry out additional geotechnical logging, as necessary, for the follow-up analysis.
- 4. A site visit to Dreamland Mine, located several thousand feet west of Rosebud that had been mined several years ago but was still available for inspection.
- 5. Previous tests on intact rock strengths were reviewed and summarized and additional testwork recommended. The additional testwork is currently in progress at the MacKay School of Mines in Reno.

The above information was used to prepare detailed geotechnical sections of the ground conditions jointly with Lac personnel at their Kirkland Lake offices. The information used in preparing this data was based on the previous work done by Lac and the additional work carried out for this prefeasibility. The detailed geotechnical evaluation is attached in Appendix II, together with the geotechnical sections showing ground conditions and logs of the Rock Quality Designation (RQD). A typical example is shown on Figure 3.

A summary of the rock mechanics factors affecting ground conditions and the recommended guidelines for mine design are presented below.

Hydrology

The hydrogeological characteristics of the project area have been examined by Hydro-Geo Consultants of Lakewood, Colorado. The work involved field testing of three monitoring wells and one borehole for permeability and falling head and pumping tests on designated holes. No additional work was carried out by BEA.



The hydrogeology study concludes that the total mine inflow is estimated to range from 100 to 500 gpm. Complete drainage of the orebody hangingwall may not be possible using drainholes drilled for the deep line and a second dewatering system of vertical wells drilled from surface may be required. High inflows can be anticipated when intersecting the South Ridge Fault. Two additional test boreholes were recommended for further evaluation of the potential high inflow areas in the South Zone and the East Zone.

BEA believes that groundwater in most underground mines does not present serious stability problems as long as adequate pumping capacity is provided. The underground development at Rosebud will provide adequate opportunities to carry out drainage, with drainholes if required, to ensure that overall stability is not jeopardized.

Ground Conditions

The anticipated ground conditions are based on visual observations of exposures at Dreamland Mine, geotechnical core logging and experience with underground operations at Bullfrog, where ground conditions are expected to be somewhat similar to those at Rosebud.

Exposures at Dreamland indicate that stope spans of up to 60 ft. in area can be sustained without significant ground problems. The stopes had been open for over 50 years without any indications of major instability.

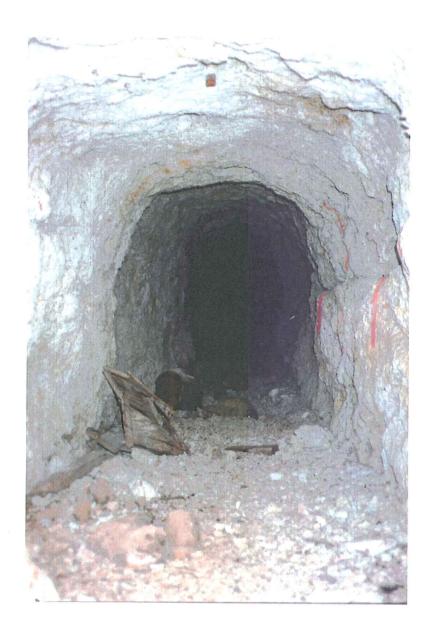
The Dozer Hill drift is an approximately 6 x 5 ft. unsupported drift through the Bud unit into the LBT. It is located within Dozer Hill, which directly overlies the North mineralized zone. The Bud is predominantly unmineralized, low strength geotechnical unit, while the LBT is the primary host for mineralization in some ore zones. There is no significant instability throughout the several hundred feet of drift length. The drift is dry.

A visual classification of the rock quality in both areas is generally fair to poor - based on the amount of fracturing evident in the excavation walls. It appears to be more fractured than the typical competent LBT inspected in drill cores and core photographs pertaining to the Rosebud/Dozer Hill project.

Point load test results indicate that the rock strengths at Rosebud typically range from 2000 to 15,000 psi with the unaltered or solicified rocks having the higher strength values.



EXPOSURE AT DREAMLAND MINE



DOZER HILL DRIFT

The estimated rockmass quality for the Rosebud project is summarized below.

TABLE 3.1

ROCK MASS QUALITY, ROSEBUD PROPERTY				
GEOLOGICAL SEQUENCE	ROCK MASS QUALITY			
Bud Tuff	Good to very good			
Lower Bud Tuff				
Upper Section	Good to fair			
Lower Section	Section 00 to 600 Poor to very poor			
	Sections 600 to 1600 Fair to good (some poor zones) Poor within 50 ft to 75 ft. of fault			
Dozer Tuff	Fair to good			

Based on the NGI classification, which has been modified to reflect any areas which contain reduced rock strength, it is suggested that:

- Very poor to poor ground conditions apply to the South Ridge Fault and the South ore zone between section 00 and section 600. The hangingwall conditions in this area would be classified as good to fair.
- ♦ Ground conditions in the mineralized Lower Bud Tuff between sections 600 to 1600 are classified as fair to good, with poor ground within 50 75 ft. of the South Ridge Fault. The hangingwall conditions in this area would be classified as good to fair.
- Fair to good ground conditions exist throughout the East Zone.
- The condition of the Dozer Tuff can be described as fair to good throughout the project area.

3.1 GUIDELINES FOR MINE DESIGN

It is envisaged that cut-and-fill is applicable to the South Zone ore between section 00 and section 600. The geological reserve indicates that the thickness of the ore in this area ranges from 10 ft. to 50 ft. vertically. Consequently, the thicker areas of the mineralization could be recovered with

approximately four mining cuts.

From section 00 to section 300, the thinner portions of the orebody, averaging 15 ft. to 20 ft. thick could also be recovered by tight cut-and-fill with breasting. In this area poor to very poor ground conditions are anticipated, therefore, panel widths should not exceed 15 ft. Ground support should generally consist of 8 ft. long mechanical rockbolts installed on an approximate 4 ft. x 4 ft. pattern, using weldmesh as a surface restraint between the rockbolts. A contingency to install friction support (ie. Swellex) and shotcrete will be required in highly kaolinized areas and through the South Ridge Fault.

Dilution in secondary pillar recovery between the primary panels is of concern, particularly in highly kaolinized areas, ie. drainage of groundwater and backfill placed in the primary panels may leach the rock mass. Narrower secondary panels may be required. External dilution in the order of 20 percent may be anticipated.

From section 600 to section 1600 the ground conditions improve and may be described as fair. The provisional extraction widths may be increased to 20 - 25 ft. Short cablebolts will be required as supplementary ground support at the intersections of access development. Poor ground is indicated within 50 ft. to 75 ft. in the hangingwall of the South Ridge Fault. A reduced panel width of 15 ft. may be required for the first two to three cuts where applicable. External dilution of approximately 15 percent is anticipated.

Fair to good ground conditions are indicated in the East Zone between sections NW8 and NW13. The South Ridge Fault consists of a silicified hydrothermal breccia, more competent ground than the clay gouge shear zone below the South and North zones. A provisional extraction width in the order of 30 ft. to 60 ft. may be applied depending on the degree of alteration. External dilution of approximately 15 percent is anticipated.

General guidelines on spans are provided below:

TABLE 3.2

Rock Mass Quality	Unsupported Span (ft)	San With Rock Bolts, Mesh & Shotcrete (ft)
Excellent Unaltered	40 to 45	80
Good Unaltered Altered	40 13 to 20	70 - 80 26 - 33
Fair Unaltered Altered	16 - 25 8 - 9	30 - 40 20 - 26
Poor Altered	5 - 6	20
Very Poor Altered	5	10

As an attempt to minimize external dilution, it is recommended that controlled blasting will be required throughout the development and ore zones.

It should be pointed out that the guidelines presented above are based on geotechnical core logging and limited analysis of the data. Additional work should be carried out for any future feasibility studies which should include identification of clay and friability zones, laboratory testing and appropriate numerical modelling to optimize the mine design.

4.0 ORE RESERVES

4.1 GEOLOGICAL RESERVES

Lac Minerals (USA) Inc. have estimated geological reserves, by the method of sections utilising grade cut offs of 0.02 oz Au per ton and 0.05 oz per ton (nominal open pit cut offs). The resources estimated by Lac Minerals (USA), Inc, are located both on jointly owned ground, 55 %, (Lac Minerals & Equinox), and 45 % on claims owned solely by Lac Minerals (USA), Inc.

TABLE 4.1
ESTIMATED GEOLOGICAL RESOURCES, LAC MINERALS (USA) INC.

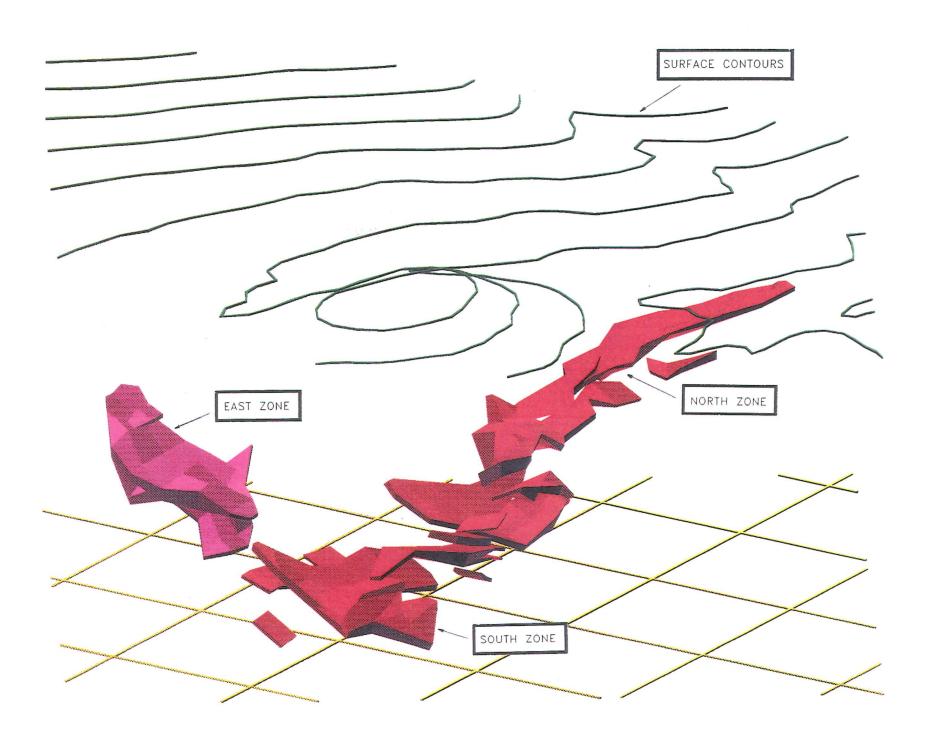
Reserves Category	Tons	Grade oz Au per ton	Gold ounces
Cutoff 0.02 oz Au per ton Probable Possible	4,088,107 1,102,786	0.105 0.133	429,631 146,563
Totals	5,190,803	0.111	576,194
Cutoff 0.05 oz Au per ton Probable Possible	1,591,720 676,659	0.210 0.194	333,942 131,250
TOTALS	2,268,379	0.206	465,192

The resource is still open in a several areas where encouraging intercepts have been made. This includes one intercept of 170 ft. @ 0.559 oz/t.

The most recent calculations of the Rosebud resource (January 3, 1992) indicate an in situ geological resource of approximately 2 million tons at grades of 0.25 oz Au per ton and 2.92 oz Ag per ton, using a 0.1 oz/t cut-off.

The geological reserve is considered accurate and reasonable within the constraints of the existing data, but insufficient for carrying out a definitive feasibility study. Important questions remain concerning the viability of samples and the impact of sampling procedures and analytical errors.





Potential resources within the Rosebud property are estimated to range from the current reserve of 275,000 ounces of gold to 1,500,000 ounces of gold.

TABLE 4.2
POTENTIAL RESOURCES, ROSEBUD PROJECT

Category	Total Oz.	Probability %	Source
Current Reserve	275,000	90-95	BHC (Uneconomic)
High Probability Reserve	500,000	70-80	внс
Good Probability Reserve	1,500,000	30-40	Consensus Estimate

4.2 MINING RESERVES

The mining reserves for this pre-feasibility study have been estimated as follows:

- 1. Preliminary mine planning and layouts were carried out using cut-and-fill stoping on geological sections and plans at a 0.10 oz/ton cut-off. Actual mineable outlines were identified.
- 2. This information was sent to Lac Minerals (USA) Inc. at the Reno offices where the mineable ore reserves were calculated at a minimum mining width of 10 ft. The reserves were calculated based on the mineable outline at cut-off grades of 0.10 oz/ton and 0.15 oz/ton.
- 3. The mineable reserves calculated were based on the drill indicated and drill inferred reserves and included the internal dilution, but did not include any external dilution. The reserves were calculated for the South Zone, East Zone and North Zone. Detailed backup on the reserve estimation is attached in Appendix III.
- 4. BEA estimated the mining dilution based on breaking waste at the end of each stope, backfill scoop from the mucking cycle, waste dilution from the backup of stope in the final cut and waste wall dilution from end panels. In addition, dilution was estimated in secondary stopes from backfill. The detailed calculation used to estimate the mining dilution is also included in Appendix III.

In addition to the dilution due to mining, estimates of the dilution due to ground conditions were obtained from the geotechnical analysis presented in Section 3.0. The total estimated dilution for the different zones was based on the mining dilution and the geotechnical estimate of dilution due to ground condition and is summarized below.

Cut-off Grade Optimization

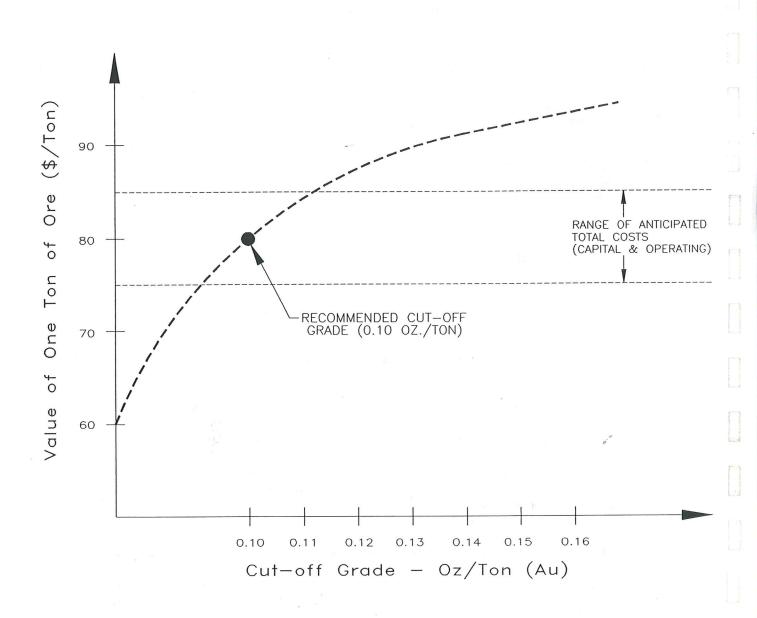


TABLE 4.3

MINING	MINE PANI	EL WIDTH (ft)	MINING DILUTION %		DILUTION DUE	TOTAL	
AREA	PRIMARY	SECONDARY	PRIMARY	SECONDARY	COMBINED	TO GROUND CONDITIONS	DILUTION
SOUTH ZONE							,
A UPPER	15	10	11	22	15	15	30
B LOWER SW	15	15	11	17	14	15	29
B LOWER NE	25	25	8	12	10	15	25
NORTH ZONE	20-25	20-25	9	13	11	20	31
EAST ZONE	30	30	6	10	8	15	23

The total estimated mineable reserves range from 1.6 million tons at a 0.1 cut-off to 1.2 million tons at a 0.15 cut-off with an average grade of 0.226 oz/ton and 0.247 oz/ton respectively, as shown below.

TABLE 4.4

MINEABLE RESERVES @ 0.10 OZ./T CUT-OFF					
	Tons	Cut Au Ozs.	Ag Ozs.	Avg. Grade Au	Avg. Grade Ag
South Zone	741,800				2
Dilution %	28				
Tons	949,500	200,917	2,279,473	0.212	2.40
East Zone	373,700				
Dilution %	23				
Tons	460,000	130,630	1,111,455	0.284	2.42
North Zone	147,800	30,547	1,018,779	. 707	
Dilution %	31				2
Tons	193,500	30573		0.158	5.27
TOTAL	1,603,000	362,094	4,409,707	0.226	2.75

TABLE 4.5

MINEABLE RESERVES @ 0.15 OZ./T CUT-OFF					
	Tons	Cut Au Ozs.	Ag Ozs.	Avg. Grade Au	Avg. Grade Ag
South Zone	604,700	185,002	2,019,402		
Dilution %	28	,			
Tons	774,000				
East Zone	315,100	115,786	1,046,291		
Dilution %	23	.367			
Tons	387,900				
North Zone	128,500	28,385	917,318		
Dilution %	31	.221			
Tons	168,200				
TOTAL	1,330,100	329,173	3,983,000	0.247	2.99

undiluted 1,048,300

.314 Cut to

·403 uncut

4.3 CUT-OFF GRADES

An evaluation of the cut-off grade for Rosebud was carried out using an estimated value of the ton of ore at various cut-off grades as shown on Figure 4. The method for estimating the cut-off grade is as follows:

1. The estimation of mining costs is largely based on local labour rates and material costs and gives rise to a best estimate, downside estimate and upside estimate as shown in the table below.

TABLE 4.6
ESTIMATED MINING OPERATING COSTS \$ PER TON OF ORE

Cost & Stoping Factors	Downside	Best Estimate	Upside
Rate of Production tpd	1000		
Productivity t/mshift	35	40	50
Manpower	29	25	20
Labour Cost \$/manshift	180.00	160.00	155.00
Direct Stoping Costs		Unit Costs \$/t	
Labour	5.22	4.00	3.10
Explosives	1.50	1.00	0.90
Backfill	3.00	2.25	2.00
Ground Support	2.00	1.00	0.80
Other Supplies	6.50	5.75	5.50
Total	18.22	14.00	12.30
Underground Mining Costs			
Direct Production			
Development	5.00	3.60	3.00
Stoping	18.22	14.00	12.30
Total	23.22	17.60	15.30
Indirect Services			
% age of Direct Costs	100%	100%	95%
Services	23.22	17.60	14.54
Total Costs	46.44	35.20	29.84

2. The overall mine operating cost for a typical 1,000 tpd mining operation was then assessed using milling, tailings and administration costs previously used in the Rosebud studies. The table below shows the best estimate for the overall mining cost is approximately \$51.00 per ton of ore, with an appropriate upside and downside.

TABLE 4.7

OVERALL ESTIMATE OPERATING COST US\$ PER TON OF ORE

Cost Centre	Downside	Best Estimate	Upside
Mining	46.44	35.20	29.84
Mill	15.00	13.50	13.00
Tailings	0.50	0.40	0.38
Administration	2.00	1.80	1.75
TOTAL	63.94	50.90	44.97

- 3. Previous studies have estimated the capital costs to be in the range of \$25 \$35 million which results in a cost of approximately \$30/ton of ore based on the current mineable reserves.
- 4. The breakeven cut-off grade can roughly therefore be defined as the cut-off grade at which the average value of the ton of ore is equal to the total property cost including operating and the capital costs. At Rosebud, this estimate is approximately \$80/ton.
- 5. As Figure 4 indicates, a cut-off of 0.10 oz/ton is considered reasonable using the \$80/ton value of ore.

BEA recognizes that this method of estimation of cut-off grades is somewhat approximate. Typically, cut-off grades are estimated through a series of interactions between mine planning and geology with different mining methods and mining geometries continually optimized and re-estimated by geological personnel. Time constraints at Rosebud and the fact that this is a pre-feasibility with an accuracy of \pm 4-25% does not warrant this detailed analysis. The main objective of the cut-off grade at Rosebud is to ensure that the reserve base being used is reasonable and will provide a sound base for the follow-up economic analysis. The approach used above is therefore considered justified.

4.4 GRADE CONTROL

Given the manner of the occurrence of the higher grade gold mineralization within structural features, a good standard of grade control would have to be practised within the underground mine. Thus chip samples would be taken from the advancing heading of each transverse stope panel. Sufficient stope panels would have to be opened to allow time for samples to be assayed.

Longitudinal stopes would be sampled by both chip samples from heading faces and by test holes drilled into the footwall and hangingwall of the stope.

Grade control would also be enhanced by the addition of 8% cement to the last section of each pour of fill.

4.5 EXPLORATION PROGRAM

An exploration program has been proposed which would develop a 2,300 feet long ramp and 2 drifts a total length of 2,500 feet. Drilling would be carried out underground, producing some 60,000 feet of core, from 200 feet sections directed through the ramp and drifts.

Development would produce approximately 135,000 tons of waste rock and up to 15,000 tons of ore from selected bulk sample locations in the underground workings.

The proposed underground exploration program is critical to the viability of the project and is necessary to obtain the following data:

- 1. geological data;
- evaluation of mining methods;
- 3. hydrogeological and dewatering requirements; and
- 4. metallurgical characteristics of the ore.

An estimate of the tonnage of ore required to recover the costs of the exploration program indicate that 25,000 to 45,000 tons of 1.0 oz Au per ton would be needed, shipped either to Pinson or Bullfrog respectively for treatment. Such material is available in either the 159 or East zones.

5.0 MINING PLAN

Various aspects of the mining plan are outlined in this chapter and encompass the selected mining method, a general mine layout, mine extraction sequence, service operations and equipment selection and fleet size.

5.1 MINING METHODS

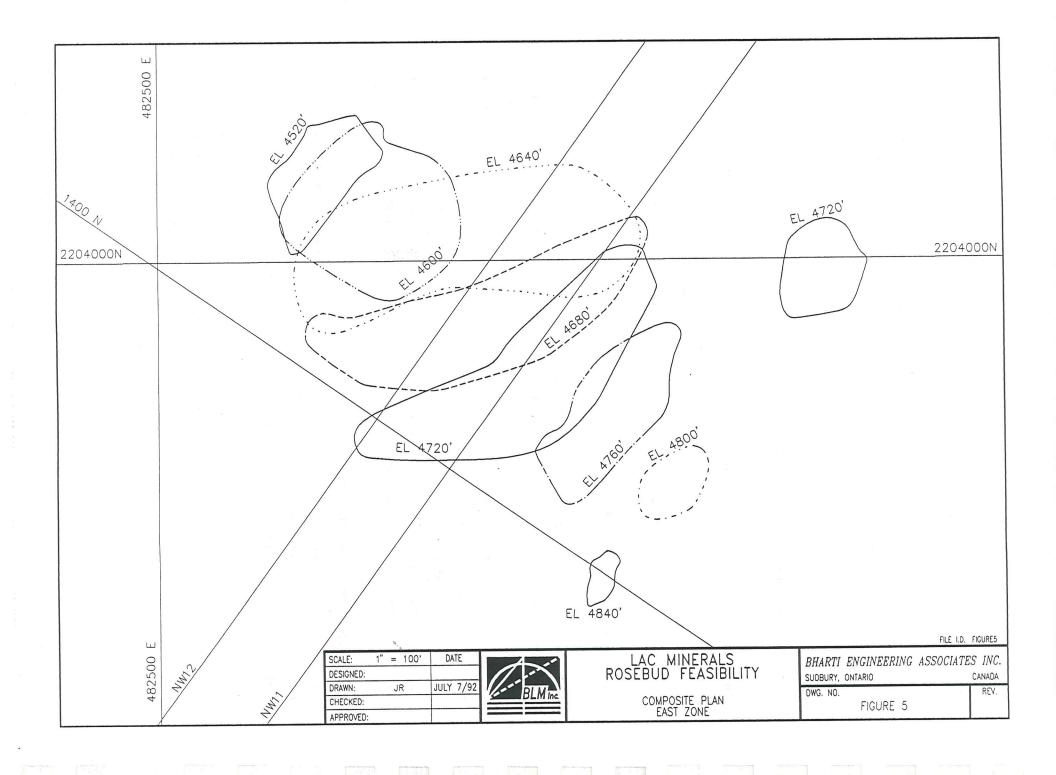
The factors considered in selecting the recommended method of cut & fill are summarised in this section, together with a description of the conceptual design for applying the method to extract the Rosebud deposit.

5.1.1 FACTORS AFFECTING SELECTION

Many factors influence the choice of a mining system such as the location of a deposit, its physical dimensions, configuration in space, distribution and value of grades and metallurgical treatment processes. The major parameters considered in the selection of a mining method are the size, shape, dip and plunge of an orebody. The width of an orebody can place physical limitations on the size of equipment that can be used and can therefore determine the mining method and the degree of mechanisation possible. The dip of an orebody determines the method of moving broken ore for gravity methods. This usually only possible with dips greater than 40°. Shallow dipping structures almost invariably demand the use of either conveyors or trucks for the conveyance of ore.

The strength of an orebody, the overlying rocks and the importance of maintaining the ground surface intact, influence the choice between caving and non-caving methods. There are currently (June 1992), no constraints on preserving the surface above the Rosebud deposit. The quantities of groundwater that exist in the rock mass will not affect the choice of mining method.

The grade and spatial distribution of mineral values also influence the selection of mining methods, in that low grade ore demand the use of low cost, high productivity methods. Gradational and erratic boundaries of mineral deposits require the adoption of selective methods to ensure that waste dilution is minimised.



From a consideration of various factors in relation to the Rosebud deposit, it is evident that cut & fill mining is more appropriate to the extraction of the Rosebud deposit than blasthole stoping, Table 5.1.

TABLE 5.1 COMPARISON OF STOPING METHODS

Mining Method	Advantages	Disadvantages
Cut & Fill	 Highly Selective High Recovery Minimizes Unsupported Span Low Dilution Good Productivity 	 High Mining Costs Labour Intensive Labour Exposed in Stope Each Lift Supported High Development Quantity
Blasthole Stoping	 Good Safety High Productivity Low Development Quantity Lower Support Costs 	 High Dilution Lower Ore Recovery Low Selectivity Requires Remote Mucking

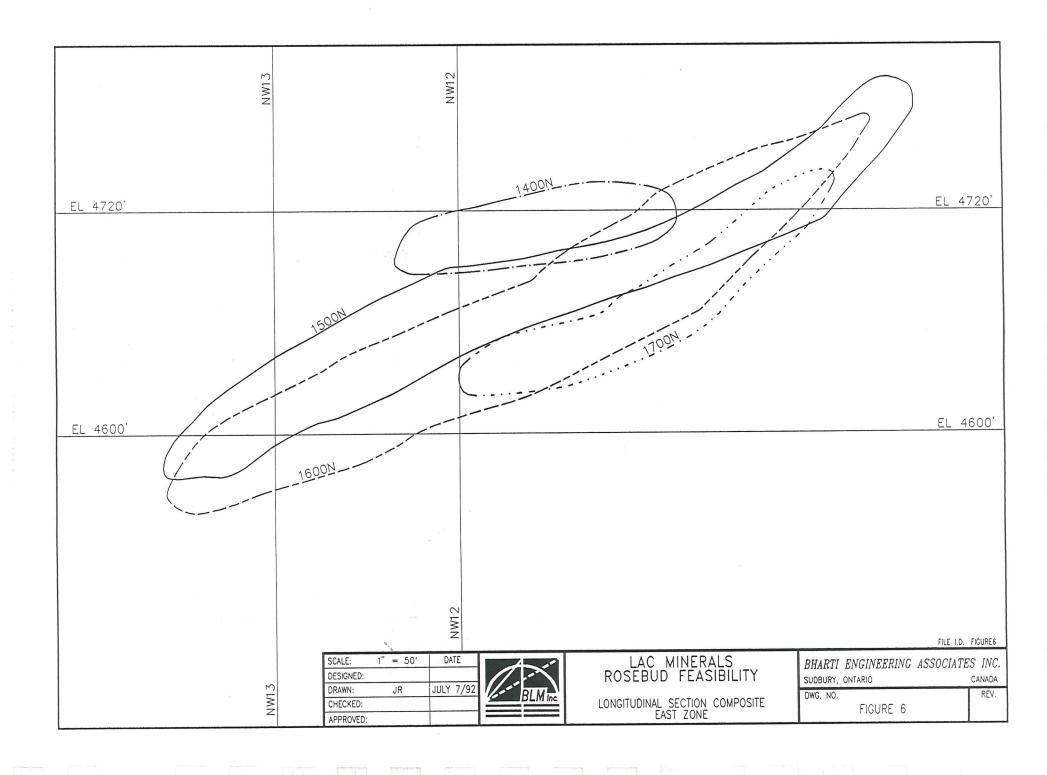
The main disadvantages of blasthole stoping are the higher dilution and lower recovery factors in comparison to the cut & fill technique recommended. It is essential that the grade is maintained and that recovery of ore is maximised, given the low ore grade and low tonnage available.

A detailed examination of the zones from a 3-D AutoCAD drawing using a number of viewing perceptives revealed that blasthole mining would not be appropriate largely because of the shallow plunge and dip of the orebody, the lack of continuity as well as the limited width and vertical height. Figures 5 and 6 show longitudinal and cross-sectional views of the East Zone as examples.

5.1.2 DESIGN CONSIDERATIONS

The proposed mining method recommended for the Rosebud deposit is based upon criteria developed from the scope of work and data provided from the exploration programme and laboratory tests. The design and layout of the cut & fill technique, as conceived herein, is, at this stage, preliminary in nature and subject to modification during subsequent studies and the initial mining trials in the preproduction development period.

Depth will not be a limiting factor with respect to the mining design for the maximum depth below surface will be approximately 800 feet. The stresses induced by the overlying rock mass will not therefore generate loads high enough to bring about failure of the orebody rock mass, other than in



atypical areas where the rock mass may be intersected by zones of multiple discontinuities. The width of panels is a major factor related to both stability and productivity. Wide panels result in increased productivity, giving greater output per development and production round which in turn reduces the number of equipment moves.

In summary, cut & fill mining has been selected for the extraction of the Rosebud deposit for it has the following advantages:

flexibility and ease of modification;

ideal application for an orebody with wide variations in quality, width, roof and floor rock mass conditions;

good selectivity and productivity; and low dilution;.

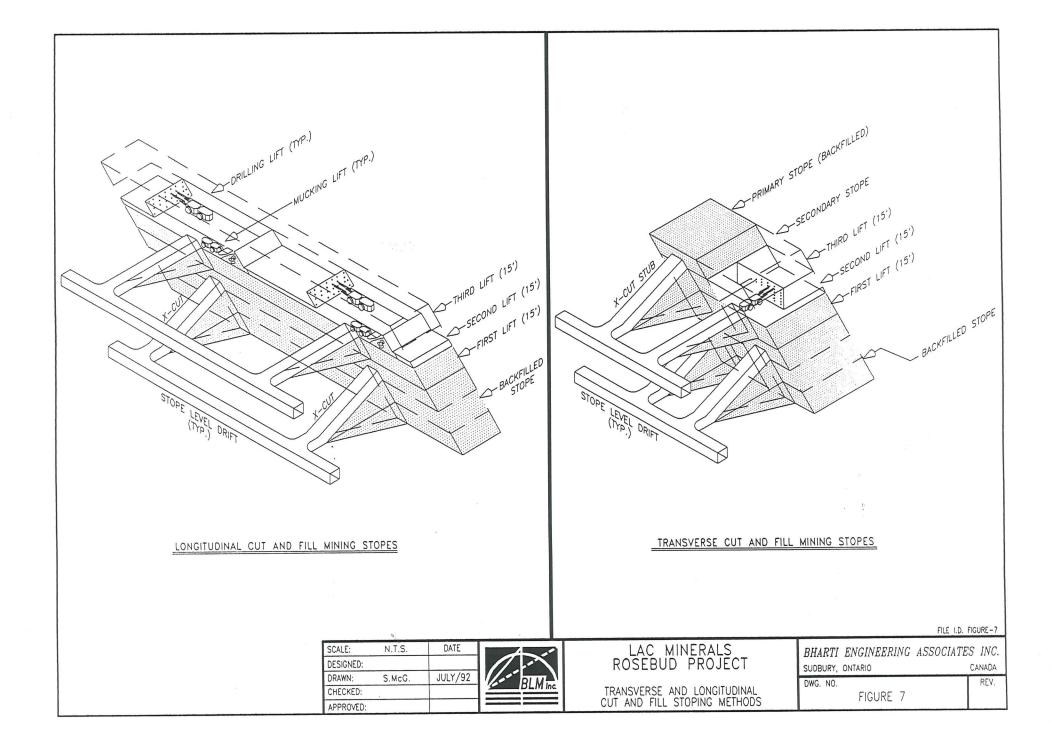
However, it is acknowledged that a disadvantage of cut & fill mining is the need to produce from multiple work places which demands:

supplying many development ends; and moving machinery and constantly extending services.

A high standard of supervision and organisation will be vital in order to produce from many workplaces.

5.2 CUT & FILL

The layout, development configuration and stoping sequence proposed for transverse primary-secondary stope cut-and-fill mining are outlined in this section. Level drawings are shown in Figures 7 to 11.



5.2.1 STOPE LAYOUT

The transverse cut & fill mining method consists of a series of parallel primary - secondary stope panels, oriented across the dip of the ore zones. Stope spans vary for the various zones as indicated in Table 5.2

TABLE 5.2 TRANSVERSE CUT-AND-FILL STOPE SPANS

Zone	Stope Type	Stope Span (ft.)
Upper South	Primary Secondary	15 10
Lower NE South	Primary Secondary	30 30
East	Primary Secondary	25 25

Cut and fill lifts have been selected to be 15 feet, a height effectively used in numerous operations.

5.2.2 STOPE ACCESS

Mining will begin from four horizons, namely the 4800, 4600, 4440 and 4320 elevations. The initial lift on each of these horizons will be accessed via an access ramp driven at +3% to provide positive drainage. The second lift will be accessed by backslashing the attach ramp at 15% and using the broken muck as a floor.

Starting from the third lift, stopes will be accessed from an attack ramp emanating from a spiral ramp would be used to access three lifts, with the first of the three being accessed by ramping at -15%, and the next two lifts accessed by blackslashing the access ramp as required, ensuring a maximum inclination of $\pm 15\%$.

Each lift will consist of primary and secondary stopes. When a particular lift is reached by the attack ramp, a strike drift is driven along the entire length of the ore zones in order to access the primary and secondary stopes.

ondary stope

s as indicated

TOPING METHOD

ill mining method involves the following elements of the stoping cycle:

drill

blast

support ground

muck/haul

backfill

t will require drift type rounds. Subsequent lifts will have an open brow, therefore asting would be used.

3 done with electric-hydraulic two-boom, rubber-tired jumbos. The flat breast holes will 5 to 1.75 inches in diameter and 12 feet long. Drill hole burden and spacing is expected 1 feet.

blasting agent is ANFO (low cost) detonated with NONELS. ANFO would be loaded from D loaders, either from a scissor lift truck or from an LHD with staging platform.

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n a spiral ramp g at -15%, and ng a maximum

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5.2.3 STOPING METHOD

The cut-and-fill mining method involves the following elements of the stoping cycle:

- drill
- blast
- support ground
- muck/haul
- backfill

Drilling:

The initial cut will require drift type rounds. Subsequent lifts will have an open brow, therefore horizontal breasting would be used.

Drilling will be done with electric-hydraulic two-boom, rubber-tired jumbos. The flat breast holes will typically be 1.5 to 1.75 inches in diameter and 12 feet long. Drill hole burden and spacing is expected to be 2.5 to 3 feet.

Blasting:

The preferred blasting agent is ANFO (low cost) detonated with NONELS. ANFO would be loaded from portable ANFO loaders, either from a scissor lift truck or from an LHD with staging platform.

Mucking:

Stopes will be mucked with 3.5 yd³ LHD dumping directly into trucks. A productivity of 30 - 35 tons/hr. has been estimated for the 3.5 yd³ LHD despite the very short hauls in stope panels since it is proposed that truck drivers load their own trucks. Given the 8 hour shifts proposed for the Rosebud Project and an effective operating time of 5.4 hours per shift, such machines should produce between 160 and 190 tons per shift or 320 to 380 tons per day. A production rate of 1,000 tons per day would require 4 machines for stope mucking at 66% availability.

Haulage:

The mining plan calls for trucks to be loaded by their drivers, as opposed to the development ore passes and the installation of chutes. An average 2-way hauling distance of say 12,000 feet and an

average hauling speed of 33,000 feet per hour (6.25 mph) would result in 2.75 round trips per truck per hour. Given a truck factor of 12 tons, each truck would haul approx. 30 - 35 tons per hour taking loading into account, which translates into a daily capacity of approx. 300 - 375 tons.

Thus, a daily output requirement of 1,000 tons would demand 5 trucks for stoping. These trucks would also be used initially for hauling development waste to surface.

Backfilling:

Backfilling will consist of high density, full stream tailings placed underground at approximately 80% pulp density. The application of high density backfill permits Rosebud to use tailings rather than rockfill. Conventional hydraulic fill, classified and placed underground at 60 - 65% density, cannot be used at Rosebud because after classification the tailings available for hydraulic fill would be less than 20%. High density fill on the other hand, permits fill to be placed using full stream tailings but at a higher density so that drainage is not required and, therefore, the tailings do not have to be classified.

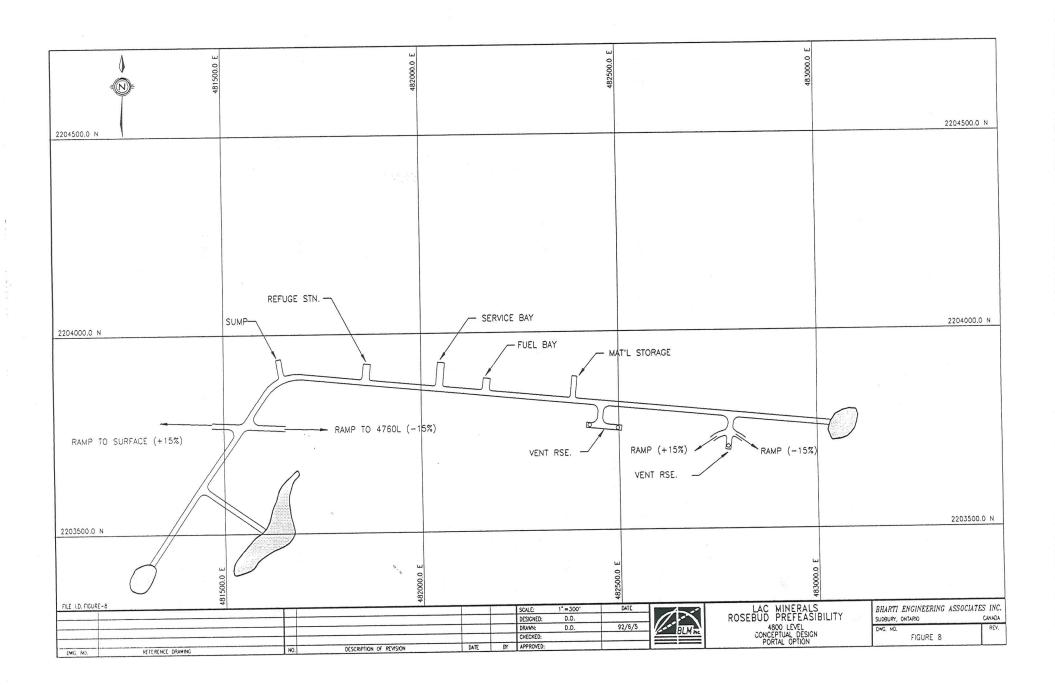
The primary stopes will be consolidated with hydraulic fill at 1:30 cement:tailings ratio (3% cement) with a 1 ft. thick cap of 1:10 cement:tailings to ensure a good mucking floor and minimize dilution. All stopes will be filled within 3 ft. of the back (brow of the subsequent lift). The secondary stopes will also use consolidated fill, but with a 1:40 cement:tailings ratio and a 1:10 floor.

Wherever possible, development waste should be placed into unfilled stopes. It is anticipated that at least 50% of the development waste will be placed underground.

Ground Support:

A geotechnical assessment of the various zones indicates a relatively broad range of ground conditions which are expected to be encountered. Accordingly, stope spans vary for specific zones (Table 4.2) dependent on the local conditions.

Additional ground support would include rockbolts to be installed where necessary, including accessories such as washers and steel straps.



5.3 GENERAL MINE LAYOUT

The general mine layout of the Rosebud project is constrained by a number of factors:

configuration, tonnage and grade distribution of the ore zones: rock mass characteristics of the ore and country rock; surface topography; infrastructure; and position of the treatment plant.

Access to the mine workings, configuration of the underground haulage, ventilation system and primary development is discussed in this section in the light of the above mentioned factors.

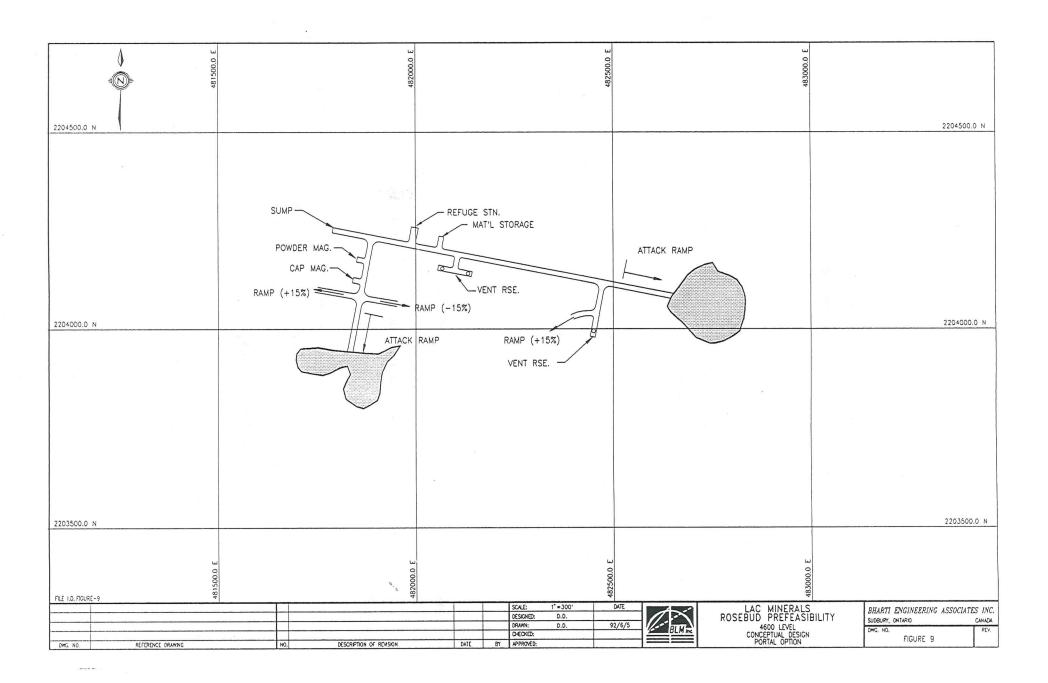
The areal extent of the proposed Rosebud mine requires a single entrance to the mine to provide adequate access for men and equipment in terms of safety and travelling time to the work place that could be either by a portal or a service shaft. Both alternatives were considered for Rosebud.

Portal Option

A portal would be established at the 5050' elevation and a decline haulage ramp driven to the east at a maximum gradient of 15 %. The cross section dimensions of the ramp would be 13' in width and 12' in height. The selected position of the decline should be verified by geotechnical exploration boreholes.

The length of the main ramp, inclusive of access cross cuts and other development, has been estimated as approximately 12,500'. Excavations cut on each level incorporate powder magazines, cap magazines and material storage excavations. Service and fuel bays would be cut on the 4800 and 4440 sublevels with the main sump on the lowermost 4320 level.

In addition to the horizontal development, an escapeway, 10 ft. diameter must be excavated from 4800 level to surface. The raise would be developed in four legs and is required in both options.



Shaft Option

This option would involve sinking a shaft to a depth of about 1030 ft. As the shaft is being sunk, stations will be cut at the 4800, 4700, 4400 and 4300 elevations for ramp takeoffs to the mining zones. The haulage ramps will have a maximum +/- 15% grade with a nominal profile of 13 ft. wide and 12 ft. high. An orepass raise with loading pocket will be established on completion of the shaft, at which point level ramp development can commence using the orepass used as a waste dump. Fresh air ducting, air and water lines will be carried in the shaft with take-offs at each level for development. All water will be pumped and drained back to the shaft sump for pumping to surface.

The length of the main ramp and access developed from the shaft inclusive of crosscuts, cap and material storage is estimated at 8000 ft.

The comparative costs are as follows:

TABLE 5.3. SHAFT VS. RAMP

(\$000s)				
ITEM	PORTAL	SHAFT		
Main Ramp Shaft	3,609	3,396		
Internal Ramp	4,958	3,456		
Ore Pass		199		
TOTAL	8,567	7,051		

The disadvantage of the shaft is that production is delayed by 6 months during sinking, and a further 4 months until the ore zone is dewatered.

The portal option is used in this prefeasibility study.

2204500.0 N 2204500.0 N SUMP -RAMP TO 4480L RAMP TO 4400L REFUGE STN. -CAP MAG.
MAT'L STORAGE
POWDER MAG. SERVICE BAY-ATTACK RAMP 2204000.0 N 2204000.0 N 2203500.0 N 2203500.0 N FILE I.D. FIGUR-10 LAC MINERALS
ROSEBUD PREFEASIBILITY
4440 LEVEL
CONCEPTUAL DESIGN
PORTAL OPTION DATE 1"=300" BHARTI ENGINEERING ASSOCIATES INC. SCALE: DESIGNED: D.D. SUDBURY, ONTARIO 92/6/5 DRAWN: D.D. DWG. NO CHECKED: FIGURE 10 DESCRIPTION OF REVISION BY APPROVED: REFERENCE DRAWING

5.3.1 UNDERGROUND HAULAGE

The removal of ore and waste rock from the mine would be carried out with diesel powered trucks, 13 ton to 15 ton, utilising the main access ramp. 15 ton trucks with 3.5 yd.³ LHD units were selected over the 26 ton truck/5 yd.³ LHD combination due to cost, in order to maintain a small drift size and to optimize ventilation requirements.

The gradient of 15 % proposed for the ramp would cater for the movement of all vehicles both into and out of the underground mine.

5.4 MINE EXTRACTION SEQUENCE

Operational needs with respect to the mine extraction sequence, dictate that:

mine stability is maintained; unmined ore is preserved in a mineable condition; major service openings are protected; and secure access to safe working places is provided.

The planned sequence to extract the three ore zones, which is based upon both geotechnical and practical considerations, requires that the:

lower section (Block B) of the South Zone (4550' to 4730') is mined first; followed by the North Zone (Block D) and the East Zone (blocks E1 and E2); and finally the upper section (Block A) of the South Zone (4800' to 4900').

5.5 PRODUCTION RATE

Several alternative production rates were examined to suit the orebody geometry and layout with alternative mining approaches and methods that would maximize production and minimize dilution. The selective production rate is 1,000 tpd on 2 shifts, five days per week basis, with the mill operating on seven days, 3 shifts a day at 750 tpd. This alternative was selected for several reasons:

-POWDER MAG. CAP MAG.~ 2204500.0 N 2204500.0 N RAMP TO 4360L ATTACK RAMP FUEL BAY-ATTACK RAMP SERVICE BAY-VENT RSE. - MAIN SUMP 2204000.0 N 2204000.0 N 2203500.0 N 2203500.0 N LAC MINERALS

ROSEBUD PREFEASIBILITY
4320 LEVEL
CONCEPTUAL DESIGN
PORTAL OPTION FILE I.O. FIGUR-11 1" = 300" BHARTI ENGINEERING ASSOCIATES INC. SCALE: DESIGNED: 0.0. SUDBURY, ONTARIO CAHADA 92/6/5 DRAWN: D.D. CHECKED: FIGURE 11 DESCRIPTION OF REVISION DATE BY APPROVED: REFERENCE DRAMMG DWC NO.

- 1. The mine has a relatively limited reserve of approximately 1.6 million tons. A maximum production rate of 250,000 tpy would exhaust these reserves in just over six years. This is a relatively rapid extraction rate, and while it is achievable, it does deplete the ore reserves rapidly.
- Cut-and-fill mining was selected because it provides several faces in the East, South and North Zones simultaneously. Mining can therefore progress in several stopes. Assuming typical stoping productivities of 40 tons per manshift and 2 men per stope, only 6 active headings are necessary to achieve the desired production rate per shift of 500 tpd. In blasthole stoping, for example, achieving this production rate would be much more difficult because the geometries are firm and significant development and sequencing has to be carried out to obtain the initial production.
- 3. An extremely high production rate would put unnecessary pressure on the materials handling system which is dependent on the one ramp accessing all the ore to surface.

Overall, it is concluded that 1,000 tpd production rate (250,000 tpy) is the optimum (maximum) achievable production rate using cut-and-fill mining. The layout of the mining method provides the flexibility to obtain this production rate from the three zones. It should be emphasized that the limited reserve base precludes the potential for a higher tonnage rate from Rosebud.

In order to mine at a rate of 1,000 tons per day, a sufficient number of stope headings must be available at all times. The flexibility of ramp access, cut-and-fill stoping together with the mobility of the equipment effectively means a mining face must be available for drilling or mucking constantly. The availability and system to place backfill in the stopes is critical to attaining the production target and maintaining it for the earlier years in the mine life.

Stope panel sequencing, access development and fill scheduling for each zone must be in place before production commences. This is to ensure access ramps are completed in time to provide stope panel availability and that fill is placed before pillars are scheduled for production.

Production is from stoping panels of 10 ft., 15 ft., 20 ft., 25 ft., 30 ft. and + 30 ft. widths. After the initial cut is taken and filled, breasting off consolidated fill commences using elec/hyd. 2 boom jumbo, to a cut height of 15 ft. Tons for each panel breast of 12 ft. depth per stoping crew is:

TABLE 5.4
ESTIMATE OF PRODUCTION RATE VS. PANEL WIDTH

Panel Width	10 ft.	15 ft.	20 ft.	25 ft.	30 ft.
Tons/blast	180	270	360	450	540
Shifts Drill and Blast	0.5	0.5	0.75	1.0	1.0
Shifts Muck-Bolt- Scale	0.5	0.75	0.75	1.0	1.0
Total Shifts	1.0	1.25	1.5	2.0	2.0
Tons/Crew Shift	180	216	240	225	270
66% Equip. Availability	119	143	158	149	178
8 Stope Crews tons per day	952	1144	1264	1192	1428
Average/day All Panels			1196		

A stoping schedule should be drawn up based on production from panel sizes stated. A fill schedule should then be made to ensure panels can be filled in sufficient time to allow pillars to be mined. Separate fill crews have been allowed for in the manpower.

A mining rate of 750 tons per day (187,500 tpy) has been calculated as the optimum (maximum) rate for the cut-off option at 0.15 oz Au. This scenario will probably reduce the effective parameters of stoping areas and require more geological control. It is, however, considered a realistic production target that can be attained earlier and sustained. A higher production rate at the 0.15 oz. cut-off may be difficult to sustain.

5.6 CONSTRUCTION AND SERVICES

The following main construction times would be necessary underground:

- refuge stations (all levels)
- service bays (4800 and 4440 levels)
- fuel bays (4800 and 4440 levels)
- sumps (all levels)

- ventilation doors (all levels)
- powder magazines (all levels)
- ♦ cap magazines (all levels)

Mine services would include:

- ♦ 4" air lines
- ♦ 2" water lines
- ♦ 6" drainage lines
- electrical power lines

all of the above would advance with development from the portal.

5.7 VENTILATION SYSTEM

It is proposed to utilise the main haulage decline as the main fresh air tunnel. Intake air would be drawn down the ramp and would flow to the stoping areas via the access cross cuts. Auxiliary fans would force air into stoping panels and development sections. The ventilation circuit would be completed with the extraction of return air via the ventilation raise situated near the East Zone The main exhaust fan would be located at surface connected to the collar of the 10 ft. diameter exhaust raise.

5.8 MAINTENANCE & POWER

The major services that would be provided by the Maintenance Section would encompass mobile and static equipment, and the supply of power and installation of the substations.

As the mine is accessed to surface via a ramp system, the majority of repairs mobile equipment could be done in the surface shops. In addition, underground service bays on the 4800 and 4440 levels could provide additional servicing.

Power would be taken underground by means of high voltage cables hung in the haulage decline. An electrical sub station would be established in the mine close to the entrance to the bottom of the exhaust ventilation raise. A suitable position would be in a cross cut connecting the fuel and service bays on 4320 sub level. Such a location would offer some protection against flooding in the mine.

However, should fires occur in a sub station the noxious gases would pass directly into the exhaust stream.

Power would be distributed underground via a substation tied into portable power centres which would serve each section independently.

5.9 MINE DRAINAGE

Pumping arrangements from underground would be based upon the removal of both service water and excess water from the placement of hydraulic fill. A simple reticulation system would be setup based upon the flow of service drilling water from production sections along drains positioned in the access cross cuts. Thereafter, water would be directed to the main sump via drain holes connected to the footwall haulages.

The main pumps would deliver waste water to surface through a 4" diameter rising main hung in the ramp.

5.10 EQUIPMENT

Table 5.5 identifies the major mobile equipment during production based on 66% availability (Bullfrog estimate).

TABLE 5.5

NO.	ITEM	
6	2 Boom E/H jumbo	
6	15 Ton diesel trucks	
6	3.5 cu. yd. Diesel LHD	
1	Anfo Truck	
6	Anfo Loaders	
1	Grader w/Blade	
1	1 Personnel Carrier	
2	Personnel Vehicles	
1	Diamond drill & rods	
1	Fuel tanker	
6	Scissor truck	

6.0 MILL AND SURFACE INFRASTRUCTURE

A detailed evaluation of the mill and surface infrastructure is beyond the scope of this study. The information used to estimate the capital and operating costs for both the mill and the infrastructure on surface has been obtained from Lac Minerals and previous studies carried out on Rosebud.

6.1 MILL

George Hope of Lac Minerals has provided the capital and operating costs for the mill and the recoveries that should be used for the Rosebud project. At a milling rate of 750 tpd on 7 days/3 shifts per week basis, the costs are as follows:

Capital Cost

\$9.5 million

Operating Cost

\$13.50/ton

The recoveries used in the follow-up economic analyses are as follows:

TABLE 6.1

	Gold	Silver
South and East Zones	91%	62%
North Zone	84.5%	61%

As mentioned earlier, limited metallurgical testwork carried out by Lac, indicate that the gold can successfully be extracted with a carbon and leach plant with gravity separation. A sag mill will likely be required with water requirements at approx. 200 gpm. Further testing, particularly towards identifying and solving any leaching problems, brought about in part by the presence of gold encapsulated by sulphides and the presence of antimony should also be carried out.

6.2 SURFACE INFRASTRUCTURE

A study on the minesite layout for the Rosebud project was carried out by Dynatec on February 6,1 992. In addition, the tailings disposal and related environmental work was completed by Hallam

Piesald Knight and is incorporated in the Beacon Hill Consultant's report.

The primary surface structure would include the following:

- Changehouse, which would be a 15 ft. x 60 ft. trailer
- o Contractor's office, also a 15 ft. x 60 ft. trailer
- Owner's office, a 15 ft. x 45 ft. trailer
- Compressor and electrical station, on a 20 ft. by 20 ft. concrete pad with 2 750 cfm compressors and electrical transformers and switchgear
- Generator station on an 8 ft. x 20 ft. trailer housing generators with a capacity of 800 kilowatts
- Water storage a 6 ft. dia. x 10 ft. high water tank with a capacity of over 2,000 gallons
- Fuel and lube storage a 40 ft. x 20 ft. dirt pad with a 3 ft. high berm would be used.
- Maintenance structure a 60 ft. x 20 ft. concrete pad with trailer facilities and a sheltered area with a built-in grease trough
- Explosives storage clear dirt pad that houses an ANFO trailer, an detonator magazine and a high explosive magazine.
- Septic tank a 10 ft. x 5 ft. x 6 ft. deep nominal 1500 gallon buried septic tank would be employed.
- Leach field a 40 ft. x 80 ft. leach field and distribution box
- Portal structure a 16 ft. wide timber portal with winged walls extending out for 10 ft. at 45°.
- Security fence a 6 ft. high chain link fence would be used.
- Settling pond for mine water discharge settling pond has been designed with overall dimensions of 180 ft. x 125 ft. with side embankments on a 3-1 slope. The pond has a nominal capacity of over 324,000 gallons and a maximum capacity of almost 389,000 gallons.
- Catch basin for surface water runoff from disturbed areas. Site drainage will be diverted into the catch basin. The impoundment will allow for skimming of oil slicks from water surfaces for containment in sealed containers and transport to an approved disposal site.
- Land Application System this will be located west of the minesite and north of the country road.
- Road construction a new road will either be constructed or the existing road improved from the country road to the minesite. This will require approximately 0.875 miles of road.
- Reclamation of site all surface structures, equipment and surplus materials and supplies will be removed from the site by the contractor when he demobilizes.

6.3 TAILINGS DISPOSAL

Tailings disposal will take place southwest of the plant and mine portal. The original estimate of storage capacity was 3 million tons. Since the present reserves stand at 1.6 million tons and approximately 50% of the tailings will be used underground for backfill, it is estimated that the tailings storage could be reduced to 1 million tons, significantly reducing the total capital costs. A 3 pond configuration will be used for the tailings dam design.

7.0 MANPOWER RESOURCES

The organisational structure of the Rosebud mine would comprise four main departments reporting directly to a Mine Manager. It is estimated that a total workforce of 132 would be required to produce at an output of 250 000 tons per annum, Table 7.1.

TABLE 7.1 MINE WORKFORCE

Department	Number
Mining	78
Maintenance	17
Milling	25
Administration	12
Grand Total	132

The Project plan incorporates a 2 shifts per day, 5 days per week operation for the mining, maintenance and administration workforce, associated with a daily output of 1 000 tons. Milling staff and hourly personnel would be required to work a 3 shifts per day, 7 days per week system for a daily throughput of 750 tons.

7.1 MINING

It is estimated that a total of 58 hourly paid employees would be needed to perform the direct and indirect activities for the underground mine (underground and surface), Table 6.2. The stoping crew structure would comprise:

- 1 jumbo operator;
- 1 man blasting crew; and
- 1 LHD operator.

Similarly, development crews would consist of:

1 jumbo operator; and

1 man blasting crew: and

TABLE 7.2 MINING DEPARTMENT WORKFORCE

Description	Day Shift	Back Shift
Direct Mining		
Stoping	12	12
Development	. 3	3
Support	2	2
Backfill	2	2
Subtotal	15	15
Services U/G		
Haulage	4	4
Grader & Cleanup	1	1
Labour	6	6
Subtotal	5	5
Services Surface		,
Haulage	2	2 /
Dry and Lamproom	1	1
Labour	2	2
Subtotal	5	5
GRAND TOTAL	29	29

A total of 20 staff has been estimated for the provision of supervision and engineering and geological services, Table 7.3.

TABLE 7.3 SUPERVISION AND TECHNICAL STAFF

Description	Day Shift	Back Shift
Supervision		
Mine Manager	1	
Mine Foreman	1	1
Safety	1	
Clerk/Secretary	1	
Engineering		
Mine Engineer	·1	
Draftsman	1	
Surveyor	1	
Assistant Surveyor	1	
Geology		,
Mine Geologist	1	
Geologist	1	1
Technician	1	1
Assayer	1	1
D/Drill Operator	4	
Total	16	4

7.2 MAINTENANCE DEPARTMENT

A Foreman would be responsible for the maintenance department which would comprise 16 mechanics and electricians working in both underground and surface areas, Table 7.4.

TABLE 7.4 MAINTENANCE DEPARTMENT MANPOWER

Description	Day Shift	Back Shift
Foreman	1	
Underground		
Mechanic	6	2
Electrician	2	1
Surface		
Mechanic	3	1
Drill Shop	1	
Total	12	4

In addition, an allowance has been made for labour on day shift for the repair of drill steels and hand held drills, Table 7.4.

7.3 MILL

A total manpower estimate for the 3 shifts per day, 7 days per week mill operation has been estimated as 25 staff and workforce, Table 7.5.

TABLE 7.5 MILL MANPOWER

Description		Shift	Total
Supervision	Superintendent	, <u>1</u> 1	1 4
Operators		3	12
Electrician		1	4
Labour		1	4
Total			25

Four crews would be needed to operate the mill round the clock.

7.4 ADMINISTRATION

An accountant would head up the Adminstration Department which would service the mine, on a largely single shift 5 day per week basis, with respect to warehousing, pay, accounting, secretarial services and security, Table 7.5.

TABLE 6.5 ADMINISTRATION DEPARTMENT STAFF

Description	Number
Accountant	1
Warehouse	2
Pay & Accounts Clerk	2
Purchasing Clerk	1
Secretary	2
Security	4
Total	12

7.5 PRODUCTIVITY

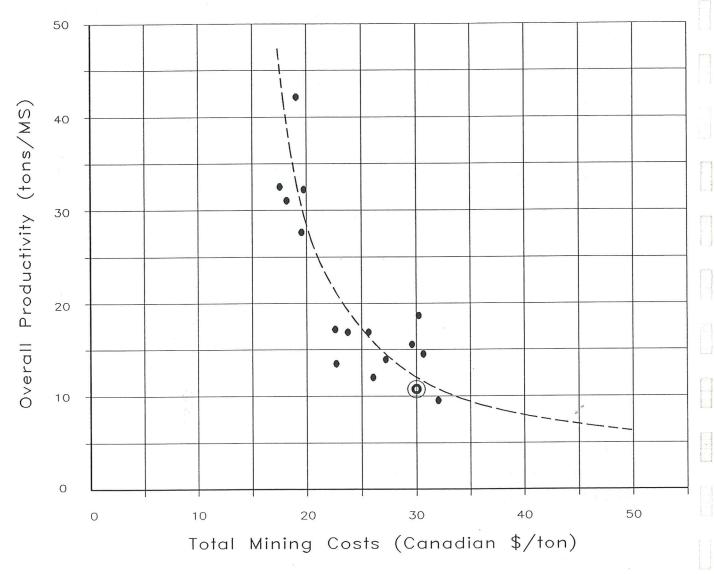
The productivity of the underground mine as conceived in this study is comparable to the productivity achieved in similar mines in both Canada and the United States which extract gold ore bodies by cut and fill mining methods.

The manpower base for the calculation of the productivities achieved for the various activities in underground mines are as follows.

Stoping

Includes all mining and maintenance daily paid workers involved in the core development and stoping activities.

Productivity & Mining Cost Comparison



O - ROSEBUD PROJECT

Operating Mines

Underground

Incorporates all the mining and maintenance employees working in all the activities underground, supervisors and senior staff in charge of underground mining, and Technical Services staff associated with the underground mine.

Mine

All employees of the mining, milling, smelter and administration departments.

To calculate the various productivities, the daily output, expressed in tons is divided by the total number of employees working each day, as defined above. Thus the cut and fill stoping productivity of the Rosebud mine as currently planned would be 29 tons per manshift, inclusive of backfill operations.

The estimated productivity for the underground mine would be approximately 11.3 tons per manshift which would reduce to 8 tons per manshift if the entire mine workforce are taken into account. Figure 12 shows the range of productivities in several mines in Eastern Canada. A productivity of 11.3 t/ms for a relatively small mine in Canada is considered excellent. It is also interesting to note that a typical mine in Canada would have a mining cost of between \$35-\$40/ton at these productivity levels.

TABLE 7.6 ESTIMATED MINE PRODUCTIVITY FACTORS

Manpower	Number	Productivity tons/manshift
Daily Production tons	1000	
Stoping		
Mining	30	
Maintenance	5	
TOTAL STOPING	35	29
Mining		
Mining	58	
Mine Maintenance	10	
Staff	20	
TOTAL MINE	88	11.3
SITE		
Mining	78	
Maintenance	17	
Mill	25	
Administration	12	^
TOTAL SITE	132	8

8.0 PROJECT SCHEDULE

8.1 RATE OF PRODUCTION AND RESOURCE DEVELOPMENT

The ore production rate has been calculated to be 1,000 tons per day (250,000 tons/yr.) coming from a combination of the East, South and North Zones. The mine life production schedule is shown in Table 8.1.

The planned sequence to extract the three zones was based upon both geotechnical and practical considerations and is as such:

- lower section (Block B) of the south Zone (4550 to 4730 ft) is mined first
- followed by the North Zone (Block D) and the East Zone (Blocks E1 and #2);
- and finally, the upper section (Block A) of the South Zone (4800 ft. to 4900 ft.)

8.2 DEVELOPMENT PROGRAM

Initial development would be performed by a contractor, advancing at a rate of 650 ft. per month. The pre-production development schedule for this work is shown in Figure 13. As production stoping is phased in, the contractor would be phased out (Year 2) and ongoing development maintained by operating crews.

The Mine Life Development schedule is shown in Table 8.2 indicating a total of 29,700 feet of development.

8.3 OTHER SCHEDULE

Production and development schedules were also prepared for:

- ♦ 350,000 tpy (1000 tpd @ 7 days/wk) @ 0.10 oz/t cut-off
- ♦ 187,500 tpy (750 tpd @ 5 days/wk) @ 0.15 oz/t cut-off
- ♦ 262,000 tpy (750 tpd @ 7 days/wk) @ 0.15 oz/t cut-off

These schedules were used in subsequent economic analyses and are included in Appendix III.

PROJE	CT: ROSEBUD									
CURRE	T DATE: 04/27/92 ROSEBUD -	PRE	PRODU	CTIO	N					
AS OF	DATE: 11/27/91	Γ	•							
- 1 - II	Nam 2	1993 JAN	B APR	JUL	OCT	1994 JAN		JUL	OCT	1995 JAN
Job#	Name								-	
10	PORTAL EXCAVATION									-
20	RAMP (SURF. TO 4800L)									
30	RAMP (4800L TO 4600L)				4					
	RAMP (4600L TO 4440L)									
50	RAMP (4440L TO 4320L)									
60										
70	4800L DEVELOPMENT				_					
80	4600L DEVELOPMENT									
90	4440L DEVELOPMENT					<u> </u>	1			
100	4320L DEVELOPMENT]			
110	* "									
	VENT RAISE (SURFACE TO 4800L)	*				٦				
	VENT RAISE (4800L TO 4600L)									
	VENT RAISE (4600L TO 4440L)						<u> </u>			
250	VENT RAISE (4440L TO 4320L)									

TABLE 8.1

MINE LIFE PRODUCTION SCHEDULE

CUT-OFF GRADE = 0.10 OZ./TON (AU), 1000 TPD, 5 DAYS/WEEK

ZONE		GRADE	YEAR 1	YEAR 2	YEAR 3	YEAR 4	YEAR 5	YEAR 6	YEAR 7	YEAR 8	YEAR 9	YEAR 10	TOTAL
EAST	Tons Au oz. Ag oz.	0.284 2.416		125,000 35,497 302,026	150,000 42,597 362,431	75,000 21,298 181,215	50,000 14,199 120,810	40,000 11,359 96,648	20,000 5,680 48,324	0	0	0	460,000 130,630 1,111,455
SOUTH	Tons Au oz. Ag oz.	0.212 2.401		75,000 15,870 180,053	100,000 21,160 240,071	175,000 37,031 420,124	200,000 42,321 480,142	175,000 37,031 420,124	125,000 26,450 300,089	65,000 13,754 156,046	34,500 7,300 82,824	0	949,500 200,917 2,279,473
NORTH (C & D)	Tons Au oz. Ag oz.	0.158 5.265		0	0	0 0	0 0	35,000 5,525 184,275	60,000 9,472 315,900	60,000 9,472 315,900	38,500 6,078 202,703	0	193,500 30,547 1,018,779
TOTAL	Tons Au oz. Ag oz.	0.226 2.751	0 0	200,000 51,368 482,079	250,000 63,757 602,502	250,000 58,329 601,340	250,000 56,520 600,952	250,000 53,915 701,048	205,000 41,602 664,313	125,000 23,226 471,947	73,000 13,378 285,527	0 0 0	1,603,000 362,094 4,409,707

4.

TABLE 8.2

MINE LIFE PRODUCTION SCHEDULE

CUT-OFF GRADE = 0.10 OZ/TON (AU), 1000 TPD, 5 DAYS/WEEK

DEVELOPMENT	ANNUAL DEVELOPMENT (FT.)										
	1	2	3	4	5	6	7	8	9	10	TOTAL
Preproduction:				2		,					
Ramps Levels	7800 6900										7800 6900 0
Total	14700										14700
Vent Raises	1000										1000
Production:											
Ramps Levels		600 2250	600 2250	2250	2250	2250	1500	800	250		1200 13800 0
Total		2850	2850	2250	2250	2250	1500	800	250	0	15000
Vent Raises											
Combined:											
Ramps Levels	7800 6900	600 2250	600 2250	0 2250	0 2250	0 2250	0 1500	0 800	0 250	0	9000 20700 0
Total	14700	2850	2850	2250	2250	2250	1500	800	250	0	29700
Vent Raises	1000		***								1000

9.0 OPERATING AND CAPITAL COSTS

9.1 OPERATING COSTS

The mine operating costs prepared by BEA have been generated from basic principles using a sophisticated spreadsheet program developed by BEA inhouse. This program inputs labour rates and material costs together with the equipment to be used and the performance of the different types of equipment and expected labour productivities and generates operating costs from basic principles. A summary of the operating costs for Rosebud is presented below. (Table 8.1) A complete breakdown of the operating costs is provided in Appendix IV.

Rosebud Mine Operating Cost Assumptions

- \$500,000/yr allocated for diamond drilling.
- 2. Materials/supplies and labour rates based on prices at Bullfrog Mine.
- 3. 5% absenteeism included in manpower.
- 4. Last year of mining (year 10) lasts only half a year, i.e. 40,000 tons mined in first 6 months of year 10.
- 5. No equipment replacement capital included, but \$100,000/yr for ongoing spare parts included.
- 6. \$1.00/ton to handle surface waste included, some waste assumed to be placed in stopes underground.
- 7. \$30,000/yr for backfill boreholes included.

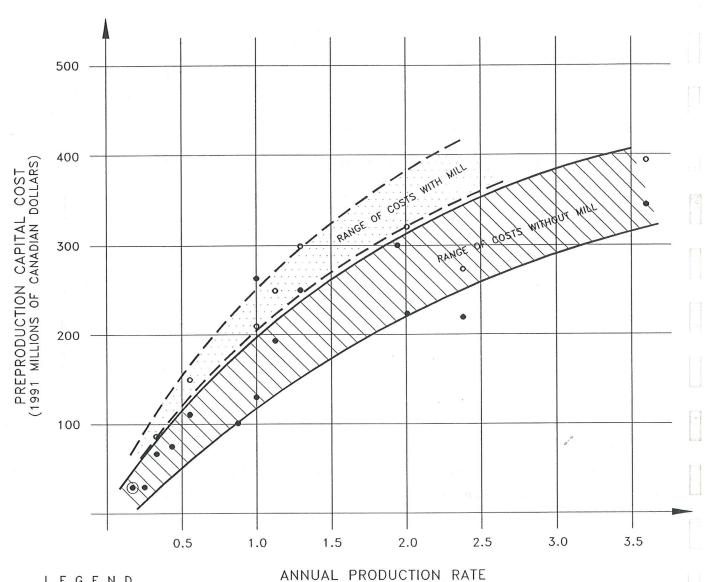
TABLE 9.1
MINE OPERATING COST SUMMARY

	Pre-Production	Production				
Item	Cost	Cost	Cost/Ton			
General Mine Expenses	\$5,441,000	\$29,409,000	\$16.80			
Direct Mining Costs	\$8,203,000	\$33,001,000	\$18.86			
Total	\$13,644,000	\$62,410,000	\$35.66			

	Pre- Production	Production			
Item	Cost	Cost	Cost/Ton		
Labour	\$6,539,000	\$26,596,000	\$15.20		
Materials	\$2,780,000	\$7,464,000	\$4.27		
Equipment	\$1,550,000	\$11,886,000	\$6.79		
Other Charges	\$2,775,000	\$16,464,000	\$9.40		
Total	\$13,644,000	\$62,410,000	\$35.66		

It should be noted that the labour rates and material costs used in Rosebud have been obtained from Lac's Bullfrog Mine and are therefore consistent with current practices in Nevada at a similar Lac operation. Although the mine operating costs for Rosebud were calculated independently, they are similar to current operating costs at Bullfrog's underground mine (\$38.16/ton).

APPROXIMATE COMPARISON OF PREPRODUCTION CAPITAL COSTS VS. ANNUAL PRODUCTION RATES AT SELECTED UNDERGROUND HARDROCK MINES



LEGEND

(MILLIONS OF TONS)

- ROSEBUD PROJECT
- WITH MILL
- WITHOUT MILL

The total site costs include milling, administration and tailings disposal and are summarized below:

	Cost/t
Mining	\$35.66
Mill	\$13.50
Tailings	\$0.40
Administration	\$1.80
TOTAL	\$51.36

9.2 CAPITAL COSTS

The total capital costs include mining equipment and related stationary equipment and surface and underground infrastructure. A breakdown is provided below. Table 9.2 provides the total capital for the mine including mine development and mining equipment and also includes the mill, surface infrastructure, tailings dam and related capital costs. The costs have been divided into pre-production and during minelife. A complete breakdown is shown in Appendix IV.

9.3 COMPARISON OF ROSEBUD COSTS WITH OTHER OPERATIONS

Figure 12 and Figure 14 are graphs showing the relationship between operating costs and productivities and between production rate and pre-production capital required. The information used to generate these graphs is based on cost data base within BEA from several mines primarily in Eastern Canada. The results indicate that the capital and operating costs and the productivities generated at Rosebud are generally consistent with typical underground mines in Eastern Canada, particularly when the exchange rate is taken into consideration.

TABLE 9.2 CAPITAL COSTS

	Pre-Production Capital Cost \$000's	Total Life \$000'S
Development	5,084	8,171
Mining Equipment	7,218	7,218
Plant (Mill)	9,500	9,500
Tailings Dam	2,500	2,500
Infrastructure and Surface Equipment	2,958	2,958
Diamond Drilling	1,000	1,000
Environmental and Permitting	500	500
EPCM 10%	3,100	3,100
Closure	-	500
TOTAL	\$31,860	\$35,447

10.0 ECONOMIC ANALYSES

Several economic analyses have been carried out using production rates of 1,000 tpd and 750 tpd at cut-off grades of 0.10 oz/t and 0.15 oz/t and assuming a mine operation of 5 days, 2 shifts per day and 7 days, 3 shifts per day. An initial review of the different alternatives indicate that the two realistic scenarios are as follows:

- 1. A production rate of 750 tpd at a 0.15 oz/t cut-off. A higher daily production rate cannot be sustained from Rosebud at this cut-off grade because the total mineable reserves are approx. 1.3 million tons.
- 2. A production rate of 1,000 tpd at a 0.10 oz/t cut-off. This rate can only be sustained at the lower cut-off because the reserves have now increased to approx. 1.6 million tons.

In both cases a 7 day and a 5 day mining option were evaluated. This permits the annual production rate to be increased substantially. BEA feels that a 5 day, 2 shift per day option for mining with the mill operating on a 7 day per week basis is the most realistic and practicable. This permits backfilling and mucking and services to be carried out during the graveyard shift and weekends for the mine and ensures that the extraction rate from the relatively small reserve can be sustained.

The economic analyses for the different cases are shown in Table 10.1. All options are in constant 1992 U.S. dollars at \$360/oz gold and \$4/oz silver. A 10% discount rate was used. The backup spreadsheets for all the options are presented in Appendix V.

The options shown on Table 10.1 do not include depreciation or taxes.

TABLE 10.1

		ECC	NOMIC ANAL	YSES - BASE CAS	SE						
	Production Rate										
Option	Daily	Annual	Cut-Off (oz/t)	NPV (millions \$)	IRR %	Comments					
1	1,000	250,000	0.10	0.77	11	-					
2	1,000	350,000	0.10	2.78	15	Production rate high at current mineable reserves					
3	750	187,500	0.15	0.70	11	-					
4	750	262,000	0.15	2.83	14	Production rate high at current mineable reserves					
	A. Capital and operating costs same in all above base case scenarios. B. Mine runs at 5 days, 2 shifts or 7 days, 3 shifts										
		× 15.5		TO BASE CASE							
	Product	ion Rate									
Option	Daily	Annual	Cut-off oz/t	NPV Millions \$	IRR %	Comments					
5	750	187,500	0.15	2.6	13	Capital reduced to reflect lower tonnage					
6	750	187,500	0.15	(1.13)	8	As above, but operating costs increased by 10%					
7	750	262,000	0.15	4.33	17	Capital reduced to reflect lower tonnage, operating costs as in base case.					
8	750	262,000	0.15	0.25	10	Capital reduced as above & operating costs increased 10%					
	IMPACT OF GOLD PRICE ON OPTIONS 7 & 8										
9	750	187,000	0.15	(3.42)	5	Gold price reduced by 10%, capital reduced, operating costs constant					
10	750	187,000	0.15	8.65	21	As above, but with gold increased to 10% above base case.					
11	750	262,000	0.15	(2.23)	6	Same as Option 9					
12	750	262,000	0.15	10.90	27	Same as Option 10					

LOSTION O O AO A OUT OFF ODADE									
SENSITIVITIES ON 1000 TPD (250,000 tpy) OPTION @ 0.10 oz/t CUT-OFF GRADE									
13	1000	250,000	0.10	7.7	21	Grade increased by 10%			
14	1000	250,000	0.10	(6.2)	0	Grade decreased by 10%			
15	1000	250,000	0.10	6.7	17	Ore reserves increased by 600,000 tons			
16	1000	250,000	0.10	10.2	19	Ore reserves increased by 1.1 million tons			
	SENSITIVITIES ON 750 tpd (187,500 tpy) @ 0.15 oz/ton CUT-OFF								
17	750	187,500	0.15	6.7	18	Grade increased by 10%			
18	750	187,500	0.15	(5.3)	3	Grade decreased by 10%			
19	750	187,500	0.15	8.3	18	Ore reserves increased by 300,000 tons			
20	750	187,500	0.15	12.9	20	Ore reserves increased by 900,000 tons			
SENSITIVITIES TO GOLD PRICE									
21	1000	250,000	0.10	7.7	21	Gold price increased 10%			
22	1000	250,000	0.10	(6.2)	0	Gold price decreased 10%			
23	750	187,500	0.15	6.7	18	Gold price increased 10%			
24	750	187,500	0.15	(5.3)	3	Gold price decreased 10%			

The following comments are made to put this table into perspective:

1. Within the base case, the two most attractive options are 1,000 tpd at 7 days per week or 750 tpd at 7 days per week at cut-offs of 0.10 and 0.15 oz/t respectively. The options of operating on 5 days per week basis with both the 750 tpd and 1,000 tpd alternatives at the different cut-off grades are marginal.

It should be noted that at current mineable ore reserves, a production rate based on mining at 7 days/week (350,000 tpy) is not considered realistic and sustainable.

- 2. It is interesting to note that the established cut-off grade in Section 4.0 of the report of 0.10 oz/t is confirmed by the economic evaluations and is, therefore, a valid cut-off grade.
- 3. Alternatives examined included modifying the 750 tpd option by reducing the capital slightly (to reflect the lower production rate) and increasing the operating costs by approximately 10%. It is obvious that small changes to the operating cost make these alternatives marginal.
- 4. Sensitivities to gold price at +/- 10% from the base (\$360/oz) are shown in Options 9 12 and again indicate that a 10% drop in gold price would make these alternatives uneconomic.
- 5. The project does not seem to be sensitive to the cut-off grade because the ore reserves do not change dramatically when cut-off grades are adjusted. The three most sensitive areas for this project are the total reserve (relatively small to justify the capital

expenditure), the metal price and the mineable grade.

6. Sensitivities to changes in grade and ore reserves are shown on options 13 through to 20 for production rates of 1000 tpd and 750 tpd at cut-off grades of 0.10 and 0.15 oz./ton, respectively. Project economics are significantly enhanced by increasing the ore reserves by between 300,000 to 600,000 tons and improve dramatically when the ore reserves are increased by an additional one million tons at the current mineable grades.

Grade changes also affect the NPV and can change it from \$7 million cost surplus to a cash deficiency of over \$6 million.

The above discussion indicates that the Rosebud project does appear to have potential but requires increased ore reserves and/or higher mineable grades. Lac geologists have a high degree of confidence in the estimated mineable grade, which may be somewhat conservative because of the dilution used. Opportunities may exist to further enhance the grade as mining progresses. Both the capital and operating costs have been estimated from basic principles and are considered reliable and accurate to a narrower range than the \pm 25% level generally used for prefeasibility studies.

In order to obtain an acceptable rate of return of about 18%, the follow-up and program for Rosebud should focus on:

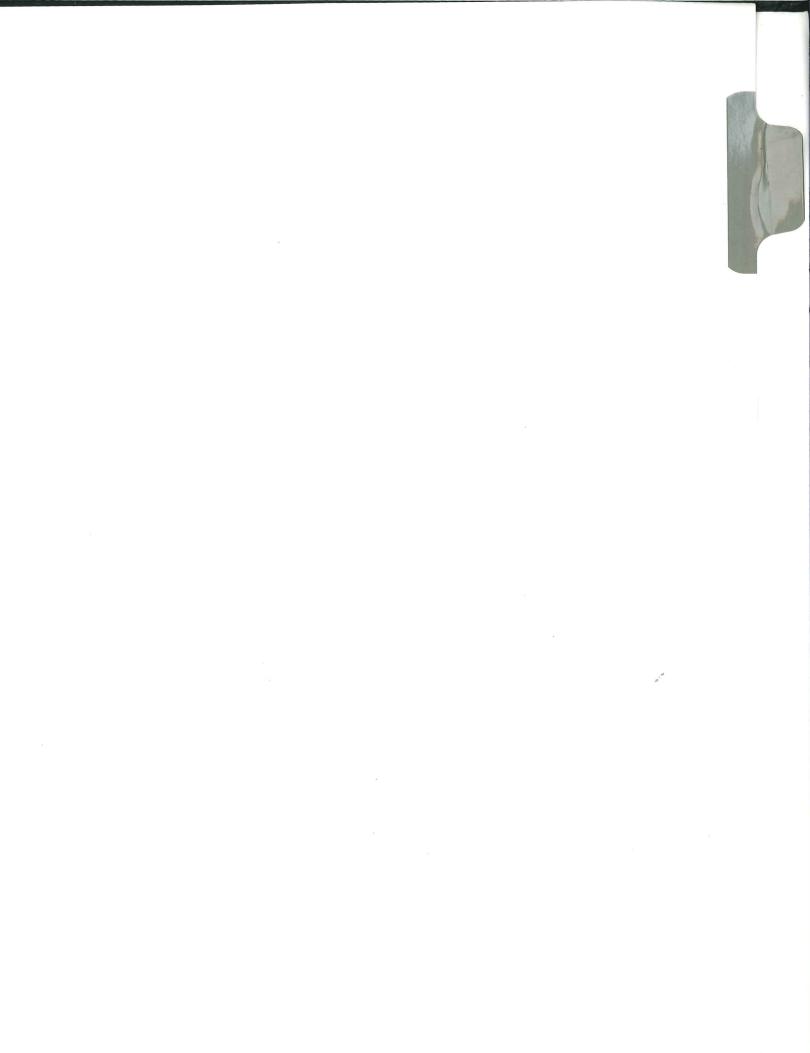
- A production rate of 1000 tpd and 250,000 tpy at a 0.10 oz./t cut-off.
- A mineable reserve base of between 2-3 million tons (an increase of about one million tons over the current mineable reserves).
- The price of gold being maintained at least in the \$350 to \$360/oz. range or higher and preferably being in the \$400/oz range.

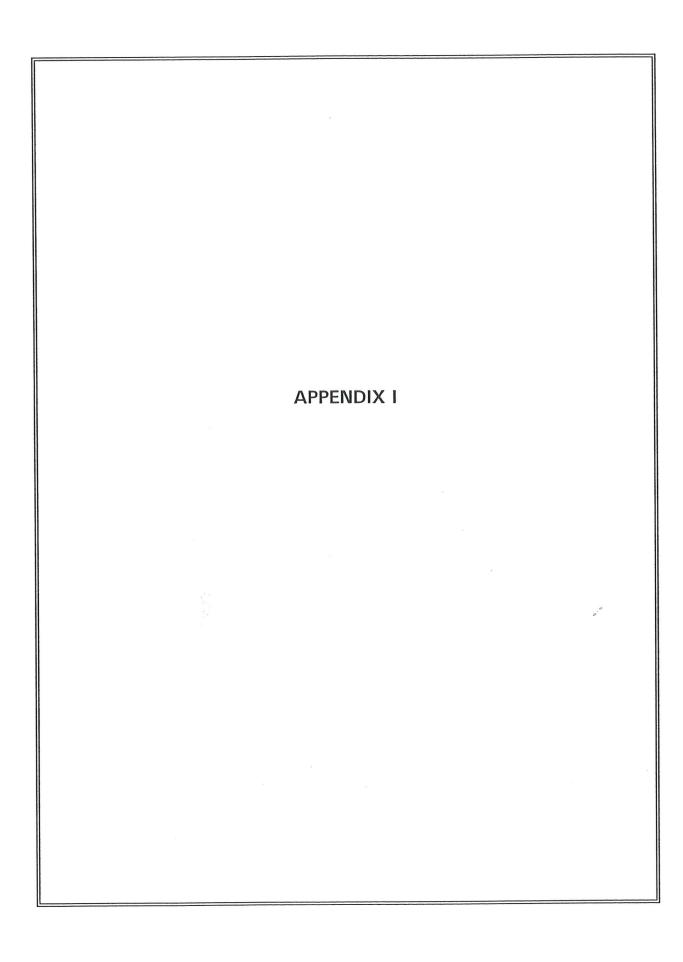


11.0 LIST OF DOCUMENTS REVIEWED

A list of documents reviewed and reported in this summary is given below in chronological order.

- Rosebud Exploration Project. Internal Company Memorandum from John F. Cook, Lac Minerals to Peter Allen, Lac Minerals. September 7, 1990
- Rosebud Project 1991 Resource Calculations. Tim Kuhl, Lac Minerals (USA) Inc. January 3, 1991.
- 3. Rosebud Project Preliminary Rock Mechanics Assessments. Dennis C. Martin, Piteau Associates Engineering Limited. February 15, 1991.
- 4. Meeting Rosebud with Beacon Hill. Memorandum to File. Hans de Ruiter, Lac Minerals. March 8, 1991.
- Reserve Audit & Conceptual Mine Plan Rosebud Property, Dozer Hill Deposit, Pershing County, Nevada. Beacon Hill Consultants Limited. March 1991.
- 6. 1990 Annual Progress Report, Rosebud Project, Pershing County, Nevada. N.H. Brewer, Lac Minerals (USA) Inc. March 1991.
- 7. Rosebud Project Metallurgical Review. Internal Company Memorandum from George Hope, Lac Minerals to Bob Thomas and Tim Kuhl, Lac Miners (USA) Inc. June 12, 1991.
- 8. Comments: Hydrologic Study, Rosebud. Internal Company Memorandum from W.Quesnel, Lac Minerals to Tim Kuhl, Lac Minerals (USA) Inc. September 1991
- 9. Cost Recovery Money Models for Rosebud Decline. Internal Company Memorandum from Tim Kuhl, Lac Minerals (USA) Inc. to Craig Nelsen, Lac Minerals. December 4, 1991.
- 10. Rosebud Evaluation High Grade Case. Internal Company Memorandum from Hans de Ruiter, Lac Minerals to Craig Nelsen, Lac Minerals. January 17, 1992.
- 11. Rosebud Preliminary Geotechnical Evaluation of Diamond Drill Core. Internal Company Memorandum from W. Quesnel, Lac Minerals to Bob Thomas, Lac Minerals. February 25, 1992.
- 12. Plan of Operations for Underground Exploration Activities, Rosebud Project, Pershing County, Nevada. Debra W. Struhsacker, Consultant. March 1992.





ROSEBUD STUDY LAC MINERALS PREFEASIBILITY DOCUMENTATION SUMMARY

The Rosebud property, located some 40 miles north of Lovelock, Pershing County, Nevada, comprises an 8,400 acre claim block covering numerous volcanic hosted epithermal gold-silver prospects, and is jointly owned by Lac MInerals (USA), Inc and Equinox Resources Limited. Surface drilling of the Dozer Hill area has outlined a mineralized zone (generally tabular in nature), over a strike length of approximately 2,000 feet, with an average width of 300 feet and mean thickness of 40 feet.. Gold mineralisation has also been intersected in other parts of the property.

Various reports and memorandum concerning the Rosebud property have been reviewed and are summarised herewith.

SUMMARY

Resource

The resource, classified as probable and possible reserves, is estimated as:

1,400,000 tonnes at a grade of 0.25 oz Au per ton.

Mining

The deposit is suitable for extraction by drift and fill underground mining methods. Access by decline is likely, given the shallow depth.

Mineral Processing

Run-of-mine ore would be amenable to cyanidation with recoveries of 95 % indicated at a cyanidation consumption less than 0.5 lb/t.

Environment & Infrastructure

The property lies more than 5 000 feet above sea level in scrubby vegetation, situated relatively close to Lovelock, (1.5 hours by gravel road), and the main Western Pacific rail line. Another mine, Hicroft, lies about 10 miles to the north which is supplied with power. Water requirements are likely to be met from underground sources.

The issue of environmental permits should proceed in a straightforward manner.

Project Schedule

Production Scenario

Rates of production considered to date range from 250,000 tpa to 500,00 tpa, giving rise to a mine life ranging from 6 to 3 years.

Estimated Capital & Operating Costs

Rate of Production		Operating Costs Capital Cost			Total		DCF			
tpa	oz/annum	\$/t	\$/oz	\$/t	\$/oz	\$	\$/t	\$/oz	IRR %	P/Back
										years
250,000	59,375	55.00	232.00	20.00	80.00	30,000,000	70.00	312.00	20	3.3
500,000	118,750	47.00	198.00	15.00	63.00	45,000,000	63.00	261.00	45	2.0

Exploitation Philosophy

Provided a resource of 1.5 million tonnes at a grade of 0.25 oz/t exists the project should be exploited.

Future Action

Continue with exploration.

Study north side of the South Equinox area.

Check power supply to Hicroft mine.

Start an hydrological scoping study.

Carry out heterogeneity tests on samples to determine cutting policy.

Keep Pershing County informed of progress.

A properly designed verification and validation program is critical to the ability to upgrade the reserves.

GEOTECHNICAL ASPECTS

The geotechnical database should be expanded and a detailed rock mechanics assessment should be conducted during the feasibility and detailed design studies. Detailed assessments of rock cores or rock testing were not conducted for the Piteau report.

Rock Mass Characteristics

The orebodies occur primarily within a sequence of Miocene volcanic and pyroclastic rocks (Lower Bud Tuff), which have variable strength, degree of alteration and fracturing. Alteration by silicification and by bleaching and argillicification have both strengthened and weakened respectively, the rock mass. A thrust fault, the South Ridge Fault, shallow dipping, defines the bottom of the Lower Bud Tuff. The South Ridge Fault is charaterised by a zone of intensely sheared and altered rock of low quality, ranging in thickness from 2 feet to 30 feet. The Dozer Tuff zone, generally less altered and more competent than the Lower Bud Tuff sequence rocks, lies below the fault. The Bud Tuff overlies the Lower Bud Tuff, and like the Dozer Tuff, is more competent than the Lower Bud Tuff.

Rock mass quality varies throughout the deposit, Table 1.

Table 1 Rock Mass Quality, Rosebud Property

Geological Sequence

Rock Mass Quality

Bud Tuff

Good to Very Good

Lower Bud Tuff

Upper Section Good to Fair

Lower Section Section 00

Poor to Very Poor

Sections 600 to 1600

Fair to Good (some poor zones)

Poor within 50 feet to 75 feet of fault

Dozer Tuff

Fair to Good

There appears to be no clear relationship between the ore zones and rock mass quality.

The water table lies 200 feet below surface. Otherwise groundwater conditions within the rock amss or along faults are unknown.

In Situ Stresses

The Piteau report offers no comments with respect to in situ stress levels or direction.

Engineering Design

Piteau report suggests working spans based upon use of the NGI classification system, Table 2.

Table 2 Excavation Spans, Temporary Mine Openings, (NGI Classification)

Rock Mass Quality	Unsupported Span (m)	Rcok Bolts, Mesh & Shotcrete		
Excellent				
Unaltered	12.0 to 14.0	24.0		
Good				
Unaltered	12.0	8.0 to 10		
Altered	4.0 to 6.0	21.0 to 24.0		
Fair				
Unaltered	5.0 to 7.5	6.0 to 8.0		
Altered	2.4 to 2.7	9.0 to 12.0		
Poor				
Altered	1.5 to 1.8	6.0		
Very Poor		,		
Altered	1.5	3.0		

The span of permanent mine openings would be about one half the width estimated for temporary excavations.

No structural information is avaliable within the mine area.

Piteau suggests a variety of stoping methods:

room & pillar; longitudinal stopes; and drift & fill. Owing to limited availability of data little mining design is offered. However, Piteau suggests a field and laboratory programme to enable mine planning work to be carried out in relation to a geotechnical assessment.

A recent appraisal by Lac Minerals (Kirkland Lake) indicates that, in general, the ground is very poor with an average fracture count of up to 2 per foot, and as high as 4 fractures per foot in heavily altered zones. Consequently, it is estimated that dilution from bulk from mining methods would range from 10 % to 30 %, and controlled blasting and extensive presupport measures would be required.

Thus, selective mining methods, such as longitudinal and panel cut and fill would be demanded for most of the orebodies. Given extensive ground support, dilution might average 15 %.

The degre of rock mass alteration suggests that ingress of groundwater could adversely affect ground conditions.

GEOLOGY, & RESERVES

Gold concentrations occur at the nearby Dreamland and the Hycroft properties, in large, irregular, very non-homegneous areas of gold mineralisation, each comprising several tens of millions of tons with gold content averaging from 0.01 oz Au/t to 0.03 oz Au/t. Higher grade pods exist within these areas with resources ranging from a few thousand tons to a few million tons with gold grades from 0.1 oz Au/t to 0.4 oz Au/t, similar to the Aurora, Rawhide, Borealis and Bodie deposits.

The geological reserve is considered accurate and reasonable within the constraints of the existsing data, but insufficient for carrying out a definitive feasibility study. Important questions remain concerning the viability of samples and the impact of sampling procedures and analytical errors.

The resource estimate (BCH), classified as probable minable reserves, is estimated as:

1,146,000 tonnes at a grade of 0.24 oz Au per ton.

Estimated gold content of this resource is approximately, 275,000 ounces. A cut off of grade of 0.12 oz Au per ton applies to these probable minable reserves, with all grades above 1.00 oz Au per ton cut to 1.00 oz Au per ton.

A properly designed verification and validation program is critical to the ability to upgrade the reserves.

Beacon Hill Consultants Estimated Probable Mining Reserves, March 1991

Zone		Geologi	ical	Dilution		Produc	tion	Total
		tonnes	oz	tonnes	Au	tonnes	Au	Au oz
			Au/tonne		oz/tonne		oz/tonne	
	Α	213120	0.197	42700	0.032	255820	0.169	43351
	В	280022	0.437	38700	0.023	318722	0.387	123260
	С	63087	0.270	13300	0.041	76387	0.230	17579
	D	132971	0.205	15200	0.089	148171	0.193	28612
	Е	308534	0.198	38400	0.025	346934	0.179	62050

The reserve also includes silver at a grade of 2.00 oz Ag per ton. A mining dilution equivalent to 15 % of the in situ minable tonnage was assumed in cosideration of the mining method, and stope height and width.

Drilling programme suggested by BHC would involve two phases to upgrade reserves to probable category based upon 100 feet centres (41,500 feet RC & 4,900 feet d/drill) and subsequently to a proven category related to 50 feet centres drill sections (15,300 feet RC & 38,900 feet d/drill). There is good potential for expanding the reserves at Dozer Hill.

Potential resources within the Rosebud property are estimated to range from the current reserve of 275,000 ounces of gold to 1,500,000 ounces of gold.

Table 1. Potential Resources, Rosebud Project

Category	Total	Probability	Source
	Oz	%	
Current Reserve	275,000	90-95	BHC (Uneconomic)
High Probability Reserve	500,000	70-80	BHC
Good Probability Reserve	1,500,000	30-40	Consensus Estimate

Lac Minerals (USA) Inc have estimated geological reserves, by the method of sections utilising grade cut offs of 0.02 oz Au per ton and 0.05 oz per ton (nominal open pit cut offs), Table 2.

Table 2 Estimated Geological Resources, Lac Minerals (USA) Inc

Reserves Category	Tons	Grade oz Au per ton	Gold Ounces
Cut Off 0.02 oz Au per ton			
Probable	4,088,017	0.105	429,631
Possible	1,102,786	0.133	146,563
Totals	5,190,803	0.111	576,194
Cut Off 0.05 oz Au per ton			
Probable	1,591,720	0.210	333,942
Possible	676,659	0.194	131,250
Totals	2,268,379	0.206	465,192

The resources estimated by Lac Minerals (USA), Inc, are located both on jointly owned ground, 55 %, (Lac Minerals & Equinox), and 45 % on claims owned solely by Lac Minerals (USA), Inc.

An undiluted reserve estimate using a higher cut off grade, for extraction by underground methods, gives rise to a resource of:

1,245,350 tons at 0.248 oz Au per ton and a silver grade of 3.20 oz per ton.

The resource is still open in a several areas where encouraging intercepts have been made. For example:

170 feet at 0.559 oz Au per ton; and 45 feet at 0.202 oz Au per ton.

The most recent calculations of the Rosebud resource (January 3, 1992) indicate an in situ geological resource of approximately 2 million tons at grades of 0.25 oz Au per ton and 2.92 oz Ag per ton.

Exploration Programme

The proposed exploration programme would develop a 2,300 feet long ramp and 2 drifts a total length of 2,500 feet. Drilling would be carried out underground, producing some 60,000 feet of core, from 200 feet sections directed through the ramp and drifts.

Development would produce approximately 135,000 tons of waste rock and up to 15,000 tons of ore from selected bulk sample locations in the underground workings.

The proposed underground exploration program is critical to the viability of the project and is necessary to obtain the following data:

- 1. geological data;
- 2. evaluation of mining methods;
- 3. hydrogeological and dewatering requirements; and
- 4. metallurgical charateristics of the ore.

An estimate of the tonnage of ore required to recover the costs of the exploration program indicate that 25,000 to 45,000 tons of 1.0 oz Au per ton would be needed, shipped either to Pinson or Bullfrog respectively for treatment. Such material is available in either the 159 or East zones.

MINING

The drift & fill mining method has been selected as the most appropriate technique given the assessment of rock quality and the configuration of the orebody. Drift & Fill is highly selective and provides the most effective ground support for the stopes with widths of 13 feet.

Mechanized mining has been assumed with electro-hydraulic jumbos (2), diesel powered LHDs (2), haulage trucks (1), Slingerbelt fill truck (1) and various service vehicles.

General mine layout incorporates both a ramp for haulage and a shaft for hoisting once the truck haulage becomes uneconomic.

A production level of 500 tons per day would need 4 or 5 active faces. Manpower estimated for the 3 shifts per day underground operation by Beacon Hill Consultants is 88, which compares with the Lac Minerals estimate of 63 for a 2 shifts per day setup, (Hans De Ruiter). Fill material demanded for use with the Slingerbelt truck would be minus 2 inches crushed rock with 5 % cement content.

Preproduction development of 4,000 feet of drfits and 800 feet of cross cuts. Mining would commence in two high grade zones, A & B.

Two production scenarios have been evaluated.

Department	Scenario 1	Scenario 2	Shift System
Mining	700 tpd	1,400 tpd	2 shifts per day
			5 days per week
Milling	500 tpd	1,000 tpd	3 shifts per day
			7 days per week

The viability of the Rosebud project will be dependent upon:

- 1. control of dilution to maintain ore grade;
- 2. choice of selective mining methods to cater for changes in width of orebody; and
- installation of appropriate ground support coupled with a well engineered mine extraction sequence to manage very poor to fair ground conditions.

MILLING

Limited metallurgical testwork indicates that gold can be successfully extracted with a Carbon-in-Leach plant with gravity separation. Metallurgical recovery is expected to range between 85 % and 90 %.

Tailings disposal would take place southwest of the plant and mine portal with storage of 3 million tons, (related to a mill throughput of 350,000 tons per year), demanding an area of 1,530 acre-feet, incorporating a 3 pond configuration.

George Hope reported that initial tests indicated that the ore was very amenable to cyanidation with good recovery and low cyanide consumption. Subsequent, work pointed towards leaching problems, possibly brought about, in part, by the presence of gold encapsulated in sulphides. Antimony may also create difficulties with recovery of gold. Hope established a test program requiring:

scoping leach tests on available ore sections;

2 additional leach tests; and
process optimisation encompassing gravity concentration and leaching.

A SAG mill would be needed for the 1,000 tons per day milling operation.

Water requirements are gauged to be 200 gpm.

Manpower for the mill is estimated as:

18 hourly paids;

12 maintenance crew; and

8 supervisors.

INFRASTRUCTURE & ENVIRONMENT

Hallam Knight Piesold Limited have reviewed environmental work done to date and have made the following comments and recommendations.

- Project permitting should be approached on the basis of a full Environmental Impact Statement (EIS).
- 2. A single comprehensive EIS document covering both federal and state requirements should be prepared.
- 3. Baseline studies should be expanded to include the installation of on-site meteorological and hydrological monitoring facilities.
- 4. Environmental work done to date has omitted a contingency for fatal flaws involving cultural resources, endangered species and the potential for acid generating waste.
- The estimated costs for environmental work are fair. The upper limit of the estimate should be used for feasibility studies.

The property lies more than 5 000 feet above sea level in scrubby vegetation, situated relatively close to Lovelock, (1.5 hours by gravel road), and the main Western Pacific rail line. Another mine, Hicroft, lies about 10 miles to the north which is supplied with power. Water requirements are likely to be met from underground sources.

A "Plan of Operations for Underground Exploration Activities" has been submitted by Lac Minerals (USA), Inc to the US Department of Interior, Bureau of Land Management, Winnemucca, Nevada. The Plan describes the proposed underground exploration activities, reclamation for the proposed project, planned environmental controls, and environmental baseline data collected to date for the project area.

CAPITAL & OPERATING COSTS

Operating costs have been estimated from \$70 per ton to \$57 per ton for the 500 tpd option and the 1,000 tpd option respectively.

Similarly, capital costs range from \$27.2 million to \$35.2 million for the 500 tpd option and the 1,000 tpd option respectively.

Labour rates have been based upon the nearby Gooseberry mine and include 38 % overheads.

DISCOUNTED CASH FLOW

BHC alternative cases for evaluation were based upon:

gold price of \$375 per oz; and

metallurgical recovery of 89 %.

The project is:

most sensitive to grade and gold price;

less sensitive to operating costs; and

least sensitive to capital expenditure.

1. The 500 tpd option is uneconomic, and to be viable requires a:

10 % increase in grade;

10 % reduction in capital expenditure; and

20 % decrease in operating costs.

2. The 1,000 tpd option is economic, but is based upon a doubling of the reserves.

The value of the property has been assessed by two methods which indicate a range of 6 million to 10 million. The market value method (accurate to +/-25 %), assumes gold at 10 per oz of

gold and land at \$500 per acre.

A recent evaluation (January 17, 1992, Hans De Ruiter), using an uncut high grade (0.31 oz Au per

ton) and assuming a metallurgical recovery of 92 % indicates a significant improvement in the

financial return of the project, given the 50 % increase in grade (cut grade of 0.226 oz Au per ton),

at a gold price of \$350 per oz and a 15 % discount rate.

High Grade:

26 % IRR & \$7 million NPV

Cut Grade:

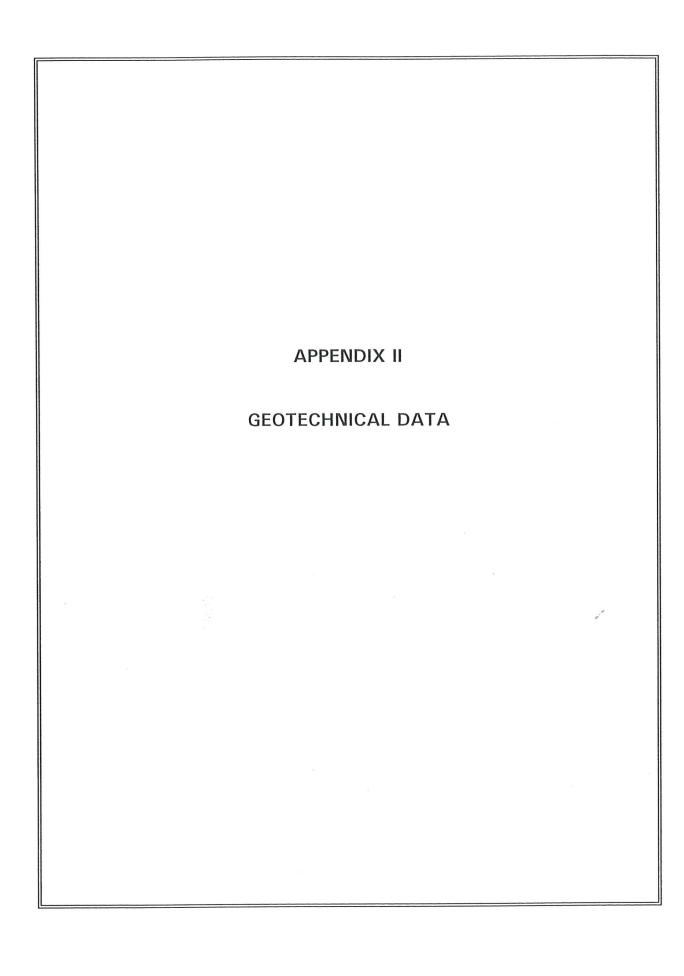
(4 %) IRR & (\$13 million) NPV

LIST OF DOCUMENTS REVIEWED

A list of the documents reviewed and reported in this summary is given below in chronological order.

- Rosebud Exploration Project. Internal Company Memorandum from John F Cook, Lac Minerals, to Peter Allen, Lac Minerals. September 7, 1990.
- Rosebud Project 1991 Resource Calculations. Tim Kuhl, Lac Minerals (USA) Inc. January 3, 1991.
- Rosebud Project Preliminary Rock Mechanics Assessments. Dennis C Martin, Piteau Associates Engineering Limited. February 15, 1991.
- Meeting Rosebud with Beacon Hill. Memorandum to File. Hans de Ruiter, Lac Minerals. March 8, 1991.
- Reserve Audit & Conceptual Mine Plan Rosebud Property, Dozer Hill Deposit, Pershing County, Nevada. Beacon Hill Consultants Limited. March 1991.
- 6. 1990 Annual Progress Report, Rosbud Project, Pershing County, Nevada. N H Brewer, Lac Minerals (USA), Inc. March 1991.
- Rosebud Project Metallurgical Review. Internal Company Memorandum from George Hope, Lac Minerals, to Bob Thomas & Tim Kuhl, Lac Minerals (USA) Inc. June 12, 1991.
- 8. Comments: Hydrologic Study, Rosebud. Internal Company Memorandum from W Quesnel, Lac Minerals, to Tim Kuhl, Lac Minerals (USA) Inc. September 1991.
- Cost Recovery Money Models for Rosebud Decline. Internal Company Memorandum from Tim Kuhl, Lac Minerals (USA) Inc to Craig Nelsen, Lac Minerals. December 4, 1991.
- Rosebud Evaluation High Grade Case. Internal Company Memorandum from Hans de Ruiter, Lac Minerals to Craig Nelsen, Lac Minerals. January 17, 1992.

- Rosebud Preliminary Geotechnical Evaluation of Diamond Drill Core. Internal Company Memorandum from W Quesnel, Lac Minerals to Bob Thomas, Lac Minerals. February 25, 1992.
- Plan of Operations for Underground Exploration Activities, Rosebud Project, Pershing County, Nevada. Debra W Struhsacker, Consultant. March 1992.



HYDROLOGY

The hydrogeological characteristics of the project area have been examined by Hydro-Geo Consultants of Lakewood, Colorado. Three monitoring wells and one borehole (RL-24F) were field-tested for permeability. Falling head and pumping tests were performed on the designated holes. The findings of Hydro-Geo Consultants may be summarized as follows:

- ♦ Local groundwater levels vary across the project area from approximately 50 ft. below the ground surface in the axis of drainage to 250 ft. below the ground surface on the hillsides.
- Groundwater is present in the volcanic breccia and tuff rocks which form the ore deposits and in the hangingwall of the project area.
- Recharge to the water table originates primarily from direct infiltration from precipitation. The Rosebud Canyon is the main source of recharge.
- ♦ The prevalent permeability and porosity of the ground are of secondary (fracture) character. The directional permeability is affected by northeast southwest orientated, sub-vertical faults.
- Significant quantities of groundwater inflow are possible during phases of mine development in vicinity of the South Ridge Fault.
- ♦ Typical ground water chemistry sampled from the site exceeds the State and Federal drinking water standards.
- ♦ The pre-mining water table is at 4950 ft. elevation in the vicinity of the proposed decline portal. During the decline development, groundwater in the general area can be expected to flow toward the decline from the northeast. The majority of inflow will be associated with faulting.
- ♦ It is anticipated that maximum inflow into the decline will not exceed 300 gpm at any time during mining.
- ♦ Increased inflows are expected between 1700 ft. and 2600 ft. elevations where the proposed decline crosses a number of faults in the Dozer Tuff and Lower Bud Tuff.
- ♦ High inflows are anticipated when intersecting the South Ridge Fault at 2000 ft. to 2100 ft. elevation, and at 3300 ft. to 3400 ft. elevation where fracture zones are present.
- The total mine inflow, including active drainage, inflow into the decline, development drifts and ramps, was estimated in a range of 100 to 500 gpm.
- ♦ Mine dewatering must be ongoing through all the active phases of mine development and mining. Eight to twelve months of active drainage is anticipated prior to any ore recovery to reduce the residual water content in the drained stratas.

- A complete drainage of the orebody hangingwall is not possible using drainholes drilled off the proposed decline. A second dewatering system of vertical wells drilled from the surface may be required. The efficiency of the drainage program will be dependent on the clay content and type of clay present within the orebody. A high content of montmorillonitic clay would hamper the drainage effort.
- Two additional test boreholes were recommended to further evaluate potential high inflow areas in the South Zone and Far East Ore Zone.

MINING HISTORY

The Rosebud/Dozer Hill area has been previously mined in adjacent near surface workings. The Dreamland mine is located approximately one mile north west of Rosebud. A recent description of the workings by Golder Associates is as follows:

Dreamland Mine is located several thousand feet west of the surface exploration at Rosebud. It consists of extensive shallow workings developed in sericitic and argillically altered Chocolate unit, which is considered to have similar mechanical characteristics to moderately clay-altered LBT. The workings are less than 100 feet below ground surface and are dry.

Workings generally dip between 20 and 30 degrees, and appear to follow a persistent flat-dipping structure. The main workings consist of an irregularly shaped stope with maximum dimensions of approximately 150 feet in each direction, ranging from a few feet up to 40 feet in height. Several small rock pillars are located at irregular positions throughout the workings, while timber posts have been used to support large spans of limited height. The largest totally unsupported span is near the updip stope entrance, and is estimated to be approximately 60 feet square. It is understood that active mining ceased in the 1930's. There are no extensive rockfalls or other indications of significant instability within the stope or an adjacent unsupported drift.

The Dozer Hill drift is an approximately 6 x 5 ft. unsupported drift through the Bud unit into the LBT. It is located within Dozer Hill, which directly overlies the North mineralized zone. The Bud is predominantly unmineralized, low strength geotechnical unit, while the LBT is the primary host for mineralization in some ore zones. There is no significant instability throughout the several hundred feet of drift length. The drift is dry.

A visual classification of the rock quality in both areas is generally fair to poor - based on the amount of fracturing evident in the excavation walls. It appears to be more fractured than the typical

competent LBT inspected in drill cores and core photographs pertaining to the Rosebud/Dozer Hill project.

ROCK MASS CHARACTERISTICS

DISCONTINUITIES

As indicated previously, the mineralization of the Rosebud deposit is characterized by discontinuous stockwork, dissemination and hydrothermal alteration. As a result, any jointing which may have been formerly present in the host rocks, is not evident in the diamond drill core.

As a general rule, the mineralization observed in the drill cores appeared to be disseminated within the upper elevations of all the ore zones. Stockwork mineralization characterized the central portions, which in turn graded to dissemination towards the footwall. Up to two phases of vein stockwork were observed, resulting in two random orientations of lightly infilled veins. Each stockwork episode could be infilled primarily with either quartz, calcite or clay, with occasional barytes or pyrite. The stockwork "sets" could contain either the same or different infilling material. Clay infill resulted in a more highly broken drill core.

More regional hydrothermal alterations overprint the disseminated and stockwork mineralization. Depending on the ore zone, these overprints may have been either progressive where silicification has welded the rock texture, or regressive where kaolinization has reduced the rock strength. Drill core recovered from higher areas of kaolinization, such as the South Zone, would typically be more broken.

RQD has been measured in a number of recently drilled diamond drill holes which have been geotechnically logged. Observations of the split core, geotechnical logs and core photographs indicate that the RQD's recorded are inclusive of drilling induced breaks and represent low values. It is felt that the drilling induced fractures are a reflection of rock strength and represent either clay infill within the stockwork or friable zones resulting from kaolinization. Consequently, the RQD does not truly represent the rock mass quality which is dependent upon the degree and nature of the hydrothermal alteration.

INTACT ROCK STRENGTH

As described in the previous section, the rock strengths throughout the project area vary and are dependent on the degree of hydrothermal alteration.

To date no laboratory tests for intact rock strengths have been conducted. However, samples have been prepared and forwarded to McKay School of Mines, Reno, for unconfined compressive strength testing. The results are expected in the immediate future.

Visual estimation of intact rock strengths were made during examination of the drill core. These estimates were later confirmed following the calculation of point-load index tests which had been performed on core from the most recent drill holes located in the far East Zone. The range of strengths are summarized as follows:

POINT, LOAD INDEX HOLES RL263, RL26 4, RL265 - EAST ZONE

	POINT-LO		EQUIVALENT UCS* (psi)			
ROCK TYPE	Diametral	Axial	Diametral	Axial		
1. Chocolate Tuff	461	387	11,000	9,300		
2. Bud Tuff	617	330	14,800	7,900		
3. Altered Bud Tuff	140	87	3,300	2,000		
4. LBT	659	583	15,800	14,000		
5. Altered LBT	198	174	4,700	4,100		
6. Dozer Tuff	640	505	15,300	12,000		
7. Altered Dozer Tuff	311	277	7,400	6,600		
8. SRF/Silicified LBT	499	355	11,900	6,100		

* The equivalent UCS has been obtained from the point-load index, (Is_{50}) where: UCS = 24 Is_{50}

From these results, it can be seen that:

- Unaltered or silicified rock types have strengths in excess of 10,000 psi.
- Generally, regressive hydrothermal alteration has resulted in a strength reduction of approximately 50 percent.
- The diametral strengths are consistently up to 50 percent higher than the axial strengths. This indicates a strength anisotropy with the weaker direction in the vertical plane for a vertical borehole.

ROCK MASS QUALITY

Previous estimates of the rock mass quality for the Rosebud project have been made by Piteau Associates using the NGI rock mass classification system. Following examination of the drill core, drill logs are core slides, BEA has confirmed these values which are reproduced as follows:

ROCK QUALITY	DEGREE OF	Q VALUE	ALLOWABLE TEMPORARY MINE OPENING SPANS (m) ¹				
(RQD)	ALTERATION		Unsupported	Rockbolts and Mesh	Rockbolts, Mesh and Shotcrete ²		
Very Poor (0 to 25)	Altered	0.02	1.5	•	3		
Poor (25 to 50)	Altered	0.02 to 0.04	1.5 to 1.8		6		
Fair (50 to 75)	Altered	0.08 to 0.12	2.4 to 2.7	-	6 to 8		
	Unaltered	0.5 to 1.5	5.0 to 7.5	9 to 12 ²	9 to 12 ²		
Good	Altered	0.6 to 0.7	4 to 6	-	8 to 10 ²		
(75 to 90)	Unaltered	4.5 to 5.4	12	21 to 24 ²	21 to 24 ²		
Excellent (90 to 100)	Unaltered	5.4 to 6.3	12 to 14	24	24 ²		

Note:

- Spans of permanent mine openings should be approximately one-half of the spans indicated for temporary mine openings.
- Shotcrete may not be required for openings in unaltered ground depending on the strength and orientation of the fractures.

It should be noted that the NGI rock mass classification was developed for application in jointed rock masses. This case does not strictly apply to the Rosebud project area where hydrothermal alteration of the rock strength governs the rock mass quality. The rock mass quality is seen to vary throughout the deposit in the following general manner:

ROCK MASS QUALITY	, ROSEBUD PROPERTY				
GEOLOGICAL SEQUENCE	ROCK MASS QUALITY				
Bud Tuff	Good to very good				
Lower Bud Tuff					
Upper Section	Good to fair				
Lower Section	Section 00 to 600 Poor to very poor				
¥	Sections 600 to 1600 Fair to good (some poor zones) Poor within 50 ft to 75 ft. of fault				
Dozer Tuff	Fair to good				

Based on the NGI classification, which has been modified to reflect any areas which contain reduced rock strength, it is suggested that:

- Very poor to poor ground conditions apply to the South Ridge Fault and the South ore zone between section 00 and section 600. The hangingwall conditions in this area would be classified as good to fair.
- ♦ Ground conditions in the mineralized Lower Bud Tuff between sections 600 to 1600 are classified as fair to good, with poor ground within 50 75 ft. of the South Ridge Fault. The hangingwall conditions in this area would be classified as good to fair.
- Fair to good ground conditions exist throughout the East Zone.
- ♦ The condition of the Dozer Tuff can be described as fair to good throughout the project area.

INSITU STRESS

The magnitude and direction of insitu stress have not been measured in the Rosebud project area. Measurements have been made at the Nevada Nuclear Test Site, from which a direct comparison is considered reasonable for a prefeasibility level of analysis. The results from the test site for volcanic tuffs at depths of 1,158 ft. show the vertical stress is roughly equal to the overburden pressure and the horizontal to vertical in-situ stress ratio is 0.9.

This would result in a corresponding vertical in-situ stress for Rosebud at the maximum proposed mining depth of 800 ft. of \pm 700 psi. The orientation of the stress field is unknown. It may be assumed that a near uniform stress distribution exists. Locally, buckling or bulging of soft, friable kaolinized areas may occur due to stress concentration effects resulting from the shape of the underground openings. Otherwise the effect of stress is not considered to be a problem area for mining.

DESIGN PROCEDURE

A preliminary assessment of allowable mining spans and possible ground support requirements for the different rock qualities encountered at the Rosebud project has been conducted by Piteau Associates using the NGI System. BEA has examined the drill core, reviewed the geotechnical logs and core slides and find that this approach is adequate for the pre-feasibility level of mine analysis.

The NGI System of rock mass classification determines a rock mass quality, Q, based on a number of parameters including RQD, the number of joint sets, joint roughness, alteration, ground stress and groundwater conditions.

	NGI ROCKMASS CLASSIFICATION					
1.	Rock	Quality Designation (RQD)				
	a)	Very Poor	0 - 25 (use nominal value of 10 where RQD < 10)			
	b)	Poor	35 - 50			
	c)	Fair	50 - 75			
	d)	Good	75 - 90			
	e)	Excellent	90 - 100			
2.	Joint	Set Number	(Jn)			
	a)	Massive, no or few joints	0.5 - 1.0			
	b)	One joint set	2			
	c)	One joint set plus random	3			
	d)	Two joint sets	4			
	e)	Two joint sets plus random	6			
	f)	Three joint sets	9			
	g)	Three joint sets plus random	12			
	h)	Four or more joint sets	15			
	i)	Crushed rock, earth-like	20			
3.	Joint	Roughness Number	(Jr)			
1	a)	Discontinuous joints	4			
	b)	Rough or irregular, undulating	3			
	c)	Smooth, undulating	2			
	d)	Slickensided, undulating	1.5			
	e)	Rough and irregular, planar	1.5			
	f)	Smooth planar	1.0			
	g)	Slickensided, planar	0.5			
	h)	No rock wall contact when sheared	1.0			
4.	Joint	Alteration Number	Ja 🦿			
	a)	Tightly healed, hard, non-softening, impermeable filling	0.75 (25 - 35 degrees)			
	b)	Unaltered, surface staining only	1.0 (25 - 30 degrees)			
	c)	Slightly altered joint walls	2.0 (20 - 25 degrees)			
	d)	Silty or sandy clay coatings	3.0			
	e)	Low friction clay coating	4.0			
	f)	Sand or clay free crushed rock	4.0			
	g)	Non-softening clay < 5 mm	6.0			

For application to the rock types present in the Rosebud/Dozer Hill project area, the strict definition of each parameter which determines Q has been loosely applied. This has resulted from the conclusion that RQD and breaks/ft. are not truly reflective of the rock mass quality, which corresponds more closely to the degree of clay alteration and friability. Each parameter has been interpreted as follows:

- A joint set number, Jn, of 3.0 corresponding to one joint set plus random joints has been applied, except where two phases of stockwork are encountered when a Jn of 4.0 has been used.
- ♦ The joint water reduction factor, Jw, has been assumed to be 1.0 to reflect that adequate drainage of the rock mass should occur during the underground development and prior to mining.
- ♦ The stress reduction factor, SRF, has been assumed as 1.0 corresponding to a relatively tight rock mass at moderate stress levels which are not anticipated to result in problems.

The relationship between Q and the support requirements of an underground excavation is determined through calculation of the equivalent dimension, De, of the excavation. This dimension is obtained by dividing the span, diameter or wall height of the excavation by a quantity called the excavation support ratio, ESR. Hence:

The excavation support ratio is related to the use for which the excavation is intended and the extent to which some degree of instability is acceptable. The following values are suggested for ESR:

	EXCAVATION CATEGORY	ESR
a)	Temporary mine openings	3 - 5
b)	Permanent mine openings	1.6
c)	Storage rooms, water treatment plants, minor road and railway tunnels	1.3
d)	Power stations, major road and railway tunnels, portals	1.0
e)	Underground nuclear power stations, railway stations, sports and public facilities	0.8

The relationship between rock mass quality, Q, and the equivalent dimension, De, which will stand unsupported is shown in Figure 2

MINING DESIGN

Beacon Hill Consultants selected drift and fill mining as the most appropriate mining method given the assessment of rock quality and the configuration of the orebody. Drift and fill is highly selective and provides the most effective ground support for stopes with widths of 13 ft.

It is envisaged that drift and fill is applicable to the South Zone ore between section 00 and section 600. The geological reserve indicates that the thickness of the ore in this area ranges from 10 ft. to 50 ft. vertically. Consequently, the thicker areas of the mineralization could be recovered with approximately four mining cuts.

From section 00 to section 300, the thinner portions of the orebody, averaging 15 ft. to 20 ft. thick could be recovered by drifting, taking down the backs, then filling. In this area poor to very poor ground conditions are anticipated, therefore, panel widths should not exceed 15 ft. Ground support should generally consist of 8 ft. long mechanical rockbolts installed on an approximate 4 ft. x 4 ft. pattern, using weldmesh as a surface restraint between the rockbolts. A contingency to install friction support (ie. Swellex) and shotcrete will be required in highly kaolinized areas and through the South Ridge Fault.

Dilution in secondary pillar recovery between the primary panels is of concern, particularly in highly kaolinized areas, ie. drainage of groundwater and backfill placed in the primary panels may leach the rock mass. Narrower secondary panels may be required. External dilution in the order of 20 percent may be anticipated.

From section 600 to section 1600 the ground conditions improve and may be described as fair. The provisional extraction widths may be increased to 20 - 25 ft. Short cablebolts will be required as supplementary ground support at the intersections of access development. Poor ground is indicated within 50 ft. to 75 ft. in the hangingwall of the South Ridge Fault. A reduced panel width of 15 ft. may be required for the first two to three cuts where applicable. External dilution of approximately 15 percent is anticipated.

Fair to good ground conditions are indicated in the East Zone between sections NW8 and NW13. The South Ridge Fault consists of a silicified hydrothermal breccia, more competent ground than the clay gouge shear zone below the South and North zones. A provisional extraction width in the order of 30 ft. to 60 ft. may be applied depending on the degree of alteration. External dilution of approximately

15 percent is anticipated.

Rock Mass Quality	Unsupported Span (FT)	Rock Bolts, Mesh & Shotcrete
Excellent Unaltered	39 to 46	24.0
Good Unaltered Altered	39 13 to 20	21.0 to 24.0 8.0 to 10
Fair Unaltered Altered	16 to 25 8 to 9	9.0 to 12.0 6.0 to 8.0
Poor Altered	5 to 6	6.0
Very Poor Altered	5	3.0

As an attempt to minimize external dilution, it is recommended that controlled blasting will be required throughout the development and ore zones.

FURTHER WORK

The current level of data acquisition pertinent to the Rosebud property is considered satisfactory for a pre-feasibility level of economic analysis.

To continue the project through to feasibility level and beyond, the confidence level in the database has to be improved. A number of areas where additional detail may be provided are recommended as follows:

♦ Investigate the cross-cutting structure

The characteristics of the cross-cutting structures which have been interpreted, trending northwest to southeast should be investigated. To date no drillhole intersections have identified the nature, i.e., gouge-filled shear zone, the thickness or the presence of groundwater associated with these structures. An exploration hole oriented northeast - southwest should be allocated to examine these features.

Written logging procedures

To preserve continuity the current logging procedures should be documented with a standardized nomenclature and symbols. For geotechnical logs this should include a clay alteration and friability index as explained below. The estimation of RQD and fractures per foot for each geotechnical domain should be continued.

Friability and Clay Content of the Ore Zone

The previous discussion has highlighted the need to identify the extent of clay and the friability of the rockmass because of its variability in the ore and surrounding rocks. Several detailed descriptions have been provided on the extent of clay around the ore zone and how it is likely to impact on stability. Most of these descriptions have been qualitative and subjective and have not developed any specific guidelines for subsequent mine design. Rosebud is a relatively shallow deposit where the ore zones have quantities of clay and can be extremely friable. It is essential that the extent of clay/friability be quantified so that areas with possible problems can be identified and location of development, etc. optimized.

It is suggested that in addition to the current geotechnical information, drill core is also logged for clay content and friability based on simple qualitative criteria as follows:

Clay Alteration/Stockwork Infill Rating

- C1 10% clay content in rock
- C2 10 30% clay content
- C3 > 30% clay content

♦ Friability/Hardness Rating

- F1 Very friable, soft, easily crumbled by hand
- F2 Friable, moderately hard, individual grains rub off when rubbing surface, can be snapped into two easily
- F3 Competent, hard, cannot be snapped into two easily or without a hammer (may be brittle).

The orebody outline can be superimposed onto the clay and friability zones. Contours may enable the relationship of high grade zones to clay content and/or friability. The primary objectives are:

- ♦ Identify any relationship between friability, clay content and the ore zone
- Determine areas within which a halo of weak friable ground exists. This may result in the relocation of access development or higher dilution allocated to a portion of the reserve.
- Identify areas where additional ground support will be required

♦ Point-Load Testing

Point-load testing of diamond drill core is an excellent index of rock strength. It is recommended that the testing continues as part of all the future drilling and logging procedures. Processing and reduction of all the data should be undertaken on site.

Laboratory Testing

The results from unconfined compressive strength tests on samples of the Rosebud rocktypes should be available in the near future. These results should be compared to the point-load strengths and a correlation established.

Slaking tests conducted on highly kaolinized stockwork from the South Zone ore, Section 00 to Section 300, are necessary to more accurately estimate the external dilution.

Triaxial testing is only seen as a requirement for the estimation of rock mass strengths at some stage beyond the feasibility level of analysis.

Monitoring

Dewatering holes drilled during the stages of ramp access development should be monitored with respect to water take and change in water pressure. It is recommended that a provisional monitoring program be established for the feasibility level of analysis. The clay chemistry for clay gouge and clay alteration zones should be examined to determine whether swelling clays such as montmorillonite are present. The presence of montmorillonite will adversely affect the drainage program and the stability of the excavations.

Analysis

Two dimensional numerical modelling and empirical support design estimations are recommended for the feasibility level of analysis.

atypical areas where the rock mass may be intersected by zones of multiple discontinuities. The width of panels is a major factor related to both stability and productivity. Wide panels result in increased productivity, giving greater output per development and production round which in turn reduces the number of equipment moves.

The necessity for ground control in stopes is a function of rock mass strength and excavation dimensions. The stope layout suggested for Rosebud is based upon an empirical approach utilising the NGI classification Q value.

In summary, cut & fill mining has been selected for the extraction of the Rosebud deposit for it has the following advantages:

flexibility and ease of modification;

ideal application for an orebody with wide variations in quality, width, roof and floor rock mass conditions;

good selectivity and productivity; and

low dilution:.

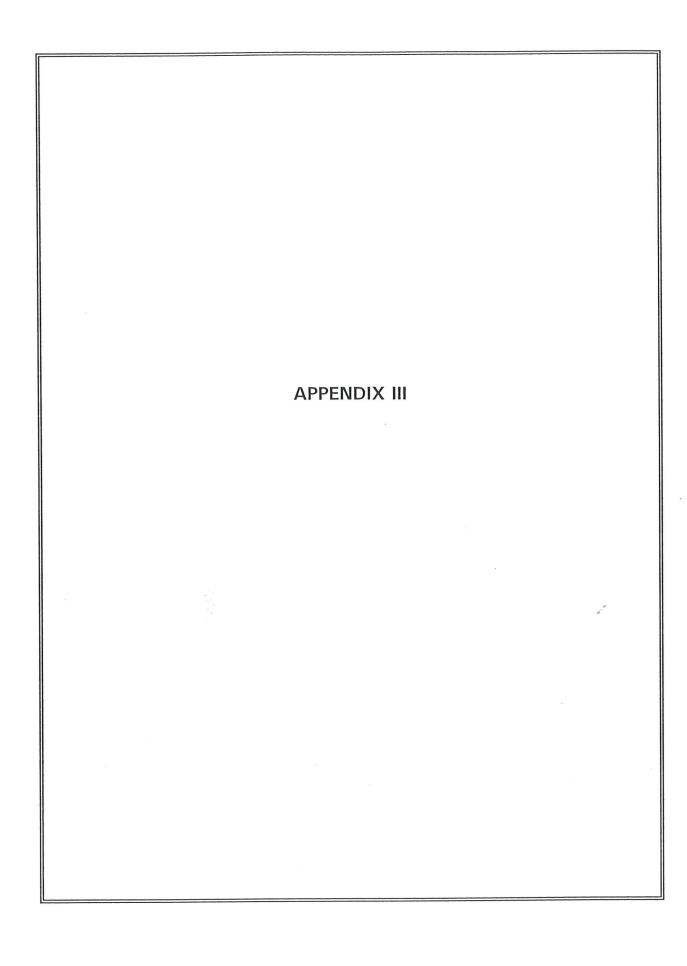
However, it is acknowledged that a disadvantage of cut & fill mining is the need to produce from multiple work places which demands:

supplying many development ends; and moving machinery and constantly extending services.

A high standard of supervision and organisation will be vital in order to produce from many workplaces.

5.2 CUT & FILL

The layout, development configuration and stoping sequence proposed for transverse primary-secondary stope cut-and-fill mining are outlined in this section. Level drawings are shown in Figures 7 to 11.



SUMMARY OF "MINABLE" RESOURCE, ROSEBUD PROJECT, PERSHING COUNTY, NEVADA. FILENAME TOTAL150.WK3 CUTOFF = 10 FEET OF 0.150 OPT AU.

			CUT		AU	CUT AU	AG
	TONS	AU OZ'S	AU OZ'S	AG OZ'S	GRADE	GRADE	GRADE
SOUTH ZONE (Northeast Sect. Orlentation)							\$7.4.IDE
DRILL INDICATED	499,700	237,653	175,291	1,929,291	0.476	0.351	3,86
DRILL INFERRED	9,700	6,889	5,415	23,736	0.710	0.558	2.45
INTERNAL DILUTION	95,300	4,296	4,296	66,735		0.045	0.70
SUBTOTAL	604,700	248,838	185,002	2,019,763		0.306	3,34
			-				
EAST ZONE (Northwest Sect. Orientation)							
DRILL INDICATED	232,100	115,060	91,342	865,019	0.496	0.394	3.73
DRILL INFERRED	83,000	24,444	24,444	181,271	0.295	0.295	2.18
SUBTOTAL	315,100	139,504	115,786	1,046,290	0.443	0.367	3.32
		- mi		1,000	0		0.02
NORTH ZONE (Northeast Sect. Orientation)	-			_			
DRILL INDICATED	128,500	33,968	28,385	917,318	0.264	0.221	7.14
DRILL INFERRED	120,000	00,000	20,000	011,010	VIEGT	0.22.	1,17
SUBTOTAL	128,500	33,968	28,385	917,318	0.264	0.221	7.14
	120,000	00,000	20,000	317,310	0.207	U.EEI	7.17
TOTAL DRILL INDICATED	860,300	386,661	295,018	3,711,628	0.449	0.343	4.31
TOTAL DRILL INFERRED	92,700	31,333	29,859	205,007		0.322	2.21
TOTAL INTERNAL DILUTION	95,300	4,298	4,296	66,735		0.045	0.70
TOTAL RESOURCE	1,048,300	422,310	329,173	3,983,370		0.314	3.80
TOTAL TEODETICA	1,040,000	422,31Q	320,173	3,303,370	0.403	0.314	3.00
<u></u>							
	-						
SOUTH ZONE (Northeast Sect. Orientation)	-						
LAC ONLY GROUND	121,600	42,420	33,096	70,596	0.349	0.272	0.58
LAC INT DILUTION	10,500	242	242	893		0.023	
EQUINOX JV GROUND	387,800	202,122	147,610	1,882,432	0.023	0.023	0.09
EQUINOX JV INT DILUTION	84,800	4.054	4,054	65,842		0.048	4.85
SUBTOTAL	604,700	248,838	185,002	2,019,763	0.048		0.78
JODIOTAL	004,700	240,030	103,002	2,019,763	V.412	0.306	3.34
EAST ZONE (Northwest Sect. Orientation)							
LAC ONLY GROUND	82,600	30,379	30,379	296,334	0.368	0.368	0.50
EQUINOX JV GROUND	232,500	109,125	85,407	749,956	0.369	0.367	3.59 3.23
SUBTOTAL	315,100	139,504	115.786	1.046,290	0.443	0.367	3.32
OODTOTAL	313,100	138,504	119,700	1,046,250	0.443	0.36/	3.32
NORTH ZONE (Northeast Sect. Orientation)	ļ		L1				
LAC ONLY GROUND	128,500	33,968	00.005	047 047	0.004	0.001	714
EQUINOX JV GROUND	120,500	33,300	28,385	917,317	0.264	0.221	7.14
SUBTOTAL	128,500	00.000	00 605	A19 p17	0.001	0.004	
SUBTUTAL	120,500	33,968	28,385	917,317	0.264	0.221	7.14
TOTAL RESOURCE	4 049 900	400 040	700 470	0.000.070	0.465	0.04.	0.00
TOTAL RESOURCE	1,048,300	422,310	329,173	3,983,370	0.403	0.314	3.80
CUSTOTAL LAC ONLY ABOUND	040.000	407.000		4 005 4 15			
SUBTOTAL LAC ONLY GROUND	343,200	107,009	92,102	1,285,140		0,268	3.74
SUBTOTAL EQUINOX JV GROUND	705,100	315,301	237,071	2,698,230		0.336	3.83
TOTAL RESOURCE	1,048,300	422,310	329,173	3,983,370	0.403	0.314	3.80
LAG MARE DE GUILLES							
LAC SHARE OF OUNCES		267,813	213,008	2,661,237			1
EQUINOX SHARE OF OUNCES		154,497		1,322,133			
TOTAL OUNCES		422,310	329,173	3,983,370			



SUMMARY OF "MINABLE" RESOURCE, ROSEBUD PROJECT, PERSHING COUNTY, NEVADA. FILENAME TOTAL 100.WK3 CUTOFF = 10 FEET OF 0.100 OPT AU.

COTOFF = 10 FEET OF 0.100 OPT AU.							
			CUT		AU	CUT AU	AG
	TONS	AU OZ'S	AU OZ'S	AG OZ'S	GRADE	GRADE	GRADE
SOUTH ZONE (Northeast Sect. Orientation)							
DRILL INDICATED	643,000	256,710	195,804	2,249,813	0.402	0.305	3.50
DRILL INFERRED	9,900	6,592	5,113	29,660	0,666	0.516	3.00
INTERNAL DILUTION	88,900						
SUBTOTAL	741,800	265,302	200,917	2,279,473	0.358	0.271	3.07
EAST ZONE (Northwest Sect. Orientation)							111
DRILL INDICATED	290,700	128,905	106,186	930,183	0.443	0.365	3.20
DAILL INFERRED	83,000	24,444	24,444	181,272		0.295	2,18
SUBTOTAL	373,700	153,349	130,630	1,111,455	0.410	0.350	2.97
					-		
NORTH ZONE (Northeast Sect. Orientation)							
DRILL INDICATED	147,800	35,808	30,547	1,018,779	0.242	0.207	6.89
DRILL INFERRED							
SUBTOTAL	147,600	35,808	30,547	1,018,779	0.242	0.207	6.89
TOTAL DRILL, INDICATED	1,081,500	423,423	332,537	4,198,775	0.392	0.307	3.88
TOTAL DRILL INFERRED	92,900	31,036	29,557	210,932	0.334	0.318	2.27
TOTAL INTERNAL DILUTION	88,900		-				
TOTAL RESOURCE	1,263,300	454,459	362,094	4,409,707	0.360	0.287	3.49
	1						
<u> </u>							
SOUTH ZONE (Northeast Sect. Orientation)							
LAC ONLY GROUND	141,200	43,963	34,639	75,370	0.311	0.245	0.54
LAC INTERNAL DILUTION	,===		0 7,000	10,070	0.011	512.12	4.4
EQUINOX JV GROUND	511,700	221,339	166,278	2.203,103	0.433	0,325	4.31
EQUINOX INTERNAL DILUTION	88,900			2,200,100		-,,,,,,,	
SUBTOTAL	741,800	265,302	200,917	2,279,473	0.358	0.271	3.07
	, , = - ;	200,002	200,011	-1414111	01000	7 1	0.07
EAST ZONE (Northwest Sect. Orientation)							
LAC ONLY GROUND	113,900	35,114	35,114	334,240	0.308	0.308	2.93
EQUINOX JV GROUND	259,800	118,235	95,516	777,216		0.368	2.99
SUBTOTAL	373,700	153,349	130,630	1,111,456		0.350	2.97
300101716	010,100	100,000	130,000	1,111,430	0,410	0.0.0	2.41
NORTH ZONE (Northeast Sect. Orientation)	 						
LAC ONLY GROUND	147,800	35,808	30,547	1,018,779	0.242	0.207	6,89
EQUINOX JV GROUND	147,000	05,000	30,041	1,010,770	V.646	0.201	0,00
SUBTOTAL	147,800	35,808	30,547	1,018,779	0.242	0.207	6.89
ODDIGIAL	147,000	05,000	30,541	1,010,178	U.246	0.201	0.00
TOTAL RESOURCE	1.263,300	454,459	362,094	4,409,708	0,360	0.287	3.49
TOTAL NEGOCITOE	1,200,000	434,438	302,009	4,403,700	0,300	0.207	3.45
SUBTOTAL LAC ONLY GROUND	402,900	114,885	100,300	1,429,389	0.285	0.249	3,55
SUBTOTAL EQUINOX JV GROUND	860,400			2,980,319		0.304	
							3.46
TOTAL RESOURCE	1,263,300	454,459	362,094	4,409,708	0.360	0.287	3.49
LIG DUADE DE DUNCTA	ļ	005					,
LAC SHARE OF OUNCES	1	288,068	233,815	2,949,352			ď
EQUINOX SHARE OF OUNCES		166,391	128,279	1,460,356			
TOTAL OUNCES	L	454,459	362,094	4,409,708			·

A Dave Blow

MINING DILUTION AND ORE LOSSES

DISCUSSION

All ore recovery is by C & F - breasting off fill tight to back.

All zones are blocked out into mining panels, primary and secondary.

PRIMARY STOPES

Dilution will be the result of:

Dilution - breaking waste at the end of the stope on each cut.

Ore Loss - fines compacted in the fill floor.

Dilution - backfill scooped during the mucking cycle.

Ore Loss - Ore left along the walls of the stope that cannot be mucked with a scoop.

Dilution - Waste dilution from the back of the stope in the final cut.

Dilution - Waste wall dilution from end panel.

SECONDARY STOPES

Dilution in addition to the above will be the result of fill from the adjacent primary stopes.

CALCULATION OF MINING DILUTION

Primary 15 Ft. Panel (Per cut) (Avg. length 60 ft.)

Waste at end of stope 3 ft.	=	68 tons	
6" backfill taken - Eq. tons	=	23 tons	
Final cut - back dilution 90 tons (avg. 4 cus)	=	23 tons	
End panel wall dilution (avg. 6 panels - 180 tons)	=	30 tons	
Total		144 tons	10.7%
Tons/cut	=	1350	10.7 /

Secondary 15 Ft. Pnael (Avg. length 60 ft.)

Primary panel tons dilution	=	144 tons	
Fill from wall sloughing Eq. tons	=	90	
Total dilution	=	234	17.3%
Tons/cut	=	1350	17.570

Secondary 10 Ft. Panel (Avg. length 60 ft.)

Waste at end of stope 3 ft.	=	45 tons	
6" backfill taken - Eq. tons	=	15	
Final cut dilution 60 tons (Avg. 4 cuts)	=	15	
Fill from wall sloughing Eq tons	=	90	
End panels	=	30	
Total	=	195	21.7%
Tons/cut	=	900	21.7%

Primary 30 Ft. Panel (Avg. length 100 ft.)

Waste at end of stope 3 ft. = 135 tons

6" backfill - Eq. tons = 75

Final cut dilution = 50

(Avg. 6 cuts)

End panels 10 panels = 30

Total = 290

Tons/cut = 4500

Secondary 30 Ft. Panel (Avg. length 100 ft.)

Primary panel dilution = 290 tons

Fill from wall sloughing Eq. tons = 150

Total = 440

Tons/cut = 4500

Primary 25 Ft. Panel (Avg. length 75 ft.)

Waste at end of stope 3 ft. = 112 tons

6" backfill Eq. tons = 47

Final cut back dilution

(Avg. 5 cuts) = 38

End panel wall 8 panels = <u>28</u>

Total tons = 225

Tons/cut = 2813

6.4%

9.8%

8.0%

Secondary 25 Ft. Panel (Avg. length 75 ft.)

	Primary dilution	=	225	
	Fill from wall slough Eq. tons	=	<u>113</u>	
	Total tons	=	338	12.0%
	Tons/cut	=	2813	12.0 /0
Primar	y 20 ft. Panel (Avg. length 65 ft.)			
	Waste at end of stope 3 ft.	=	90	
	6" backfill Eq. tons	=	38	
	Final cut back dilution (Avg. 4 cuts)	=	33	
	End wall panel 6 panels	=	_33	
	Total	=	194	8.7%
	Tons/cut	=	2241	0.7 70
Secon	dary 20 Ft. Panel (Avg. length 65 ft.)			
	Primary dilution	=	194	
	Fill from wall slough	=	98	
	Total	=	292	13.0%
	Tons/cut	=	2241	13.0 /0

0.10% CUT-OFF 1000 TPD 7 DAY/WEEK

ROSEBUD\PROD10B.WK1

TABLE 8.1: Mine Life Production Scedule

Cut-off Grade = 0.10 oz/ton (Au); 1000 tpd; 7 days/wk.

Zone		Grade	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	TOTAL
East:	Tons Au oz	0.284		175,000 49,696	210,000 59,635	75,000 21,298	0	0	0	0	0	0	460,000 130,630 1,111,455
	Ag oz	2.416		422,836	507,403	181,215	V		Ü	·			0
South:	Tons			105,000	140,000	245,000	245,000	180,000 38,089	34,500 7,300	0	0	0	949,500 200,917
	Au oz Ag oz	0.212 2.401		22,218 252,074	29,624 336,099	51,843 588,174	51,843 588,174	432,128	82,824	ō	0	0	2,279,473
North (C & D):	Tons					30,000	90,000	73,500					0 193,500
Notur (C & D).	Au oz	0.158		0	0	4,736	14,208	11,603	0	0	0	0	30,547
	Ag oz	5.265		0	0	157,950	473,851	386,978	0	0	0	0	1,018,779 0
T0T41	T		0	280,000	350,000	350,000	335,000	253,500	34,500	0	0	0	1,603,000
TOTAL:	Tons	0.226	0	71,915	89,260	77,877	66,051	49,692	7,300	0	0	0	362,094
	Au oz Ag oz	0.226 2.751	0	674,911	843,503	927,339	1,062,024	819,106	82,824	0	0	0	4,409,707

ROSEBUD\DEVT10B.WK1

TABLE 8.2 MINE LIFE DEVLOPMENT SCHEDULE

Cut-off Grade = 0.10 oz/ton (Au); 1000 tpd; 7 days/week

DEVE	LOPMENT	1	2	3	ANNUAL DE	VELOPMEN 5	NT (ft.) 6	7	8	9	10	TOTAL
PREP	RODUCTION: Ramps Levels	7800 6900										7800 6900 0
	Total	14700										14700 0
	Vent Raises	1000										1000 0 0
	DUCTION: Ramps Levels		600 2800	600 2800	3200	3200	1500	300				0 1200 13800 0
	Total		3400	3400	3200	3200	1500	300	0	0	0	15000
	Vent Raises											0 0 0
COMI	BINED: Ramps Levels	7800 6900	600 2800	600 2800	0 3200	0 3200	0 1500	0 300	0	0	0	9000 20700 0
	Total	14700	3400	3400	3200	3200	1500	300	0	0	0	29700 0
	Vent Raises	1000										1000

0.15% CUT-OFF 750 TPD 5 DAY/WEEK

ROSEBUD\PROD15.WK1

TABLE 8.1; Mine Life Production Scedule

Cut-off Grade = 0.15 oz/ton (Au); 750 tpd; 5 days/wk

Zone	O	Grade	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	TOTAL
East:	Tons Au oz Ag oz			75,000 22,387 202,299	100,000 29,849 269,732	100,000 29,849 269,732	75,000 22,387 202,299	37,900 11,313 102,228	0	0	0	0	387,900 115,786 1,046,290 0
South: Lower;	Tons Au oz Ag oz			50,000 11,951 130,452	87,500 20,914 228,292	87,500 20,914 228,292	112,500 26,890 293,518	112,500 26,890 293,518	112,500 26,890 293,518	112,500 26,890 293,518	75,000 17,927 195,678	24,000 5,736 62,617	0 774,000 185,002 2,019,402 0
North (C & D):	Tons Au oz Ag oz			0	0	0	0	37,100 6,261 202,333	50,000 8,438 272,686	50,000 8,438 272,686	31,100 5,248 169,611	0	0 168,200 28,385 917,317
TOTAL:	Tons Au oz Ag oz		0 0 0	125,000 34,338 332,751	187,500 50,764 498,023	187,500 50,764 498,023	187,500 49,277 495,817	187,500 44,464 598,079	162,500 35,328 566,204	162,500 35,328 566,204	106,100 23,175 365,289	24,000 5,736 62,617	1,330,100 329,173 3,983,009

ROSEBUD\DEVT15.WK1

TABLE 8.2 MINE LIFE DEVLOPMENT SCHEDULE

Cut-off Grade = 0.15 oz/ton (Au)

		2	A 3	NNUAL DE\	/ELOPMEN 5	NT (ft.) 6	7	8	9	10	TOTAL
DEVELOPMENT	1	2	3	7	J	Ü	·	-			
PREPRODUCTION: Ramps Levels	7800 6900										7800 6900
Total	14700										14700
Vent Raises	1000										1000
PRODUCTION: Ramps Levels Total Vent Raises		600 2000 2600	600 2000 2600	2200	2200 2200	2200 2200	1500 1500	1200 1200	500		1200 13800 15000
COMBINED: Ramps Levels	7800 6900	600 2000	600 2000	2200	2200	2200	1500	1200	500		9000 20700
Total	14700	2600	2600	2200	2200	2200	1500	1200	500		29700
Vent Raises	1000										1000

0.15% CUT-OFF 750 TPD 7 DAY/WEEK

ROSEBUD\DEVT15B.WK1

TABLE 8.2 MINE LIFE DEVLOPMENT SCHEDULE

Cut-off Grade = 0.15 oz/ton (Au); 750 tpd; 7 days/week

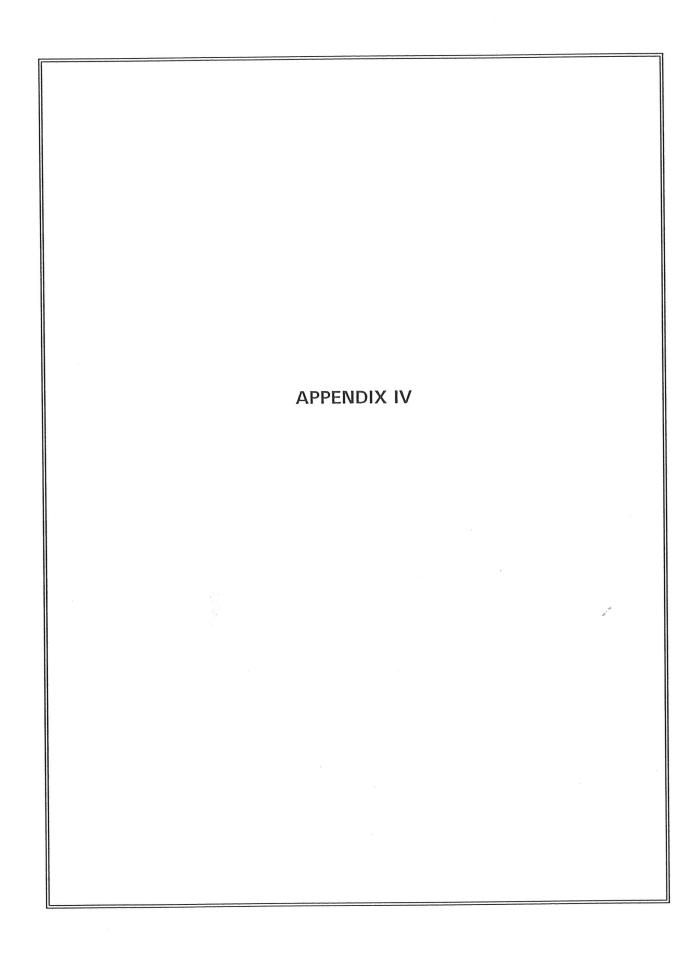
DEVE	ELOPMENT	1	2	3	ANNUAL DE	VELOPMEI 5	NT (ft.) 6	7	8	9	10	TOTAL
PREF	PRODUCTION: Ramps Levels	7800 6900										7800 6900 0
	Total	14700										14700 0
	Vent Raises	1000										1000 0 0
PRO	DUCTION: Ramps Levels		600 2800	600 2800	2800	2800	2000	600				0 1200 13800 0
	Total Vent Raises		3400	3400	2800	2800	2000	600 -a	0	0	0	15000 0 0 0 0
COM	IBINED: Ramps Levels	7800 6900	600 2800	600 2800	0 2800	0 2800	0 2000	0 600	0	0	0	0 9000 20700 0
	Total Vent Raises	14700 1000	3400	3400	2800	2800	2000	600	0	0	0	29700 0 1000

ROSEBUD\PROD15B.WK1

TABLE 8.1: Mine Life Production Scedule

Cut-off Grade = 0.15 oz/ton (Au); 750 tpd; 7 days/wk

Zone		Grade	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	TOTAL
East:	Tons Au oz Ag oz	0.298 2.697		105,000 31,342 283,218	140,000 41,789 377,625	110,000 32,834 296,705	32,900 9,820 88,742	0 0	0	0	0	0	387,900 115,786 1,046,290 0
South: Lower;	Tons Au oz Ag oz			70,000 16,731 182,633	122,500 29,280 319,608	152,500 36,451 397,880	152,500 36,451 397,880	152,500 36,451 397,880	100,000 23,902 260,905	24,000 5,736 62,617	0	0	0 774,000 185,002 2,019,402 0
North (C & D):	Tons Au oz Ag oz			0	0	0	77,100 13,011 420,482	77,100 13,011 420,482	14,000 2,363 76,352	0	0	0	0 168,200 28,385 917,317 0
TOTAL:	Tons Au oz Ag oz		0	175,000 48,073 465,852	262,500 71,069 697,233	262,500 69,285 694,585	262,500 59,282 907,104	229,600 49,462 818,362	114,000 26,265 337,257	24,000 5,736 62,617	0 0 0	0 0 0	1,330,100 329,173 3,983,009

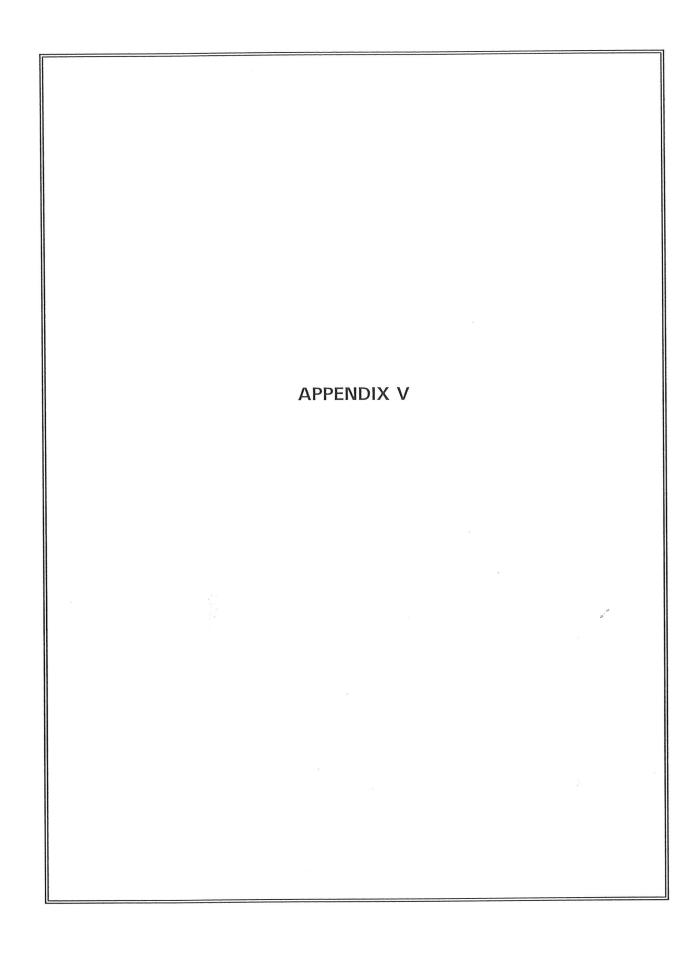


	Year	0	1 F	Subtotal Preproduction	2	3	4 Operating Co	5 st \$US	6	7	8	9	10	Total Production
MILLFEED tons		0	0	0	200,000	250,000	250,000	250,000	250,000	245,000	175,000	90,000	40,000	1,750,000
GENERAL MINE EXPENSES 301 Mine Supervision 302 Engineering 303 Mine Geology 312 Mine Ventilation System Maint 313 Mine Pumping 314 Mine Services 315 Compressed Air Generation 316 Roadbed Maintenance 317 Bit Sharpening 318 Small Tools 319 Nipping, Sanitation, etc. 332 Surface Ore & Waste Handling 333 Surface Operations 340 Allowance For Absenteeism		\$207,000 \$171,000 \$161,000 \$40,000 \$31,000 \$32,000 \$194,000 \$21,000 \$55,000 \$114,000 \$114,000 \$114,000 \$30,000	\$286,000 \$273,000 \$264,000 \$58,000 \$46,000 \$1,227,000 \$275,000 \$34,000 \$51,000 \$97,000 \$193,000 \$282,000 \$144,000	\$493,000 \$444,000 \$425,000 \$78,000 \$77,000 \$1,918,000 \$65,000 \$469,000 \$55,000 \$85,000 \$162,000 \$162,000 \$170,000 \$466,000 \$277,000	\$351,000 \$308,000 \$501,000 \$64,000 \$84,000 \$55,000 \$299,000 \$34,000 \$51,000 \$112,000 \$25,000 \$348,000 \$348,000 \$344,000	\$352,000 \$317,000 \$303,000 \$69,000 \$71,000 \$31,504,000 \$37,000 \$37,000 \$37,000 \$59,000 \$114,000 \$50,000 \$50,000	\$352,000 \$317,000 \$303,000 \$69,000 \$71,000 \$31,504,000 \$37,000 \$37,000 \$37,000 \$59,000 \$114,000 \$50,000 \$50,000	\$352,000 \$317,000 \$303,000 \$69,000 \$74,000 \$1,504,000 \$37,000 \$37,000 \$59,000 \$17,000 \$350,000 \$174,000	\$352,000 \$317,000 \$303,000 \$69,000 \$74,000 \$1,504,000 \$37,000 \$37,000 \$59,000 \$114,000 \$37,000 \$59,000 \$17,000 \$50,000	\$352,000 \$316,000 \$303,000 \$69,000 \$73,000 \$1,502,000 \$70,000 \$37,000 \$59,000 \$17,000 \$37,000 \$17,000 \$37,000	\$248,000 \$215,000 \$215,000 \$215,000 \$56,000 \$72,000 \$56,000 \$29,000 \$45,000 \$45,000 \$14,000 \$286,000 \$14,000 \$35,000 \$174,000	\$130,000 \$113,000 \$116,000 \$34,000 \$34,000 \$1,002,000 \$34,000 \$17,000 \$25,000 \$77,000 \$10,000 \$188,000 \$188,000 \$174,000	\$55,000 \$48,000 \$47,000 \$17,000 \$20,000 \$502,000 \$87,000 \$6,000 \$12,000 \$38,000 \$4,000 \$54,000 \$8,000 \$8,000	2,544,000 2,268,000 2,194,000 516,000 688,000 12,003,000 271,000 271,000 428,000 893,000 146,000 2,626,000 351,000 1,479,000
Subtotal \$/Ton Ore		\$2,088,000	\$3,353,000	\$5,441,000	\$3,751,000 \$18.76	\$3,847,000 \$15.39	\$3,845,000 \$15.38	\$3,842,000 \$15.37	\$3,842,000 \$15.37	\$3,834,000 \$15.65	\$3,286,000 \$18.78	\$2,161,000 \$24.01	\$1,001,000 \$25.03	\$29,409,000 \$16.81
DIRECT MINING COSTS 340 Underground DDH 351 Decline Development 352 Remuck Stations 353 Level Development 354 Slashing Waste 358 H/W Cablebolt Drilling 359 H/W Cablebolt Install 363 Longhole Stope Drilling 364 Longhole Stope Blasting 365 Longhole Stope Mucking 380 High Density Backfill 390 Misc Devel, Equip Replace		\$2,858,000 \$61,000 \$0 \$0 \$0 \$0 \$0 \$0 \$0 \$0	\$500,000 \$2,488,000 \$61,000 \$2,063,000 \$172,000 \$0 \$0 \$0 \$0 \$0 \$0	\$500,000 \$5,346,000 \$122,000 \$2,063,000 \$172,000 \$0 \$0 \$0 \$0	\$500,000 \$80,000 \$0 \$538,000 \$45,000 \$316,000 \$302,000 \$737,000 \$577,000 \$30,000	\$500,000 \$80,000 \$0 \$538,000 \$45,000 \$395,000 \$378,000 \$25,000 \$721,000 \$30,000	\$500,000 \$80,000 \$538,000 \$45,000 \$248,000 \$378,000 \$778,000 \$725,000 \$717,000 \$721,000	\$500,000 \$80,000 \$0 \$538,000 \$45,000 \$248,000 \$378,000 \$721,000 \$721,000 \$130,000	\$500,000 \$80,000 \$0,538,000 \$45,000 \$395,000 \$378,000 \$725,000 \$721,000 \$721,000	\$400,000 \$80,000 \$0 \$538,000 \$45,000 \$243,000 \$377,000 \$906,000 \$707,000 \$230,000	\$200,000 \$80,000 \$0 \$448,000 \$37,000 \$174,000 \$264,000 \$647,000 \$505,000 \$120,000	\$100,000 \$80,000 \$0 \$359,000 \$39,000 \$142,000 \$136,000 \$333,000 \$258,000 \$260,000	\$0 \$40,000 \$0 \$149,000 \$12,000 \$40,000 \$63,000 \$60,000 \$116,000 \$115,000 \$50,000	3,200,000 680,000 0 4,184,000 349,000 1,737,000 2,765,000 2,644,000 6,473,000 5,021,000 5,021,000 900,000
Subtotal \$/Ton Ore		\$2,919,000	\$5,284,000	\$8,203,000	\$3,900,000 \$19.50	\$4,577,000 \$18.31	\$4,677,000 \$18.71	\$4,677,000 \$18.71	\$4,677,000 \$18.71	\$4,609,000 \$18.81	\$3,254,000 \$18.59	\$1,837,000 \$20.41	\$793,000 \$19.83	\$33,001,000 \$18.86
TOTAL \$/TON ORE		\$5,007,000	\$8,637,000	\$13,644,000	\$7,651,000 \$38.26	\$8,424,000 \$33.70	\$8,522,000 \$34.09	\$8,519,000 \$34.08	\$8,519,000 \$34.08	\$8,443,000 \$34.46	\$6,540,000 \$37.37	\$3,998,000 \$44.42	\$1,794,000 \$44.85	\$62,410,000 \$35.66

CAPITAL COST BREAKDOWN

NO.	ITEM	UNIT COST	TOTAL (\$000s)
6	2 Boom E/H jumbo	337,150	2,023
6	15 Ton diesel truck	146,240	877
6	3.5 cu. yd. Diesel LHD	173,000	1,038
10	Stopes (air)	3,180	32
10	Jackleg (air)	3,180	32
1	Portable refuge station	10,000	10
3	Service vehicles elec/mech/lube	71,000	213
1	Anfo Truck	100,008	100
6	Anfo Loaders	1,000	6
1	Grader w/Blade	7,500	75
1	1 Personnel Carrier	21,000	21
2	Personnel Vehicles	20,000	40
1	Diamond drill & rods	70,000	70
1	Fuel tanker	86,000	86
6	Scissor truck	297,500	1,785
6	Pumps 58 HP	15,699	94
12	Pumps 13 HP	4,372	52
1	Traffic signals/communication		100
	U.G Electrician		309 🖋
2	Service Shop - outfit ?? tools	72,056 40,000	112
2	Outfit Refuge Station	28,000	56
1 lot	Misc. Tools	200,000	200
2	Main pumps & install.		500
12	Auxiliary fans	5000	60
4	Mine Johns	3000	12
1	2 Motor Alimak raise climber and rail	149	149
2	Surface Fans W/ cooling system	175	350
2	Surface trucks	130	260

1	Surface loader/forklit	ft	129	129
2	Compressor		80	160
TOTAL				8,951
		SURFACE II	NFRASTRUCTURE	
1	Backfill plant & bore	holes		415
1	Portal (set-up, excav	ate and const	t. dump)	640
	Electrical - Generato	r/Powerline		594
	Surface Shop	Dry Office Safety Sup		000
TOTAL				2,059



OP710M/

CASHO1A.WK1 BASE 3

CASE: Tax Free

Haulage Decline - Cut-off = 0.10 oz/ton (Au) @ 1000 tpd & 5 days/week

NPV Cash Surplus IRR % \$770,406

		R	ESERVES SUMMA	ARY							METAL PRICES	
Category		In Situ	Available	Grade	Diluted	Diluted	Recovery	Troy		old	360 U	
		tons	tons	Au oz/t	tons	Au oz/t	%	ounces	S	Silver	4.00 U	S\$/oz
Indicated							0.91					
Inferred							0.91				RECOVERY (Au)	0.906
Total		0	0		0	0.22	0.91	0			(Ag)	0.620
Total		Ü	v		•	0.22		-			, 0,	
PRODUCTION	Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Totals
Tons	Tour o	rour r	200,000	250,000	250,000	250,000	250,000	205,000	125,000	73,000		1,603,000
Au oz/t			0.26	0.26	0.23	0.23	0.22	0.20	0.19	0.18		0.22
Gold oz (mined)			51,368	63,757	58,329	56,520	53,915	41,602	23,226	13,378	0	362,095
Silver oz (mined)			482,079	602,502	601,340	600,952	701,048	664,313	471,947	285,527	0	4,409,708
Sliver oz (mined)			402,078	002,302	001,040	000,002	,	55,,515				
Gold oz (poured)			46539.408	57763.842	52846.074	51207.120	48846.990	37691.412	21042.756	12120.468	0.000	
Silver oz (poured)			298888.980	373551.240	372830.800	372590.240	434649.760	411874.060	292607.140	177026.740	0.000	
Sliver oz (podred)			200000.000	0,000,12,10	0.200.000	• • • • • • • • • • • • • • • • • • • •	100000000000000000000000000000000000000					
REVENUES												
Gold			16,754,187	20,794,983	19,024,587	18,434,563	17,584,916	13,568,908	7,575,392	4,363,368	0	118,100,905
Silver			1,195,556	1,494,205	1,491,323	1,490,361	1,738,599	1,647,496	1,170,429	708,107	0	10,936,076
Gross			17,949,743	22,289,188	20,515,910	19,924,924	19,323,515	15,216,405	8,745,821	5,071,475	0	129,036,981
31000												
OPERATING COST												
Mining (\$/ton)			35.20	35.20	35.20	35.20	35.20	35.20	35.20	35,20	35.20	
Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	
Tailings (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	
Total (\$)			10,180,000	12,725,000	12,725,000	12,725,000	12,725,000	10,434,500	6,362,500	3,715,700	0	81,592,700
10101 (0)			,,				100-00 TO 100-00-00 COOK-0-000	ALLON COOKS AS MANAGED				
CAPITAL COSTS												
Development	2,286,000	2,074,800	723,900	723,900	571,500	571,500	571,500	381,000	203,200	63,500		8,170,800
Mining Equipment	70,000	2,011,000	7,148,000	. 20,000			100.0 W. 100.000	0.00 O.0000000				7,218,000
Plant	70,000	9,500,000	1,140,000									9,500,000
Tailings Dam		500,000	2,000,000									2,500,000
Infrastructure		2,000,000	958,000									2,958,000
Diamond Drilling	500,000	500000.000	330,000	is .								1,000,000
Environmental & Permitti		250000.000										500,000
Closure	ig 250,000	230000.000								250,000	250,000	500,000
EPCM		2,300,000	800,000							200,000		3,100,000
Total	3,106,000	17,124,800	11,629,900	723,900	571,500	571,500	571,500	381,000	203,200	313,500	250,000	35,446,800
Total	3,100,000	17,124,000	11,020,000	120,000	37 1,000	3, 1,000	3, ,,550	55.,500	211,200	-,-,		10000 to 1000 to 100 To To
TOTAL CASH COST	3,106,000	17,124,800	21,809,900	13,448,900	13,296,500	13,296,500	13,296,500	10,815,500	6,565,700	4,029,200	250,000	117,039,500
CASH SURPLUS	(3,106,000)	(17,124,800)	(3,860,157)	8,840,288	7,219,410	6,628,424	6,027,015	4,400,905	2,180,121	1,042,275	(250,000)	11,997,481
ONG! I BUNFLUG	(0,100,000)	(17,124,000)	•	0,040,200	1,210,410	0,020,724	5,52.,510	.,,	-11	.,	,	e reconnect while
			N.									

CASHO1B.WK1 BASE 4

CASE: Tax Free Hautage Decline - Cut-off = 0.10 oz/ton (Au) @ 1000 tpd & 7 days/week

NPV Cash Surplus IRR % 2,777,418 15

												METAL PRICES		
				SERVES SUMMA		Mark and	0400000000			Go		380 U	25/07	
	Category		in Situ	Available	Grade	Diluted	Diluted	Recovery	Troy		ver	4.00 U		
			tons	tons	Au oz/t	tons	Au oz/t	%	ounces	50	VUI	4.00 0.	3402	
	Indicated							0.85				RECOVERY (Au)	0.91	0.91
	Interned							0.85					0.62	0.62
	Total		0	0		0	0.22	0.82	0			(Aq)	402	ubz
	1010													
												400	_	
PRODUCTION		Year O	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Totals	
PHOCOCINCIA	Tons			280,000	350,000	350,000	335,000	257,500	34,500				1,803,000	
	Au ozr			0.26	0.26	0.22	0.20	0.50	0.21				0.23	
	Gold oz (mined)			71,915	89,260	77,877	66,051	49,692	7,300				362,095	
	Silver oz (mined)			674,911	843,503	927,339	1,082,024	819,108	82,824				4,409,707	
	SIVER OZ (MICHEO)			514,511	0.4,000									
	0-14-1-1-1-1			651 55	80870	70557	59842	45021	681 4	0	0	0		
	Gold az (poured)			418445	522972	574950	658455	507848	51 351	0	0	0		
	Silver oz (poured)			410440	CEACH E	0000		25.05						
REVENUES	Dr			23,455,798	29,113,042	25,400,362	21,543,194	16,207,543	2,390,999	0	0	0	118,100,905	
	Gold			1.673.779	2,091,887	2,299,801	2,633,820	2,031,383	205,404	0	0	0	10,930,073	
10000	Silver			25.129.576	31,204,929	27,700,163	24,177,014	18,238,926	2,586,372	0	0	0	129,036,979	
Gros	•			23,124,575	31,204,029	21,100,100	24,177,014	14204520	4					
OPERATING CO				35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20		
	Mining (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50		
	Milling (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40		
	Talings (S/ton)			1,80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80		
	Admin (\$/ton)				17,815,000	17,815,000	17,051,500	12,903,150	1,750,050	0	0	0	81,592,700	
Tot	m (2)			14,252,000	17,812,000	17,812,000	17,001,000	12,000,100	1,104,000	•				
	_													
CAPITAL COST	The same of the control of the contr			000 000	863,600	812,800	812,800	381,000	76,200				8,170,800	
	Development	2298000	2,074,800	863,600	807,000	812,000	012000	001,000	, 4,200				7,218,000	
	Mining Equipment	70,000		71 48000									9,500,000	
	Plant		9,500,000										2.500,000	
	Tailings Dam		500,000	2,000,000									2,958,000	
	Infrastructure		2000000	958000									1,000,000	
	Diamond Drilling	500000	500000										500,000	
	Environmental & Permitting	250,000	250,000						250000	250000			500,000	
	Clasure								<u>ڪ</u> ست	2000			3100,000	
	EPCM		2,300,000	800,000						000.000			35,446,800	
Tot		3,105,000	17,124,800	11,769,600	883,600	812,800	812,800	381,000	326,200	250,000		, ,	3474300	
100								46		000.00		. 0	117,039,500	
TOTAL CASH	COST	3,108,000	17,124,800	26,021,600	18,678,600	18,627,800	17,864,300	13,284,150	2,082,250	250,000	(11,997,479	
CASH SURPLL		(3,108,000)	(17,124,800)	(892,024)	12,526,329	9,072,363	6,312,714	4,954,776	504,122	(250,000)			11,991,479	

M770M 3

CASHO15.WK1 BASE 1

CASE: Tax Free

Diamond Drilling

Closure

EPCM

Total

TOTAL CASH COST

CASH SURPLUS

Encironmental & Permitting

500000.000

250000.000

3,106,000

3,106,000

(3,106,000)

500000.000

250000.000

2,300,000

17,124,800

17,124,800

(17, 124, 800)

800,000

660,400

10,204,150

7,588,133

558,800

10,102,550

7,689,733

558,800

10,102,550

7,199,262

11,566,400

17,928,900

(5,903,995)

Haulage Decline - Cut-off = 0.15 oz/ton (Au) @ 750 tpd & 5 days/week

NPV Cash Surplus IRR %

\$697,744 11%

381,000

8,652,250

4,274,516

558,800

10,102,550

5,883,064

500,000

500,000

(35,446,800)

3,100,000

103,148,890

14,092,359

250000.000

250,000

1,471,600

554,544

250000.000

377,000

5,777,490

2,687,185

304,800

8,576,050

4,350,716

METAL PRICES RESERVES SUMMARY Recovery Gold 360 US\$/oz Category Diluted Troy In Situ Available Grade Diluted Silver 4.00 US\$/oz % ounces tons tons Au oz/t tons Au oz/t 0.92 Indicated RECOVERY (Au) 0.906 0.92 Inferred (Ag) 0.620 0 0.22 0.92 0 0 0 Total Year 10 Totals Year 8 Year 9 Year 6 Year 7 Year 2 Year 3 Year 4 Year 5 PRODUCTION Year 0 Year 1 106,100 24,000 1,330,100 162,500 162,500 187,500 Tons 125,000 187,500 187,500 187,500 0.22 0.24 0.25 0.24 0.22 0.22 0.27 0.27 0.27 0.26 Au oz/t 23.175 5,736 329,174 44,464 35,328 35,328 Gold oz (mined) 34,338 50,764 50,764 49,277 598,079 566,204 566,204 365,289 62,617 3,983,007 495,817 Silver oz (mined) 332,751 498,023 498,023 298,232 40284.384 32007.168 32007.168 20996.550 5196.816 45992.184 44644.962 31110.228 45992.184 Gold oz (poured) 308774.260 307406.540 370808.980 351046.480 351046.480 226479.180 38822.540 2,469,464 Silver oz (poured) 0.000 206305.620 308774.260 REVENUES 14,502,378 11,522,580 11.522.580 7.558,758 1,870,854 107,363,392 16,557,186 16,557,186 16,072,186 Gold 11,199,682 905,917 155,290 9,877,857 1,229,626 1,483,236 1,404,186 1,404,186 1,235,097 Silver 825,222 1,235,097 2,026,144 15,985,614 12,926,766 12,926,766 8,464,675 117,241,249 17,792,283 17,792,283 17,301,812 12,024,905 Gross OPERATING COST 35.20 35.20 35.20 35.20 35.20 35.20 35.20 35.20 Mining (\$/ton) 35.20 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 Milling (\$/ton) 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 Tailings (\$/ton) 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 Admin (\$/ton) 9.543.750 8,271,250 8,271,250 5,400,490 1,221,600 6,362,500 9,543,750 9,543,750 9,543,750 Total (\$) CAPITAL COSTS 127,000 8,170,800 2286000.000 2,074,800 660,400 660,400 558,800 558,800 558,800 381,000 304,800 Development 7,218,000 Mining Equipment 70.000 7,148,000 9,500,000 9,500,000 Plant 2,500,000 500,000 2,000,000 Tailings Dam 2,958,000 2.000.000 958.000 Infrastructure 1,000,000

CASHO15B.WK1 BASE 2

CASE: Tax Free NPV Cash Surplus \$2,831,147
Haulage Decline - Cut-off = 0.15 oz/ton (Au) @ 750 tpd & 7 days/week IRR % 14

METAL PRICES RESERVES SUMMARY 360 US\$/oz Gold Diluted Recovery Troy Diluted Available Grade In Situ Category 4.00 US\$/oz Silver % ounces Au oz/t Au oz/t tons tons tons 0.92 Indicated 0.92 Inferred RECOVERY (Aq) 0.906 0 0.92 0 0.22 0 0 Total 0.620 (Au) Totals Year 10 Year 8 Year 9 Year 5 Year 6 Year 7 Year 3 Year 4 Year 1 Year 2 Year 0 PRODUCTION 1,330,100 24,000 262,500 229,600 114,000 175,000 262,500 262,500 Tons 0.25 0.22 0.23 0.24 0.26 0.23 0.27 0.27 Au oz/t 329,199 0 0 5,763 49,462 26,265 69,285 59,282 48.073 71,069 Gold oz (mined) 0 3,983,010 0 818,362 337.257 62,617 907,104 697,233 694,585 465,852 Silver oz (mined) 0 298,254 5.221 0 23,796 53,709 44,813 43,554 64,389 62,772 Gold oz (poured) 0 2,469,466 38,823 0 209,099 507,384 288,828 432,284 430,643 562,404 Silver oz (poured) REVENUES 107,371,546 1,879,660 0 0 8,566,592 16,132,526 22,597,996 19,335,417 15,679,490 23,179,865 Gold 0 9,877,865 155,290 Ω 836,397 2.029,538 1,729,138 1,722,571 2,249,618 1,155,313 Silver 0 117,249,411 2,034,950 0 9,402,990 21,585,035 18,162,064 24,909,003 24,320,566 16,834,803 Gross OPERATING COST 35.20 35.20 35.20 35.20 35.20 35.20 35.20 35.20 35.20 Mining (\$/ton) 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 13.50 Milling (\$/ton) 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 Tailings (\$/ton) 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 Admin (\$/ton) 67,702,090 0 1,221,600 11,686,640 5,802,600 13,361,250 13,361,250 8,907,500 13,361,250 Total (\$) CAPITAL COSTS 8,170,800 508,000 152,000 711,200 711,200 863,800 863,800 2.286,000 2,074,800 Development 7,218,000 7,148,000 70,000 Mining Equipment 9,500,000 9,500,000 Plant 2,500,000 500,000 2,000,000 Tallings Dam 2,958,000 2,000,000 958,000 Infrastructure 1,000,000 500,000 Diamond Drilling 500,000 500,000 250,000 250,000 Environmental & Permitting 500,000 250,000 250,000 Closure 3,100,000 800,000 2,300,000 **EPCM** 0 35,446,800 0 402,000 250,000 711,200 508,000 863,800 711,200 11,769,800 17,124,800 3,106,000 Total 103,148,890 12,194,640 6,204,600 1,471,600 0 14,072,450 20,677,300 14,225,050 14,072,450 17,124,800 3,106,000 TOTAL CASH COST 14,100,521 0 3,198,390 563,350 7,512,585 5,967,424 (3,842,497)10,683,953 10,248,116 (3,106,000)(17,124,800)CASH SURPLUS

cash015-1	A MOD 1													
CASE:	Tax Free Haulage Decline - Cut-off = 0.15 o. reduced capital	z/10.1 (Au) @ 750 tp	d & 5 days/week				V Cash Surplus R %		\$2,613,597 13%					
	ope same										м	ETAL PRICES		
				SERVES SUMMAR			. 01	Deaming	Troy	G	old	380 US	S/oz	
	Category		in Situ	Available	Grade	Diluted	Diuted	Recovery	ounces		lver .	4.00 US		
			tons	tons	Au oz/t	tons	Au oz/t	0.92	COLICUS	5,				
	Indicated							0.92			RE	ECOVERY (Au)	0.908	
	Interred			_		0	0.22	0.82	0			(Aq)	0.620	
	Total		0	0		0	u22	0.82	Ü					
						egyene e		V	Year 7	Year B	Year 9	Year 10	Totals	
PRODUCTION		Year O	Year 1	Year 2	Year 3	Year 4	Year 5	Year 5 187,500	162,500	162,500	105,100	24,000	1,330,100	
	Tons			125,000	187,500	187,500	187,500		0.22	0.22	0.22	0.24	0.25	
	Au ozn			0.27	0.27	0.27	0.26	0.24 44,484	35,328	35,328	23,175	5,736	329,174	
	Gold oz (mined)			34,338	50,764	50,764	49,277	598,079	586,204	565,204	365,289	- 62,617	3.983.007	2,995
	Silver oz (mined)			332,751	498,023	498,023	495,817	560,079	554204	300,204	Control			
						45992.184	44644,962	40284,384	32007.168	32007.168	20998,550	5196.816	298,232	
	Gold oz (poured)		2222	31110.228	45992.184	308774.260	307408.540	370808.980	351 046, 480	351048.480	226479.180	38822.540	2,469,464	
	Silver az (poured)		0.000	208305.620	308774,260	308/74.200	307402540	370000	001010100	55.5.5				
0055														
REVENUES	Gold			11,199,682	16,557,186	16,557,186	16,072,188	14,502,378	11,522,580	11,522,580	7,558,758	1,870,854	107,363,392	
	Silver			825,222	1,235,097	1,235,097	1,229,626	1,483,236	1,404,186	1,404,185	905,917	155,290	9,877,857	9,877,857
Gros				12,024,905	17,792,283	17,792,283	17,301,812	15,985,614	12,926,766	12,926,766	8,484,675	2,026,144	117,241,249	
Gros	•			1402 1100										
OPERATING CO	OST								25.00	35.20	35.20	35.20		
	Mining (\$/ton)			35.20	35.20	35.20	35.50	35.20	35.20 13.50	13.50	13.50	13.50		
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	0.40	0.40	0.40	0.40		
	Talings (\$/ton)			0.40	0.40	0.40	0.40	0.40 1.80	1.80	1.80	1.80	1.80		
	Admin (\$/ton)			1.80	1.80	1.80	1.80	9,543,750	8,271,250	8.271,250	5,400,490	1,221,600	67,702,090	
Tot	B (S)			6,362,500	9,543,750	9,543,750	8,543,750	8,5-4,750	4271,250	42.11220	4.54			
CAPITAL COST	'S												8,170,800	
0111112000	Development	2295000,000	2,074,800	680,400	690,400	558,800	558,800	558,800	381,000	304,800	127,000		6,218,000	
	Mining Equipment	70,000		6,148,000									8,000,000	
	Piant		8,000,000										1,500,000	
	Tallings Dam		500,000	1,000,000									2,958,000	
	Infrastructure		2,000,000	958,000									1,000,000	
	Diamond Drilling	500000.000	500000.000										500,000	
	Environmental & Permitting	250000.000	250000,000								250000,000	250000,000	500,000	
	Clasure										2000	2000	3,100,000	
	EPCM		2,300,000	800,000								~~~	32,946,800	
Tat	and the state of t	3,105,000	16,624,800	9,500,400	660,400	558,800	558,800	558,800	381,000	304,800	377,000	250,000	مدمسم	
						101mers	10,102,550	10,102,550	8.652,250	8,576,050	5,777,490	1,471,600	100,648,890	
TOTAL CASH		3,108,000	16,624,800	15,928,900	10,204,150	10,102,550		5.883.084	4,274,516	4,350,716	2,887,185	554,544	16,592,359	
CASH SURPLL	JS	(2105,000)	(16,624,800)	(3,903,595)	7,588,133	7,689,733	7,199,262	0,663,064	7,2/4,510	4,000,710	2,301,100	30,,0		

cash015-1	A MOD 2						560			i.	\bigcirc	PTI	DN	6
CASE:	Tax Free Haulage Decline - Cut-off = 0.15 oz reduced capital	/ton (Au) @ 750 tp	od & 5 days/week				V Cash Surplus R %		(\$1,125,005) 8%					
	increase op		В	ESERVES SUMMA	RY							ETAL PRICES		
	Category		in Situ	Available	Grade	Diluted	Diluted	Recovery	Troy		old	390 US		
			tons	tons	Au oz/t	tons	Au oz/t	% 0.00	ounces	5	Mar	4.00 0	25/07	
	indicated Inferred Total		0	0		0	0.22	085 085 085	0		R	(Ag)	0.620	
PRODUCTION		Year O	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Your 8	Year 9	Year 10 24,000	Totals 1,330,100	
111000011011	Tons			125,000	187,500	187,500	187,500	187,500	162,500	162,500	105,100	0.24	0.25	
	Au oz/t			0.27	0.27	0.27 50.764	0.26 49,277	0.24	35,328	35,328	23,175	5,736	329,174	
	Gold oz (mined)			34,338 332,751	50,764 498,023	498,023	495,817	598,079	566,204	588,204	365, 289	62,617	3,983,007	2,995
	Silver az (mined)			332,751	400,020	490,025	104011	0040.0						
	Gold az (paured)			31110.228	45992.184	45992.184	44844.982	40284.384	32007.168	32007.168	20996.550	5198.816	298,232	
	Silver oz (poured)		0.000	208305.620	308774.280	308774.280	307408.540	370808.980	351046.480	351 046, 480	226479.180	38822.540	2,489,484	
REVENUES				11,199,682	16,557,186	16,557,186	16,072,186	14,502,378	11,522,580	11,522,580	7,558,758	1,870,854	107,363,392	
	Gold			825,222	1,235,097	1,235,097	1,229,626	1,483,236	1,404,188	1,404,188	905,917	155,290	9,877,857	9,877,857
Grasi	Silver			12,024,905	17,792,283	17,792,283	17,301,812	15,995,614	12,926,765	12,926,766	8,464,675	2,026,144	117,241,249	
0.00														
OPERATING CO	ST					~~~	35.20	35.20	35.20	35.20	35.20	35.20		
	Mining (\$/ton)			35.20 13.50	35.20 13.50	35.20 13.50	13.50	13.50	13.50	13.50	13.50	13.50		
	Milling (S/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40		
	Tailings (\$/ton) Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	m	
Tota	(S)			6,998,750	10,498,125	10,498,125	10,498,125	10,498,125	9,098,375	9,098,375	5,940,539	1,343,780	74,472,299	
CAPITAL COST			0.074.000	680,400	680,400	558,900	558,800	558,800	381,000	304,800	127,000		8,170,800	
	Development	2298000.000 70.000	2,074,800	6148,000	224	33,000	000,000						6,218,000	
	Mining Equipment Plant	74400	9,000,000	4144000									8,000,000	
	Talings Dam		500,000	1,000,000									1,500,000	
	Mrastructure		2000,000	958,000									1,000,000	
	Diamond Drilling	500000.000	. 500000.000										500,000	
	Environmental & Permitting	250000.000	250000.000								250000.000	250000.000	500,000	
	Closure		2300,000	800,000									3,100,000	
Tot	EPCM	3,105,000	16,624,800	9,566,400	660,400	558,800	558,800	558,800	381,000	304,800	377,000	250,000	32,945,800	
100	CP C	4,0400												

11,056,925

6,244,887

11,056,925

4,928,699

107,419,000

9,822,150

6,317,539

2,147,138

1,583,760

432,384

9,479,375

3,447,391

8,403,175

3,523,591

3108000

(2102000)

TOTAL CASH COST CASH SURPLUS

16,624,800

(16,624,800)

16,585,150

11,158,525

6,633,758

11,056,925

CASHO15B.WK1	B MOD 1												
CASE:	Tax Free Haulage Decline - Cut-off = 0.15 oz	v/ton (Áu) @ 750 tp	od & 7 days/week				PV Cash Surplus RR %		\$4,333,777 17				
	red cap		-	ESERVES SUMMA	DV							METAL PRICES	
	ope same		In Situ	Available	Grade	Diluted	Diluted	Recovery	Troy	G	old	360 L	S\$/oz
	Category		tons	tons	Au oz/t	tons	Au oz/t	%	ounces	SI	lver	4.00 L	S\$/oz
	Indicated		toris	tons	7,0 021			0.92					
	Inferred							0.92					
	Total		0	0		0	0.22	0.92	0			RECOVERY (Ag)	0.906 0.620
												(Au)	0.620
				v0.140.00	V0	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Totals
PRODUCTION	_	Year 0	Year 1	Year 2 175,000	Year 3 262,500	262,500	262,500	229,600	114,000	24,000	1.550		1,330,100
	Tons			0.27	0.27	0.26	0.23	0.22	0.23	0.24			0.25
	Au oz/t			48,073	71,069	69,285	59,282	49,462	26,265	5,763	0	0	329,199
	Gold oz (mined)			465,852	697,233	694,585	907,104	818,362	337,257	62,617	0	0	3,983,010
	Silver oz (mined)			400,002	001,200	00.1000	2-11-12-11	2000 mar - 1000					
	Gold oz (poured)			43,554	64,389	62,772	53,709	44,813	23,796	5,221	0	0	298,254
	Silver oz (poured)			288,828	432,284	430,643	562,404	507,384	209,099	38,823	0	0	2,469,466
	u ,												
REVENUES									0.500.500	1,879,660	0	0	107,371,546
	Gold			15,679,490	23,179,865	22,597,996	19,335,417	16,132,526	8,566,592 836,397	1,879,860	0	0	9,877,865
	Silver			1,155,313	1,729,138	1,722,571	2,249,618	2,029,538 18,162,064	9,402,990	2,034,950	0	o	117,249,411
Gros	s			16,834,803	24,909,003	24,320,566	21,585,035	18,102,004	9,402,990	2,004,500	•		
OPERATING CO	OCT.												
OPERATING CC	Mining (\$/ton)			35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	
	Tailings (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
	Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1,80	67,702,090
Tota	al (\$)			8,907,500	13,361,250	13,361,250	13,361,250	11,686,640	5,802,600	1,221,600	U	O	67,702,090
CAPITAL COST		0.000.000	2,074,800	863,800	863,800	711,200	711,200	508,000	152,000				8,170,800
	Development	2,288,000 70,000	2,074,800	6,148,000	,	711,200	7.1.1200	********	00000 100 Feet				6,218,000
	Mining Equipment	70,000	9,500,000	0,140,000									9,500,000
	Plant Tailings Dam		500,000	1,000,000									1,500,000
	Infrastructure		2,000,000	958,000									2,958,000
	Diamond Drilling	500,000	500,000										1,000,000
	Environmental & Permitting	250,000	250,000										500,000
	Closure		semetares.€no Ect?						250,000	250,000			500,000
	EPCM		2,300,000	800,000								.2.	3,100,000
Tot		3,106,000	17,124,800	9,769,800	863,800	711,200	711,200	508,000	402,000	250,000	0	0	33,446,800
, , ,				N.,		2 2 42240 2 224	Windstein Vern		0.004.005	4 474 000	0	0	101,148,890
TOTAL CASH C	COST	3,106,000	17,124,800	18,677,300	14,225,050	14,072,450	14,072,450	12,194,640	6,204,600	1,471,600 563,350	0	0	16,100,521
CASH SURPLU	S	(3,106,000)	(17,124,800)	(1,842,497)	10,683,953	10,248,116	7,512,585	5,967,424	3,198,390	563,550	Ü	0	10,100,021

CASHO15B.WK	B MOD 2			*									
CASE:	Tax Free Haulage Decline - Cut-off = 0.15 or	z/ton (Au) @ 750 tp	od & 7 days/week				PV Cash Surplus RR %		\$245,903 10				
	red cap		0.0	ESERVES SUMMAI	RY							METAL PRICES	
	increase op 10%		In Situ	Available	Grade	Diluted	Diluted	Recovery	Troy	Go	old	360 L	
	Category		tons	tons	Au oz/t	tons	Au oz/t	%	ounces	Si	lver	4.00 L	JS\$/oz
	Indicated							0.92 0.92	Λ.				
	Inferred		_			0	0.22	0.92	0			RECOVERY (Ag)	0.906
	Total		0	0		Ü	0.22	0.02				(Au)	0.620
PRODUCTION		Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Totals
PRODUCTION	Tons		. • • • • • • • • • • • • • • • • • • •	175,000	262,500	262,500	262,500	229,600	114,000	24,000			1,330,100 0.25
	Au oz/t	•		0.27	0.27	0.26	0.23	0.22	0.23	0.24	_	0	329,199
	Gold oz (mined)			48,073	71,069	69,285	59,282	49,462	26,265	5,763	0	0	3,983,010
	Silver oz (mined)			465,852	697,233	694,585	907,104	818,362	337,257	62,617	0	0	3,983,010
				43,554	64,389	62,772	53,709	44,813	23,796	5,221	0	0	298,254
	Gold oz (poured)			288,828	432,284	430,643	562,404	507,384	209,099	38,823	0	0	2,469,466
	Silver oz (poured)			200,020	102,20		2000 S 400 S	5 p *					
REVENUES						00 507 000	19,335,417	16,132,526	8,566,592	1,879,660	0	0	107,371,546
	Gold			15,679,490	23,179,865	22,597,996 1,722,571	2,249,618	2,029,538	836,397	155,290	o	0	9,877,865
	Silver			1,155,313	1,729,138		21,585,035	18,162,064	9,402,990	2,034,950	0	0	117,249,411
Gros	s			16,834,803	24,909,003	24,320,566	21,565,035	18,102,004	0,402,000	2,004,000			
OPERATING CO	OST										05.00	35.20	
Of Elevinion	Mining (\$/ton)			35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20 13.50	13.50	
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50 0.40	0.40	0.40	
	Tailings (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40 1.80	1.80	1.80	1.80	
	Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	6.382.860	1,343,760	1.50	0	74,472,299
Tot	al (\$)			9,798,250	14,697,375	14,697,375	14,697,375	12,855,304	6,382,860	1,343,760	Ü	·	,,
CAPITAL COST	S							500.000	152,000				8,170,800
	Development	2,286,000	2,074,800	863,800	863,800	711,200	711,200	508,000	152,000				6,218,000
	Mining Equipment	70,000		6,148,000	la .							i i	9,500,000
	Plant		9,500,000	N 12107A WARRES									1,500,000
	Tailings Dam		500,000	1,000,000									2,958,000
	Infrastructure		2,000,000	958,000									1,000,000
	Diamond Drilling	500,000	500,000										500,000
	Environmental & Permitting	250,000	250,000						250,000	250,000			500,000
	Closure						/		200,000				3,100,000
	EPCM		2,300,000	800,000	963 900	711,200	711,200	508,000	402,000	250,000	0	0	33,448,800
Tot	al	3,106,000	17,124,800	9,769,800	863,800	711,200	711,200	333,300					
	2007	3,106,000	17,124,800	19,568,050	15,561,175	15,408,575	15,408,575	13,363,304	6,784,860	1,593,760	0	0	107,919,099
TOTAL CASH ((3,106,000)	(17,124,800)	(2,733,247)	9,347,828	8,911,991	6,176,460	4,798,760	2,618,130	441,190	0	0	9,330,312
CASH SURPLU	15	(3,100,000)	(17,124,000)	(2,100,241)	-1 -20		24 222 24						

EPCM

*p+2Y

Total

TOTAL CASH COST

CASH SUPPLUS

300 751

250,000

1.471.600

741,629

32,948,800

100 848 890

27,328,698

C85h015-1 A MOD 18 \$8,648,631 21% NPV Cash Surplus CASE: Haulage Decline - Cut-off = 0.15 oz/ton (Au) @ 750 tpd & 5 days/week reduced capital ope same gold +10% METAL PRICES 396 US\$/oz Troy Gold Grade Diluted Darted Category 4.00 US\$/0Z ounces Au oz/t tons Au oz/t 0.85 RECOVERY (Au) 0.906 referred 0.620 (Aq) 0.82 0.22 OTotal 0 Year 9 Year 10 Totals Year 4 187,500 Year 6 Year 7 Year 1 Year 3 Year 5 Year O PRODUCTION 162,500 24,000 1,330,100 187,500 187,500 162,500 105,100 187,500 125,000 0.24 0.25 0.22 0.27 0.26 0.24 0.22 0.22 0.27 Au ozn 0.27 35,328 23,175 5,738 329,174 35,328 49 277 44.484 34,338 50,764 50,764 Gold oz (mined) 2,995 3,983,007 62.617 495,817 508,079 586,204 568,204 305,289 498,023 498,023 Silver oz (mined) 32007.168 32007.168 20008.550 5198.816 208 232 31110.228 45992.184 45992.184 44844 090 40284,384 Gold oz (poured) 370808.980 351048.480 351046.480 226479.180 38822,540 2,469,464 307408.540 308774.260 0.000 208305.820 308774,260 Silver oz (poured) REVENUES 118,000,731 2.057.039 18,212,905 17,679,405 15,952,616 12,674,839 12,674,839 8.314.634 Gold 12319,650 18 212 905 9,877,857 9,877,857 155,290 1,229,626 1,483,236 1,404,188 1,404,186 905,917 1.235.097 1,235,097 825,222 13,144,873 14,079,024 2213220 127,977,588 17,435,852 19,448,002 19,448,002 18,909,001 G/Oss OPERATING COST 35.20 35.20 13.50 35.20 13.50 35.20 35.20 13.50 35.20 13.50 35.20 13.50 35.20 Mining (\$/ton) 13.50 13.50 13.50 Milling (\$/ton) 0.40 0.40 0.40 0.40 0.40 1.80 1.80 0.40 0.40 Talangs (S/ton) 1.80 1.80 1.80 1.80 Admin (\$100) 1,221,600 67,702,090 8.271,250 5,400,490 9,543,750 B,543,750 9,543,750 8,271,250 9.543,750 Total (S) 6.362.500 CAPITAL COSTS 8,170,800 127,000 304.800 680,400 558,800 551,800 558,800 381,000 2298000.000 2,074,800 690,400 Development 6,218,000 9,000,000 6,148,000 Mining Equipment 8000000 Plant 1,500,000 1.000.000 Tailings Dam 500.000 2,968,000 2000,000 958,000 intrastructure 500000.000 500000.000 Diamond Drilling 500,000 250000.000 250000,000 Environmental & Permitting 250000 500,000 3100,000

559 PCO

10.102.550

9.345,452

558,800

10.102.550

8,808,481

558,800

10.102.550

7,333,302

381,000

8,652,250

5,426,774

304,800

8,576,050

5,502,974

377.000

5,777,490

3,443,081

2300,000

16,624,800

16,624,800

(16,624,800)

3108,000

3108000

(2108,000)

800,000

890,400

10,204,150

9,243,852

9,585,400

(2,784,027)

(3

CASHO15B.WK1 B M	OD	1b
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OASI 10 100.111	B 1100 113												
CASE:	Tax Free Haulage Decline - Cut-of100 f = 0.	15 oz/ton (Au) @ 7	50 tpd & 7 days/wee	ek			PV Cash Surplus RR %		(\$2,229,262) 6				
	red cap												
	ope same gold - 10%		RES	SERVES SUMMA	RY							IETAL PRICES	
	Category		In Situ	Available	Grade	Diluted	Diluted	Recovery	Troy		old	324 U	
	outogo.)		tons	tons	Au oz/t	tons	Au oz/t	%	ounces	Si	ilver	4.00 U	S\$/oz
	Indicated		toris	torio	7.0 041	10.10		0.92					
								0.92					
	Inferred						0.00	0.92	0			ECOVERY (Ag)	0.906
	Total		0	0		0	0.22	0.92	U			(Au)	0.620
												(Au)	0.020
											V (400 0	Year 10	Totals
PRODUCTION		Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year (100 9	Year 10	
	Tons			175,000	262,500	262,500	262,500	229,600	114,000	24,000			1,330,100
	Au oz/t			0.27	0.27	0.26	0.23	0.22	0.23	0.24			0.25
	Gold oz (mined)			48,073	71,069	69,285	59,282	49,462	26,265	5,763		0	0 329,199
	Silver oz (mined)			465,852	697,233	694,585	907,104	818,362	337,257	62,617	0	0	3,983,010
	Silver 62 (mined)			400,002	007,200	55 1,555		- / - /					
	0.11			43,554	64,389	62,772	53,709	44,813	23,796	5,221	0	0	298,254
	Gold oz (poured)			1000 M	04,300	430,643	562,404	507,384	209,099	38,823	0	0	2,469,466
	Silver oz (poured)			288,828		450,045	302,404	307,304	200,000	00,020			E1 15.11 13.1
REVENUES											^	0	96,634,391
	Gold			14,111,541	20,861,879	20,338,196	17,401,875	14,519,273	7,709,933	1,691,694	0		
	Silver			1,155,313	1,729,138	1,722,571	2,249,618	2,029,538	836,397	155,290	0	0	9,877,865
Gros	\$			15,266,854	22,591,016	22,060,767	19,651,493	16,548,811	8,546,331	1,846,984	0	0	106,512,256
0.00	•												
OPERATING CO	OST												
OI LI WIII O	Mining (\$/ton)			35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	
				0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
	Tailings (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	
	*Ramin (\$/ton)							11,686,640	5,802,600	1,221,600	0	0	67,702,090
Tota	al (S)			8,907,500	13,361,250	13,361,250	13,361,250	11,000,040	5,802,800	1,221,000	•	·	0.1.001000
CAPITAL COST					222 222		711.000	500.000	450,000				8,170,800
	Development	2,286,000	2,074,800	863,800	863,800	711,200	711,200	508,000	152,000				6,218,000
	Mining Equipment	70,000		6,148,000	*								
	Plant		9,500,000										9,500,000
	Tailings Dam		500,000	1,000,000									1,500,000
	Infrastructure		2,000,000	958,000									2,958,000
	Diamond Drilling	500,000	500,000										1,000,000
	Environmental & Permitting	250,000	250,000										500,000
	Care to the property of the pr	250,000	200,000						250,000	250,000			500,000
	Closure								200,000	,-30			3,100,000
	EPCM		2,300,000	800,000		m.,	244.000	E00.000	400.000	250,000	0	0	33,446,800
Tota	al 2Y p 2Y	3,106,000	17,124,800	9,769,800	863,800	711,200	711,200	508,000	402,000	250,000	U	U	33,440,000
	p 2Y			4							•	0	101,148,890
TOTAL CASH C	COST	3,106,000	17,124,800640	18,677,300	14,225,050	14,072,450	14,072,450	/g _m_m	6,204,600		0		
CASH SURPLU	S	(3,106,000)	(17,124,800)	(3,410,446)	8,365,966	7,988,317	5,579,043	4,354,171	2,341,731	375,384	0	0	5,363,366

CASHO15B.WK1	B MOD 1a												
CASE:	Tax Free Haulage Decline - Cut-off = 0.15 oz	z/ton (Au) @ 750 tp	od & 7 days/week				NPV Cash Surplus IRR %	•	\$10,896,815 27				
	red cap			ESERVES SUMMAI	>							METAL PRICES	
	ope same gold +10%			Available	Grade	Diluted	Diluted	Recovery	Troy	Gold	1	396	US\$/oz
	Category		In Situ		Au oz/t	tons	Au oz/t	%	ounces	Silve	er	4.00	US\$/oz
			tons	tons	Au 02/1	toris	Au 021	0.92	Carro				
	Indicated							0.92					
	Inferred		0	0		0	0.22	0.92	0			RECOVERY (Ag)	0.906
	Total		· ·	U		v	0.22	3.2-				(Au)	0.620
PRODUCTION		Year 0	Year 1	Year 2	Year 3	Year 4	Y (100 ear 5	Year 6		Year 8Year 7	Year 9	Year 10	Totals
PHODOCTION	Tons	rour o	,	175,000	252,500	262,500	262,500	229,600	114,000	24,000			1,330,100
	Au oz/t			0.27	0.27	0.26	0.23	0.22	0.23	0.24			0.25
0	Gold oz (mined)			48.073	71,069	69,285	59,282	49,462	26,265	5,763		0	329,199
O	Silver oz (mined)			465,852	697,233	694,585	907,104	818,362	337,257	62,617	0	0	3,983,010
							F0 700	44,813	23,796	5,221	0	0	298,254
	Gold oz (poured)			43,554	(100 64,389		53,709	507,384	209,099	38,823	0	0	
	Silver oz (poured)			288,828	432,284	430,643	562,404	507,384	209,099	00,020	·		2,,
REVENUES				17,247,439	25,497,852	24,857,795	21,268,959	(100 17,745,779	9,423,252	2,067,626	0	0	118,108,700
	Gold			1,155,313	1,729,138	1,722,571	2,249,618	2,029,538	836,397	155,290	0	0	9,877,865
0	Silver			18,402,752	27,226,989	26,580,366	23,518,577	19,775,316	10,259,649	2,222,916	0	0	127,986,565
Gross	5			10,402,752	21,220,303	20,000,000	20,010,011	, 0, ,	,				
OPERATING CO	ost .												
0. 2.0110	*MRYng (\$/ton)			35.20	35.20	35.20	35.20	35.20		35.2035.20		35.20	
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	(100 13.50		13.50	
	Tailings (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
	Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	
Tota	u 1(\$21,600			8,907,500	13,361,250	13,361,250	13,361,250	11,686,640	5,802,600		0	0	67,702,090
CAPITAL COSTS		0.000.000	0.074.900	863,800	863,800	711,200	711,200	508,000	152,000				8,170,800
	Development	2,286,000	2,074,800	6,148,000	863,800	711,200	711,200	000,000	,04,000				6,218,000
	Mining Equipment	70,000	0.500.000	6,146,000	>								9,500,000
	Plant		9,500,000	1 000 000									1,500,000
	Tallings Dam		500,000 2,000,000	1,000,000 958,000									2,958,000
	Infrastructure	500,000	500,000	930,000									1,000,000
	Diamond Drilling	250,000	250,000										500,000
	Environmental & Permitting Closure	255,000	200,000						250,000	250,000			500,000
	EPCM		2,300,000	800,000									3,100,000
Tota	_ TI TI TI	3,106,000	17,124,800	9,769,800	863,800	711,200	711,200	508,000	402,000	250,000	0	C	
							44.000 (55	10 101 010	0.004.000	1,471,600	0	(101,148,890
TOTAL CASH C		3,106,000	17,124,800	18,677,300	14,225,050	14,072,450		12,194,640 7,580,676	6,204,600 4,055,049	751,316	0		
CASH SURPLU	S	(3,106,000)	(17,124,800)	(274,548)	13,001,939	12,507,916	9,446,127	7,500,676	4,000,048	751,510	O		23,00.,000

OP 710N B

CASHO1A.WK1 BASE 3+10%au

CASE:

Tax Free

Haulage Decline - Cut-off = 0.10 oz/ton (Au) @ 1000 tpd & 5 days/week

NPV Cash Surplus IRR %

\$7,696,240

	Category Indicated Inferred Total		In Situ tons	ESERVES SUMMA Available tons	RY Grade Au oz/t	Diluted tons	Diluted Au oz/t 0.22	Recovery % 0.91 0.91 0.91	Troy ounces 0		old ilver	METAL PRICES 360 U 4.00 U RECOVERY (Au) (Ag)	
PRODUCTION	Tons Au oz/t Gold oz (mined) Silver oz (mined) Gold oz (poured) Silver oz (poured)	Year 0	Year 1	Year 2 200,000 0.28 56,505 482,079 51193.349 298888.980	Year 3 250,000 0.28 70,133 602,502 63540.226 373551.240	Year 4 250,000 0.26 64,162 601,340 58130.681 372830.800	Year 5 250,000 0.25 62,172 600,952 56327.832 372590.240	Year 6 250,000 0.24 59,307 701,048 53731.689 434649.760	Year 7 205,000 0.22 45,762 664,313 41460.553 411874.060	Year 8 125,000 0.20 25,549 471,947 23147.032 292607.140	Year 9 73,000 0.20 14,716 285,527 13332.515 177026.740	Year 10 0 0 0.000 0.000	Totals 1,603,000 0,24 398,305 4,409,708
REVENUES Gross	Gold Silver s			18,429,606 1,195,556 19,625,161	22,874,481 1,494,205 24,368,686	20,927,045 1,491,323 22,418,369	20,278,020 1,490,361 21,768,380	19,343,408 1,738,599 21,082,007	14,925,799 1,647,496 16,573,295	8,332,931 1,170,429 9,503,360	4,799,705 708,107 5,507,812	0 0 0	129,910,996 10,936,076 140,847,072
OPERATING CO	Mining (\$/ton) Milling (\$/ton) Tailings (\$/ton) Admin (\$/ton)			35.20 13.50 0.40 1.80 10,180,000	35.20 13.50 0.40 1.80 12,725,000	35.20 13.50 0.40 1.80 12,725,000	35.20 13.50 0.40 1.80 12,725,000	35.20 13.50 0.40 1.80 12,725,000	35.20 13.50 0.40 1.80 10,434,500	35.20 13.50 0.40 1.80 6,362,500	35.20 13.50 0.40 1.80 3,715,700	35.20 13.50 0.40 1.80	81,592,700
CAPITAL COST	Development Mining Equipment Plant Taillings Dam Infrastructure Diamond Drilling Environmental & Permitting Closure EPCM	2,286,000 70,000 500,000 250,000 3,106,000	2,074,800 9,500,000 500,000 2,000,000 500000.000 250000.000 2,300,000 17,124,800	723,900 7,148,000 2,000,000 958,000 800,000 11,629,900	723,900 723,900	571,500 571,500	571,500 571,500	571,500 571,500	381,000	203,200	63,500 250,000 313,500	250,000	8,170,800 9,500,000 2,500,000 2,958,000 1,000,000 500,000 500,000 3,100,000 35,446,800
TOTAL CASH C CASH SURPLU		3,106,000 (3,106,000)	17,124,800 (17,124,800)	21,809,900 (2,184,739)	13,448,900 10,919,786	13,296,500 9,121,869	13,296,500 8,471,880	13,296,500 7,785,507	10,815,500 5,757,795	6,565,700 2,937,660	4,029,200 1,478,612		117,039,500 23,807,572

CASHO1A.WK1 BASE 3-10%au

CASE: Tax Free

Haulage Decline - Cut-off = 0.10 oz/ton (Au) @ 1000 tpd & 5 days/week

NPV Cash Surplus IRR % (\$6,155,427)

	Category Indicated Inferred		RE In Situ tons	ESERVES SUMMA Available tons	RY Grade Au oz/t	Diluted tons	Diluted Au oz/t	Recovery % 0.91 0.91	Troy ounces		Gold Silver	4.00 L	0.906
	Total		0	0		0	0.22	0.91	0			(Ag)	0.620
PRODUCTION	Tons Au oz/t Gold oz (mined) Silver oz (mined)	Year 0	Year 1	Year 2 200,000 0.23 46,231 482,079	Year 3 250,000 0.23 57,381 602,502	Year 4 250,000 0.21 52,496 601,340	Year 5 250,000 0.20 50,868 600,952	Year 6 250,000 0.19 48,524 701,048	Year 7 205,000 0.18 37,442 664,313	Year 8 125,000 0.17 20,903 471,947	Year 9 73,000 0.16 12,040 285,527	Year 10 0 0	Totals 1,603,000 0.20 325,886 4,409,708
	Gold oz (poured) Silver oz (poured)			41885.467 298888.980	51987.458 373551.240	47561.467 372830.800	46086.408 372590.240	43962.291 434649.760	33922.271 411874.060	18938.480 292607.140	10908.421 177026.740	0.000	
REVENUES	Gold Silver			15,078,768 1,195,556 16,274,324	18,715,485 1,494,205 20,209,690	17,122,128 1,491,323 18,613,451	16,591,107 1,490,361 18,081,468	15,826,425 1,738,599 17,565,024	12,212,017 1,647,496 13,859,514	6,817,853 1,170,429 7,988,282	3,927,032 708,107 4,635,139	0 0 0	106,290,815 10,936,076 117,226,891
OPERATING Co	OST Mining (\$/ton) Milling (\$/ton) Tailings (\$/ton) Admin (\$/ton) al (\$)			35.20 13.50 0.40 1.80 10,180,000	35.20 13.50 0.40 1.80 12,725,000	35.20 13.50 0.40 1.80 12,725,000	35.20 13.50 0.40 1.80 12,725,000	35.20 13.50 0.40 1.80 12,725,000	35.20 13.50 0.40 1.80 10,434,500	35.20 13.50 0.40 1.80 6,362,500	35.20 13.50 0.40 1.80 3,715,700	35.20 13.50 0.40 1.80	81,592,700
CAPITAL COST	Development Mining Equipment Plant Tailings Dam Infrastructure Diamond Drilling Environmental & Permitting Closure	2,286,000 70,000 500,000 250,000	2,074,800 9,500,000 500,000 2,000,000 500000.000 250000.000	723,900 7,148,000 2,000,000 958,000	723,900	571,500	571,500	571,500	381,000	203,200	63,500 250,000		8,170,800 7,218,000 9,500,000 2,500,000 2,958,000 1,000,000 500,000 5,0000 3,100,000
Tot	EPCM al	3,106,000	2,300,000 17,124,800	800,000 11,629,900	723,900	571,500	571,500	571,500	381,000	203,200	313,500	250,000	35,446,800
TOTAL CASH (CASH SURPLU		3,106,000	17,124,800 (17,124,800)	21,809,900 (5,535,576)	13,448,900 6,760,790	13,296,500 5,316,951	13,296,500 4,784,968	13,296,500 4,268,524	10,815,500 3,044,014	6,565,700 1,422,582	4,029,200 605,939		117,039,500 187,391

OPT10 N 15

CASHO1A.WK1 BASE 3+600,000t

CASE: Tax Free

Haulage Decline - Cut-off = 0.10 oz/ton (Au) @ 1000 tpd & 5 days/week

NPV Cash Surplus IRR %

\$6,729,871

			R	ESERVES SUMMA	RY						N	METAL PRICES	
	Category		In Situ	Available	Grade	Diluted	Diluted	Recovery	Troy	G	iold	360 U	
	Category		tons	tons	Au oz/t	tons	Au oz/t	%	ounces	S	ilver	4.00 U	S\$/oz
	Indicated		tono					0.91					
	Inferred							0.91			F	RECOVERY (Au)	0.906
	Total		0	0		0	0.22	0.91	0			(Ag)	0.620
	Total		Ü	ŭ		•							
							20 10				V0	Year 10	Totals
PRODUCTION		Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	250,000	2,200,000
	Tons			200,000	250,000	250,000	250,000	250,000	250,000	250,000	250,000	0.22	0.23
	Au oz/t			0.26	0.26	0.23	0.23	0.22	0.22	0.22	0.22		499,549
	Gold oz (mined)			51,368	63,757	58,329	56,520	53,915	53,915	53,915	53,915	53,915	
	Silver oz (mined)			482,079	602,502	601,340	600,952	701,048	664,313	471,947	285,527	322,625	4,732,333
	Cald an (nausad)			46539.408	57763.842	52846.074	51207.120	48846.990	48846.990	48846.990	48846.990	48846.990	
	Gold oz (poured)			298888.980	373551.240	372830.800	372590.240	434649.760	411874.060	292607.140	177026.740	200027.500	
	Silver oz (poured)			290000.900	070001.240	072000.000	0,5000,510	10 10 1011 00					
REVENUES				10.754.107	20,794,983	19,024,587	18,434,563	17,584,916	17,584,916	17,584,916	17,584,916	17,584,916	162,932,902
	Gold			16,754,187		1,491,323	1,490,361	1,738,599	1,647,496	1,170,429	708,107	800,110	11,736,186
7000	Silver			1,195,556	1,494,205			19,323,515	19,232,413	18,755,345	18,293,023	18,385,026	174,669,088
Gros	s			17,949,743	22,289,188	20,515,910	19,924,924	19,323,515	19,202,410	10,733,040	10,200,020	10,000,020	1. 1,000,000
OPERATING CO	OST												
	Mining (\$/ton)			35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	
	Tailings (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
	Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	
Tota	al (\$)			10,180,000	12,725,000	12,725,000	12,725,000	12,725,000	12,725,000	12,725,000	12,725,000	12,725,000	111,980,000
CAPITAL COST	·e												
CAFITAL COST	Development	2,286,000	2,074,800	723,900	723,900	571,500	571,500	571,500	381,000	203,200	63,500		8,170,800
	Mining Equipment	70,000	2,014,000	7,148,000	. 20,000	0,000		5500 W. 1000	San Carrier III II I				7,218,000
	Plant	70,000	9,500,000	7,140,000									9,500,000
			500,000	2,000,000									2,500,000
	Tailings Dam		2,000,000	958,000									2,958,000
	Infrastructure	E00.000		938,000	a .								1,000,000
	Diamond Drilling	500,000	500000.000										500,000
	Environmental & Permitting	250,000	250000.000								250,000	250,000	500,000
	Closure		0.000.000	200 000							200,000	200,000	3,100,000
7-1	EPCM	3,106,000	2,300,000 17,124,800	800,000 11,629,900	723,900	571,500	571,500	571,500	381,000	203,200	313,500	250,000	35,446,800
Tota	aı	3,100,000	17,124,000	11,029,900	123,300	371,500	37 1,000	37 1,000	55,,550	200,200			
													1 17 100 000
TOTAL CASH O	COST	3,106,000	17,124,800	21,809,900	13,448,900	13,296,500	13,296,500	13,296,500	13,106,000	12,928,200	13,038,500	12,975,000	147,426,800
CASH SURPLL	JS	(3,106,000)	(17,124,800)	(3,860,157)	8,840,288	7,219,410	6,628,424	6,027,015	6,126,413	5,827,145	5,254,523	5,410,026	27,242,288
				N.									

CASHO1A.WK1 BASE 3+1.1M t

CASE: Tax Free

Haulage Decline - Cut-off = 0.10 oz/ton (Au) @ 1000 tpd & 5 days/week

NPV Cash Surplus IRR %

\$9,996,554 17

			RE	ESERVES SUMMAR	RY							IETAL PRICES			
	Category		In Situ	Available	Grade	Diluted	Diluted	Recovery	Troy	G	old	360			S\$/oz
			tons	tons	Au oz/t	tons	Au oz/t	%	ounces	S	ilver	4.00		U	S\$/oz
	Indicated							0.91							
	Inferred							0.91			R	ECOVERY (Au)			0.906
	Total		0	0		0	0.22	0.91	0			(Ag)			0.620
	Total		•			-									
PRODUCTION		Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Year 11	Year 12	Totals
	Tons			200,000	250,000	250,000	250,000	250,000	250,000	250,000	250,000	250,000	250,000	250,000	2,700,000
	Au oz/t			0.26	0.26	0.23	0.23	0.22	0.22	0.22	0.22	0.22	0.22	0.22	0.23
	Gold oz (mined)			51,368	63,757	58,329	56,520	53,915	53,915	53,915	53,915	53,915	53,915	53,915	607,379
	Silver oz (mined)			482,079	602,502	601,340	600,952	701,048	664,313	471,947	285,527	322,625	322,625	322,625	5,377,583
					4.00.000		54007400	100 10 000	48846.990	48846.990	48846.990	48846.990	48846.990	48846.990	
	Gold oz (poured)			46539.408	57763.842	52846.074	51207.120	48846.990	411874.060	292607.140	177026.740	200027.500	200027.500	200027.500	
	Silver oz (poured)			298888.980	373551,240	372830.800	372590.240	434649.760	411874.000	292007.140	177020.740	200027.000	200027.000	200027.000	
REVENUES															
HEVENUES	Gold			16,754,187	20,794,983	19,024,587	18,434,563	17,584,916	17,584,916	17,584,916	17,584,916	17,584,916	17,584,916	17,584,916	198,102,735
	Silver			1,195,556	1,494,205	1,491,323	1,490,361	1,738,599	1,647,496	1,170,429	708,107	800,110	800,110	800,110	13,336,406
Gross				17,949,743	22,289,188	20,515,910	19,924,924	19,323,515	19,232,413	18,755,345	18,293,023	18,385,026	18,385,026	18,385,026	211,439,140
Gros.	•			17,0-10,7-10	22,200,100	20,010,010	10,021,021	,,		0.000 \$ 0.000 \$ 0.000 \$					
OPERATING CO	eT.														
OFERAING CO	Mining (\$/ton)			35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35,20	35,20	35.20	
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	
	Tailings (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
	Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1,80	1.80	1.80	
Tota	± (\$)			10,180,000	12,725,000	12,725,000	12,725,000	12,725,000	12,725,000	12,725,000	12,725,000	12,725,000	12,725,000	12,725,000	137,430,000
100	- (4)				.4.24										
CAPITAL COSTS	S														
	Development	2,286,000	2,074,800	723,900	723,900	571,500	571,500	571,500	381,000	203,200	203,200	203,200	203,200	63,500	8,780,400
	Mining Equipment	70,000		7,148,000											7,218,000
	Plant		9,500,000												9,500,000
	Tailings Dam		500,000	2,000,000											2,500,000
	Infrastructure		2,000,000	958,000											2,958,000
	Diamond Drilling	500,000	500000.000												1,000,000
	Environmental & Permitting	250,000	250000.000												500,000
	Closure												250,000	250,000	500,000
	EPCM		2,300,000	800,000											3,100,000
Tota	al	3,106,000	17,124,800	11,629,900	723,900	571,500	571,500	571,500	381,000	203,200	203,200	203,200	453,200	313,500	36,056,400
					,					SOR ANALISMO	Accordance agreement				
TOTAL CASH CO	OST	3,106,000	17,124,800	21,809,900	13,448,900	13,296,500	13,296,500	13,296,500	13,106,000	12,928,200	12,928,200	12,928,200	13,178,200	13,038,500	173,486,400
CASH SURPLUS	}	(3,106,000)	(17,124,800)	(3,860,157)	8,840,288	7,219,410	6,628,424	6,027,015	6,126,413	5,827,145	5,364,823	5,456,826	5,206,826	5,346,526	37,952,740

OP 7 100 17

CASHO15.WK1 BASE 1+10%au

CASE: Tax Free

Haulage Decline - Cut-off = 0.15 oz/ton (Au) @ 750 tpd & 5 days/week

NPV Cash Surplus IRR % \$6,732,778

			R	ESERVES SUMMA	ARY							METAL PRICES	
	Category		In Situ	Available	Grade	Diluted	Diluted	Recovery	Troy		Sold	360 U	0-00
			tons	tons	Au oz/t	tons	Au oz/t	%	ounces	S	Silver	4.00 U	IS\$/oz
	Indicated							0.92					90.0000
	Inferred							0.92				RECOVERY (Au)	0.906
	Total		0	0		0	0.22	0.92	0			(Ag)	0.620
	1 5 6 6												
PRODUCTION		Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Totals
PHODUCTION	Tons	rearo	1041	125,000	187,500	187,500	187,500	187,500	162,500	162,500	106,100	24,000	1,330,100
	Au oz/t			0.30	0.30	0.30	0.29	0.26	0.24	0.24	0.24	0.26	0.27
	Gold oz (mined)			37,772	55,840	55,840	54,205	48,910	38,861	38,861	25,493	6,310	362,091
	Silver oz (mined)			332,751	498,023	498,023	495,817	598,079	566,204	566,204	365,289	62,617	3,983,007
	Silver 02 (mined)			002,701	400,020	100,000		,					
	Gold oz (poured)			34221.251	50591.402	50591.402	49109.458	44312,822	35207.885	35207.885	23096.205	5716.498	328,055
	Silver oz (poured)		0.000	206305.620	308774.260	308774.260	307406.540	370808.980	351046.480	351046.480	226479,180	38822.540	2,469,464
													
REVENUES							.= .=	15.050.010	10.074.000	12,674,839	8,314,634	2,057,939	118,099,731
	Gold			12,319,650	18,212,905	18,212,905	17,679,405	15,952,616	12,674,839		905,917	155,290	9,877,857
	Silver			825,222	1,235,097	1,235,097	1,229,626	1,483,236	1,404,186	1,404,186 14,079,024	9,220,551	2,213,229	127,977,588
Gross	s			13,144,873	19,448,002	19,448,002	18,909,031	17,435,852	14,079,024	14,079,024	9,220,551	2,210,223	127,577,000
OPERATING CO	net												
OF ERATING OC	Mining (\$/ton)			35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	
	Tailings (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
	Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	
Tota	al (\$)			6,362,500	9,543,750	9,543,750	9,543,750	9,543,750	8,271,250	8,271,250	5,400,490	1,221,600	67,702,090
100	i (o)			5,000,000	5,5 .5,. 55		· · · · · · · · · · · · · · · · · · ·						
CAPITAL COST	S												
	Development	2286000.000	2,074,800	660,400	660,400	558,800	558,800	558,800	381,000	304,800	127,000		8,170,800
	Mining Equipment	70,000		7,148,000									7,218,000
	Plant		9,500,000										9,500,000
	Tailings Dam		500,000	2,000,000									2,500,000
	Infrastructure		2,000,000	958,000									2,958,000
	Diamond Drilling	500000.000	500000.000										1,000,000 500,000
	Encironmental & Permitting	250000,000	250000.000								050000 000	050000 000	
	Closure										250000.000	250000.000	500,000
	EPCM		2,300,000	800,000								050 000	3,100,000
Tota	al	3,106,000	17,124,800	11,566,400	660,400	558,800	558,800	558,800	381,000	304,800	377,000	250,000	35,446,800
TOTAL CASH C	COST	3,106,000	17,124,800	17,928,900	10,204,150	10,102,550	10,102,550	10,102,550	8,652,250	8,576,050	5,777,490	1,471,600	103,148,890
CASH SURPLU		(3,106,000)	(17,124,800)	(4,784,027)	9,243,852	9,345,452	8,806,481	7,333,302	5,426,774	5,502,974	3,443,061	741,629	24,828,698
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CASHO15.WK1 BASE 1-10%au

CASE:

Tax Free

Haulage Decline - Cut-off = 0.15 oz/ton (Au) @ 750 tpd & 5 days/week

NPV Cash Surplus

(\$5,337,290) 3%

Category		In Situ tons	ESERVES SUMM/ Available tons	ARY Grade Au oz/t	Diluted tons	Diluted Au oz/t	Recovery % 0.92	Troy ounces	Gold · Silver		METAL PRICES 360 US\$/oz 4.00 US\$/oz	
Indicated Inferred Total		0	0		0	0.22	0.92 0.92	0		I	RECOVERY (Au) (Ag)	0.906 0.620
PRODUCTION Tons Au oz/t Gold oz (mined) Silver oz (mined) Gold oz (poured) Silver oz (poured)	Year 0	Year 1	Year 2 125,000 0.25 30,904 332,751 27999.205 206305.620	Year 3 187,500 0.24 45,688 498,023 41392,966 308774,260	Year 4 187,500 0.24 45,688 498,023 41392,966 308774,260	Year 5 187,500 0.24 44,349 495,817 40180.466 307406.540	Year 6 187,500 0.21 40,018 598,079 36255.946 370808.980	Year 7 162,500 0.20 31,795 566,204 28806.451 351046.480	Year 8 162,500 0.20 31,795 566,204 28806.451 351046.480	Year 9 106,100 0.20 20,858 365,289 18896.895 226479.180	Year 10 24,000 0.22 5,162 62,617 4677.134 38822.540	Totals 1,330,100 0.22 296,257 3,983,007 268,408 2,469,464
REVENUES Gold Silver Gross			10,079,714 825,222 10,904,936	14,901,468 1,235,097 16,136,565	14,901,468 1,235,097 16,136,565	14,464,968 1,229,626 15,694,594	13,052,140 1,483,236 14,535,376	10,370,322 1,404,186 11,774,508	10,370,322 1,404,186 11,774,508	6,802,882 905,917 7,708,799	1,683,768 155,290 1,839,059	96,627,053 9,877,857 106,504,910
OPERATING COST Mining (\$/ton) Milling (\$/ton) Tailings (\$/ton) Admin (\$/ton) Total (\$)			35.20 13.50 0.40 1.80 6,362,500	35.20 13.50 0.40 1.80 9,543,750	35.20 13.50 0.40 1.80 9,543,750	35.20 13.50 0.40 1.80 9,543,750	35.20 13.50 0.40 1.80 9,543,750	35.20 13.50 0.40 1.80 8,271,250	35.20 13.50 0.40 1.80 8,271,250	35.20 13.50 0.40 1.80 5,400,490	35.20 13.50 0.40 1.80 1,221,600	67,702,090
CAPITAL COSTS Development Mining Equipment Plant Tailings Dam Infrastructure Diamond Drilling Encironmental & Permitting Closure EPCM Total	2286000.000 70,000 500000.000 250000.000	2,074,800 9,500,000 500,000 2,000,000 500000.000 250000.000 17,124,800	660,400 7,148,000 2,000,000 958,000 800,000 11,566,400	660,400 660,400	558,800 558,800	558,800 558,800	558,800 558,800	381,000 381,000	304,800	127,000 250000.000 377,000	250000.000 250,000	8,170,800 7,218,000 9,500,000 2,550,000 1,000,000 500,000 500,000 3,100,000 35,446,800
TOTAL CASH COST CASH SURPLUS	3,106,000 (3,106,000)	17,124,800 (17,124,800)	17,928,900 (7,023,964)	10,204,150 5,932,415	10,102,550 6,034,015	10,102,550 5,592,044	10,102,550 4,432,826	8,652,250 3,122,258	8,576,050 3,198,458	5,777,490 1,931,309	1,471,600 367,459	103,148,890 3,356,020

CASHO15.WK1 BASE 1+300

CASE:

Tax Free

Haulage Decline - Cut-off = 0.15 oz/ton (Au) @ 750 tpd & 5 days/week

NPV Cash Surplus IRR % \$8,383,164

METAL PRICES RESERVES SUMMARY 360 US\$/oz Gold Grade Diluted Diluted Recovery Troy In Situ Available Category 4.00 US\$/oz Silver ounces Au oz/t tons Au oz/t tons tons 0.92 Indicated RECOVERY (Au) 0.906 0.92 Inferred 0.620 (Ag) 0 0.22 0.92 0 0 0 Total Year 10 Totals Year 5 Year 6 Year 7 Year 8 Year 9 Year 3 Year 4 Year 2 PRODUCTION Year 0 Year 1 187,500 187,500 187,500 1,625,000 187,500 187,500 187,500 187,500 187,500 125,000 Tons 0.26 0.26 0.27 0.26 0.26 0.26 0.26 0.27 0.27 0.27 Au oz/t 49,277 431,528 49,277 49,277 49,277 50,764 49,277 49,277 34,338 50,764 Gold oz (mined) 495,817 4,303,699 495,817 495,817 495,817 332,751 498,023 498,023 495,817 495,817 Silver oz (mined) 390,964 44644.962 44644.962 44644.962 44644.962 44644.962 31110.228 45992.184 45992.184 44644.962 Gold oz (poured) 307406.540 307406.540 307406.540 307406.540 307406.540 2,668,293 0.000 206305.620 308774.260 308774.260 307406.540 Silver oz (poured) REVENUES 16,072,186 16,072,186 140,747,172 16,072,186 16,072,186 16,072,186 16,072,186 11,199,682 16,557,186 16,557,186 Gold 1.229.626 1,229,626 10,673,174 1,229,626 1,229,626 825,222 1,235,097 1,235,097 1,229,626 1,229,626 Silver 151,420,346 17,301,812 17,301,812 17,301,812 17,792,283 17,301,812 17,301,812 17,301,812 12,024,905 17,792,283 Gross OPERATING COST 35.20 35.20 35.20 35.20 35.20 35.20 35.20 Mining (\$/ton) 35.20 35.20 13.50 13.50 13.50 13.50 13.50 13.50 13.50 Milling (\$/ton) 13.50 13.50 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 0.40 Tailings (\$/ton) 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 1.80 Admin (\$/ton) 9,543,750 9,543,750 9,543,750 9,543,750 9,543,750 82,712,500 9,543,750 9,543,750 6,362,500 9,543,750 Total (\$) CAPITAL COSTS 8,170,800 558,800 381,000 304,800 127,000 660,400 558,800 558,800 Development 2286000.000 2,074,800 660,400 7,218,000 7,148,000 Mining Equipment 70,000 9,500,000 9,500,000 Plant 2,500,000 Tailings Dam 500,000 2,000,000 2,958,000 Infrastructure 2,000,000 958,000 1,000,000 500000.000 500000.000 Diamond Drilling 500,000 Encironmental & Permitting 250000.000 250000.000 500,000 250000.000 250000.000 Closure 3,100,000 2,300,000 800,000 **EPCM** 250,000 35,446,800 558,800 558,800 558,800 381,000 304,800 377,000 17,124,800 11,566,400 660,400 3,106,000 Total 9.920.750 9,793,750 118,159,300 9,848,550 17,928,900 10,204,150 10,102,550 10,102,550 10,102,550 9,924,750 TOTAL CASH COST 3,106,000 17,124,800 33,261,046 7,453,262 7,381,062 7,508,062 7,377,062 (17,124,800) (5,903,995)7,588,133 7,689,733 7,199,262 7,199,262 CASH SURPLUS (3,106,000)

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CASHO15.WK1 BASE 1+900

CASE: Tax Free

Haulage Decline - Cut-off = 0.15 oz/ton (Au) @ 750 tpd & 5 days/week

NPV Cash Surplus IRR %

\$12,950,282

	Category Indicated Inferred Total		In Situ tons	ESERVES SUMMAI Available tons	RY Grade Au oz/t	Diluted tons	Diluted Au oz/t 0.22	Recovery % 0.92 0.92 0.92	Troy ounces		iold	METAL PRICES 360 4.00 RECOVERY (Au) (Ag)			S\$/oz S\$/oz 0.906 0.620
PRODUCTION	Tons Au oz/t Gold oz (mined) Silver oz (mined)	Year O	Year 1	Year 2 125,000 0.27 34,338 332,751	Year 3 187,500 0.27 50,764 498,023	Year 4 187,500 0.27 50,764 498,023	Year 5 187,500 0.26 49,277 495,817	Year 6 187,500 0.26 49,277 495,817	Year 7 187,500 0.26 49,277 495,817	Year 8 187,500 0,26 49,277 495,817	Year 9 187,500 0.26 49,277 495,817	Year 10 187,500 0.26 49,277 495,817	Year 11 187,500 0.26 49,277 495,817	Year 112 187,500 0.26 49,277 495,817	Totals 2,000,000 0,27 530,082 5,295,333
	Gold oz (poured) Silver oz (poured)		0.000	31110.228 206305.620	45992.184 308774.260	45992.184 308774.260	44644.962 307406.540	44644.962 307406.540	44644.962 307406.540	44644.962 307406.540	44644.962 307406.540	44644.962 307406.540	44644.962 307406.540	44644.962 307406.540	390,964 2,668,293
REVENUES Gros	Gold Silver s			11,199,682 825,222 12,024,905	16,557,186 1,235,097 17,792,283	16,557,196 1,235,097 17,792,283	16,072,186 1,229,626 17,301,812	16,072,186 1,229,626 17,301,812	16,072,186 1,229,626 17,301,812	16,072,186 1,229,626 17,301,812	16,072,186 1,229,626 17,301,812	16,072,186 1,229,626 17,301,812	16,072,186 1,229,626 17,301,812	16,072,186 1,229,626 17,301,812	172,891,545 13,132,426 186,023,971
OPERATING CO	SST Mining (\$/ton) Milling (\$/ton) Tailings (\$/ton) Admin (\$/ton) J (\$)			35.20 13.50 0.40 1.80 6,362,500	35.20 13.50 0.40 1.80 9,543,750	35.20 13.50 0.40 1.80 9,543,750	35.20 13.50 0.40 1.80 9,543,750	101,800,000							
CAPITAL COST:	Development Mining Equipment Plant Tailings Dam Infrastructure Diamond Drilling Encironmental & Permitting Closure EPCM	2286000.000 70,000 500000.000 250000.000	2,074,800 9,500,000 500,000 2,000,000 50000,000 250000,000	660,400 7,148,000 2,000,000 958,000	660,400	558,800	558,800	558,800	381,000	304,800	127,000	250000.000	250000.000	250000.000	8,170,800 7,218,000 9,500,000 2,500,000 2,958,000 1,000,000 500,000 1,000,000 3,100,000
Tota		3,106,000	17,124,800	11,566,400	660,400	558,800	558,800	558,800	381,000	304,800	377,000	250,000	250,000	250,000	35,946,800
TOTAL CASH C CASH SURPLUS		3,106,000 (3,106,000)	17,124,800 (17,124,800)	17,928,900 (5,903,995)	10,204,150 7,588,133	10,102,550 7,689,733	10,102,550 7,199,262	10,102,550 7,199,262	9,924,750 7,377,062	9,848,550 7,453,262	9,920,750 7,381,062	9,793,750 7,508,062	9,793,750 7,508,062	9,793,750 7,508,062	137,746,800 48,277,171

base 3 +10%gold price

CASE:

Tax Free

Haulage Decline - Cut-off = 0.10 oz/ton (Au) @ 1000 tpd & 5 days/week

NPV Cash Surplus IRR % \$7,696,240 21

				ESERVES SUMMA				_	-		Sold	METAL PRICES 396 U	55/57
	Category		In Situ	Available	Grade "	Diluted	Diluted	Recovery %	Troy ounces		Silver	4.00 U	
	to Provide		tons	tons	Au oz/t	tons	Au oz/t	0.91	ounces		mver	4.00 0	00/02
	Indicated Inferred							0.91				RECOVERY (Au)	0.906
	Total		0	0		0	0.22	0.91	0			(Ag)	0.620
	Total		U	· ·		V	0.22	0.01	·			V-9/	
PRODUCTION		Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Totals
	Tons			200,000	250,000	250,000	250,000	250,000	205,000	125,000	73,000		1,603,000
	Au oz/t			0.26	0.26	0.23	0.23	0.22	0.20	0.19	0.18		0.22
	Gold oz (mined)			51,368	63,757	58,329	56,520	53,915	41,602	23,226	13,378	0	362,095
	Silver oz (mined)			482,079	602,502	601,340	600,952	701,048	664,313	471,947	285,527	0	4,409,708
	Gold oz (poured)			46539,408	57763.842	52846.074	51207.120	48846.990	37691.412	21042.756	12120.468	0.000	
	Silver oz (poured)			298888.980	373551.240	372830.800	372590.240	434649.760	411874.060	292607.140	177026.740	0.000	
	Silver 52 (poured)			200000.000	0.000								
REVENUES	2.24							10.010.100	14,925,799	8,332,931	4,799,705	0	129,910,996
	Gold			18,429,606	22,874,481	20,927,045	20,278,020 1,490,361	19,343,408 1,738,599	1,647,496	1,170,429	708,107	0	10,936,076
	Silver			1,195,556	1,494,205 24,368,686	1,491,323 22,418,369	21,768,380	21,082,007	16,573,295	9,503,360	5,507,812	0	140,847,072
Gros	s			19,625,161	24,300,000	22,416,369	21,700,300	21,002,007	10,575,255	0,000,000	0,007,012		
OPERATING CO	OST												
	Mining (\$/ton)			35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	
	Tailings (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
	Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	24 500 700
Tota	al (\$)			10,180,000	12,725,000	12,725,000	12,725,000	12,725,000	10,434,500	6,362,500	3,715,700	0	81,592,700
CAPITAL COST	-S												
	Development	2,286,000	2,074,800	723,900	723,900	571,500	571,500	571,500	381,000	203,200	63,500		8,170,800
	Mining Equipment	70,000		7,148,000									7,218,000
	Plant		9,500,000										9,500,000
	Tailings Dam		500,000	2,000,000									2,500,000
	Infrastructure		2,000,000	958,000	9								2,958,000
	Diamond Drilling	500,000	500000.000										1,000,000
	Environmental & Permitting	250,000	250000.000									Partition (Partition of Artista)	500,000
	Closure										250,000	250,000	500,000
	EPCM		2,300,000	800,000						000.05	010 ===	050 000	3,100,000
Tota	al	3,106,000	17,124,800	11,629,900	723,900	571,500	571,500	571,500	381,000	203,200	313,500	250,000	35,446,800
TOTAL CASH O	COST	3,106,000	17,124,800	21,809,900	13,448,900	13,296,500	13,296,500	13,296,500	10,815,500	6,565,700	4,029,200	250,000	117,039,500
CASH SURPLU		(3,106,000)	(17,124,800)	(2,184,739)	10,919,786	9,121,869	8,471,880	7,785,507	5,757,795	2,937,660	1,478,612		23,807,572
ONO TOO THE		(0, .00,000)	,,,	(2,1.5.,1.50)	, 5,5 . 5, . 50	-, , - 50	-11	an coreta	E \$10,000 \$0,000.	MAKEN YOU ALO IS IS		20 20 30	

BASE 3-10%au

CASE:

Tax Free
Haulage Decline - Cut-off = 0.10 oz/ton (Au) @ 1000 tpd & 5 days/week

NPV Cash Surplus IRR % (\$6,155,427)

			В	ESERVES SUMMA	ARY							METAL PRICES	
	Category		In Situ	Available	Grade	Diluted	Diluted	Recovery	Troy		iold		JS\$/oz
			tons	tons	Au oz/t	tons	Au oz/t	%	ounces	8	Silver	4.00 (JS\$/oz
	Indicated							0.91				DE00\(ED\(\(L\)	0.000
	Inferred					_		0.91				RECOVERY (Au)	0.906 0.620
	Total		0	0		0	0.22	0.91	0			(Ag)	0.620
PRODUCTION		Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Totals
THODOGHON	Tons	rear o	rear r	200,000	250,000	250,000	250,000	250,000	205,000	125,000	73,000		1,603,000
	Au oz/t			0.23	0.23	0.21	0.20	0.19	0.18	0.17	0.16		0.20
	Gold oz (mined)			46,231	57,381	52,496	50,868	48,524	37,442	20,903	12,040	0	325,886
	Silver oz (mined)			482,079	602,502	601,340	600,952	701,048	664,313	471,947	285,527	0	4,409,708
	5						**************************************	2 2 2					
	Gold oz (poured)			41885.467	51987.458	47561.467	46086.408	43962.291	33922.271	18938.480	10908.421	0.000	
	Silver oz (poured)			298888.980	373551.240	372830.800	372590.240	434649.760	411874.060	292607.140	177026.740	0.000	
REVENUES										0.017.050	0.007.000		100 000 015
	Gold			15,078,768	18,715,485	17,122,128	16,591,107	15,826,425	12,212,017	6,817,853	3,927,032 708,107	0	106,290,815 10,936,076
-	Silver			1,195,556	1,494,205	1,491,323	1,490,361	1,738,599	1,647,496	1,170,429		0	117,226,891
Gross	s			16,274,324	20,209,690	18,613,451	18,081,468	17,565,024	13,859,514	7,988,282	4,635,139	U	117,220,091
OPERATING CO	DST												
OFERATING CC	Mining (\$/ton)			35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	
	Tailings (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
	Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1,80	1.80	1.80	
Tota	al (\$)			10,180,000	12,725,000	12,725,000	12,725,000	12,725,000	10,434,500	6,362,500	3,715,700	0	81,592,700
	· · · · · · · · · · · · · · · · · · ·			55 . 55. 55. 55.			262 6						
CAPITAL COST	S												
	Development	2,286,000	2,074,800	723,900	723,900	571,500	571,500	571,500	381,000	203,200	63,500		8,170,800
	Mining Equipment	70,000		7,148,000									7,218,000
	Plant		9,500,000										9,500,000
	Tailings Dam		500,000	2,000,000									2,500,000
	Infrastructure		2,000,000	958,000	×								2,958,000
	Diamond Drilling	500,000	500000.000										1,000,000
	Environmental & Permitting	250,000	250000.000										500,000
	Closure										250,000	250,000	500,000
	EPCM	0.400.000	2,300,000	800,000	700 000	E71 E00	E71 E00	E71 E00	201 000	202 202	212 500	250,000	3,100,000 35,446,800
Tota	Al .	3,106,000	17,124,800	11,629,900	723,900	571,500	571,500	571,500	381,000	203,200	313,500	250,000	35,446,800
		×											
TOTAL CASH C	COST	3,106,000	17,124,800	21,809,900	13,448,900	13,296,500	13,296,500	13,296,500	10,815,500	6,565,700	4,029,200	250,000	117,039,500
CASH SURPLU		(3,106,000)	(17,124,800)	(5,535,576)	6,760,790	5,316,951	4,784,968	4,268,524	3,044,014	1,422,582	605,939	(250,000)	187,391
		(-1:1-20)	,, . = ., = /	(0)000(0.0)		CACCOCACO C			mater or stor in h			1.00	

BASE1+10%GOLD PRICE

CASE:

Tax Free
Haulage Decline - Cut-off = 0.15 oz/ton (Au) @ 750 tpd & 5 days/week

NPV Cash Surplus IRR % \$6,732,778 18%

			R	ESERVES SUMMA	ARY							METAL PRICES	
	Category		In Situ	Available	Grade	Diluted	Diluted	Recovery	Troy		Gold		JS\$/oz
			tons	tons	Au oz/t	tons	Au oz/t	%	ounces	\$	Silver	4.00 (JS\$/oz
	Indicated							0.92					
	Inferred							0.92				RECOVERY (Au)	0.906
	Total		0	0		0	0.22	0.92	0			(Ag)	0.620
PRODUCTION		Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Totals
111000011011	Tons	rear o	rear r	125,000	187,500	187,500	187,500	187,500	162,500	162,500	106,100	24,000	1,330,100
	Au oz/t			0.27	0.27	0.27	0.26	0.24	0.22	0.22	0.22	0.24	0.25
	Gold oz (mined)			34,338	50,764	50,764	49,277	44,464	35,328	35,328	23,175	5,736	329,174
	Silver oz (mined)			332,751	498,023	498,023	495,817	598,079	566,204	566,204	365,289	62,617	3,983,007
	Silver 02 (milled)			002,701	400,020	400,020	400,017	000,070	000,00		,		
	Gold oz (poured)			31110.228	45992.184	45992.184	44644.962	40284.384	32007.168	32007.168	20996.550	5196.816	298,232
	Silver oz (poured)		0.000	206305.620	308774.260	308774.260	307406.540	370808.980	351046.480	351046.480	226479.180	38822.540	2,469,464
	(,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,												
REVENUES													
	Gold			12,319,650	18,212,905	18,212,905	17,679,405	15,952,616	12,674,839	12,674,839	8,314,634	2,057,939	118,099,731
	Silver			825,222	1,235,097	1,235,097	1,229,626	1,483,236	1,404,186	1,404,186	905,917	155,290	9,877,857
Gross	5			13,144,873	19,448,002	19,448,002	18,909,031	17,435,852	14,079,024	14,079,024	9,220,551	2,213,229	127,977,588 96.21
													16 17
OPERATING CO													
	Mining (\$/ton)			35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	
	Milling (\$/ton)			13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	
	Tailings (\$/ton)			0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
	Admin (\$/ton)			1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	1.80	
Total	I (\$)			6,362,500	9,543,750	9,543,750	9,543,750	9,543,750	8,271,250	8,271,250	5,400,490	1,221,600	67,702,090
0.074.0007													
CAPITAL COSTS		0000000 000	0.074.000	660 400	660 400	558,800	558,800	558,800	381,000	304,800	127,000		8,170,800
	Development	2286000.000	2,074,800	660,400	660,400	558,800	558,800	558,800	381,000	304,800	127,000		7,218,000
	Mining Equipment	70,000	0.500.000	7,148,000									9,500,000
	Plant		9,500,000	0.000.000									
	Tailings Dam		500,000	2,000,000									2,500,000 2,958,000
	Infrastructure		2,000,000	958,000									1,000,000
	Diamond Drilling	500000.000	500000.000										500,000
	Encironmental & Permitting	250000.000	250000.000								050000 000	050000 000	
	Closure										250000.000	250000.000	500,000
	EPCM		2,300,000	800,000								050 000	3,100,000
Total	I	3,106,000	17,124,800	11,566,400	660,400	558,800	558,800	558,800	381,000	304,800	377,000	250,000	35,446,800
TOTAL CASH CO	OST	3,106,000	17,124,800	17,928,900	10,204,150	10,102,550	10,102,550	10,102,550	8,652,250	8,576,050	5,777,490	1,471,600	103,148,890
CASH SURPLUS		(3,106,000)	(17,124,800)	(4,784,027)	9,243,852	9,345,452	8,806,481	7,333,302	5,426,774	5,502,974	3,443,061	741,629	24,828,698
CASI I SUITELUS	9	(0,100,000)	(11,124,000)	(4,704,027)	3,240,002	3,040,402	0,000,401	7,000,002	0,720,774	0,002,074	0,410,001	7 - 1,020	24,020,000

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BASE1-10%GOLD PRICE

CASE:

Tax Free

Haulage Decline - Cut-off = 0.15 oz/ton (Au) @ 750 tpd & 5 days/week

NPV Cash Surplus IRR % (\$5,337,290)

			R	ESERVES SUMMA	ARY							METAL PRICES	
	Category		In Situ	Available	Grade	Diluted	Diluted	Recovery	Troy		Gold	324 U	
			tons	tons	Au oz/t	tons	Au oz/t	%	ounces	8	Silver	4.00 U	S\$/oz
	Indicated							0.92			_	1500\((50\((4)	0.906
	Inferred					_		0.92			-	RECOVERY (Au)	0.620
	Total		0	0		0	0.22	0.92	0			(Ag)	0.620
PRODUCTION		Year 0	Year 1	Year 2	Year 3	Year 4	Year 5	Year 6	Year 7	Year 8	Year 9	Year 10	Totals
111000011011	Tons	1.440.4		125,000	187,500	187,500	187,500	187,500	162,500	162,500	106,100	24,000	1,330,100
	Au oz/t			0.27	0.27	0.27	0.26	0.24	0.22	0.22	0.22	0.24	0.25
	Gold oz (mined)			34,338	50,764	50,764	49,277	44,464	35,328	35,328	23,175	5,736	329,174
	Silver oz (mined)			332,751	498,023	498,023	495,817	598,079	566,204	566,204	365,289	62,617	3,983,007
	Gold oz (poured)			31110.228	45992.184	45992.184	44644.962	40284.384	32007.168	32007.168	20996,550	5196.816	298,232
	Silver oz (poured)		0.000	206305.620	308774.260	308774.260	307406.540	370808.980	351046.480	351046.480	226479.180	38822.540	2,469,464
REVENUES												1 000 700	00 007 050
	Gold			10,079,714	14,901,468	14,901,468	14,464,968	13,052,140	10,370,322	10,370,322	6,802,882	1,683,768	96,627,053
	Silver			825,222	1,235,097	1,235,097	1,229,626	1,483,236	1,404,186	1,404,186	905,917	155,290	9,877,857
Gros	s			10,904,936	16,136,565	16,136,565	15,694,594	14,535,376	11,774,508	11,774,508	7,708,799	1,839,059	106,504,910
													8
OPERATING CO				25.00	35.20	35.20	35.20	35.20	35.20	35.20	35.20	35.20	
	Mining (\$/ton)			35.20	13.50	13.50	13.50	13.50	13.50	13.50	13.50	13.50	
	Milling (\$/ton)			13.50 0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	0.40	
	Tailings (\$/ton)					1.80	1.80	1.80	1.80	1.80	1.80	1.80	
T-1-	Admin (\$/ton)			1.80 6,362,500	1.80 9,543,750	9,543,750	9,543,750	9,543,750	8,271,250	8,271,250	5,400,490	1,221,600	67,702,090
lota	al (\$)			6,362,500	9,543,750	9,543,750	9,545,750	9,545,750	6,271,250	0,271,200	3,400,400	1,221,000	50.90
CAPITAL COST	'S												
OAI ITAL OOOT	Development	2286000.000	2,074,800	660,400	660,400	558,800	558,800	558,800	381,000	304,800	127,000		8,170,800
	Mining Equipment	70,000	2,014,000	7,148,000	1000(100	555,555	,						7,218,000
	Plant	. 0,000	9,500,000	.,,									9,500,000
	Tailings Dam		500,000	2,000,000									2,500,000
	Infrastructure		2,000,000	958,000									2,958,000
	Diamond Drilling	500000.000	500000.000	000,000									1,000,000
	Encironmental & Permitting	250000.000	250000.000										500,000
	Closure	230000.000	200000.000								250000.000	250000.000	500,000
	EPCM		2,300,000	800,000									3.100.000
Tota		3,106,000	17,124,800	11,566,400	660,400	558,800	558,800	558,800	381,000	304,800	377,000	250,000	35,446,800 26.65
100	21	0,100,000	17,124,000	11,000,400	000,400	000,000	555,555	000,000	55.1,555	11	and street.		26.63
TOTAL CASH C	COST	3,106,000	17,124,800	17,928,900	10,204,150	10,102,550	10,102,550	10,102,550	8,652,250	8,576,050	5,777,490	1,471,600	103,148,890
CASH SURPLU		(3,106,000)	(17,124,800)	(7,023,964)	5,932,415	6,034,015	5,592,044	4,432,826	3,122,258	3,198,458	1,931,309	367,459	3,356,020
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